Appendix A

Water Model Inputs and Results

Future Growth Water Demands

Short-Term

Node	ADD (L/s)	MDD (L/s)	PHD (L/s)
BBR	15.4983	21.6976	32.5464
J10011	0.3079	0.4310	0.6465
J10014	0.0000	0.0000	0.0000
J10015	0.0000	0.0000	0.0000
J10033	0.0000	0.0000	0.0000
J10034	0.0000	0.0000	0.0000
J10036	0.0000	0.0000	0.0000
J10068	0.1053	0.1475	0.2212
J10084	0.0000	0.0000	0.0000
J10089	0.1053	0.1475	0.2212
J10098	1.9242	2.6939	4.0408
J10099	0.1134	0.1588	0.2382
J10100	0.4537	0.6352	0.9528
J10101	1.7378	2.4330	3.6495
J10107	0.0000	0.0000	0.0000
J10110	0.0000	0.0000	0.0000
J10114	0.0000	0.0000	0.0000
J10117	0.3038	0.4253	0.6380
J10141	0.0000	0.0000	0.0000
J10143	0.0000	0.0000	0.0000
J10152	0.0000	0.0000	0.0000
J10158	2.2720	3.1808	4.7712
J10185	1.6447	2.3025	3.4538
J-1071	0.3711	0.5195	0.7792
J-1134	0.9765	1.3671	2.0507
J-115	0.9884	1.3838	2.0757
J-1198	0.0000	0.0000	0.0000
J-1219	0.0000	0.0000	0.0000
J-1227	0.0000	0.0000	0.0000
J-1292	0.0000	0.0000	0.0000
J-1342	0.0000	0.0000	0.0000
J-1405	0.0000	0.0000	0.0000
J-1450	0.4752	0.6653	0.9979
J-1548	0.0000	0.0000	0.0000
J-1564	0.8593	1.2031	1.8046
J-1582	0.9439	1.3215	1.9823
J-1800	1.9139	2.6795	4.0193
J-1844	0.0000	0.0000	0.0000
J-1887	0.0000	0.0000	0.0000
J-19	0.1944	0.2722	0.4083
J-1912	0.0456	0.0638	0.0957
J-1979	0.0000	0.0000	0.0000
J-1980	0.0000	0.0000	0.0000
J-2014	0.0000	0.0000	0.0000
J-2125	0.0000	0.0000	0.0000
J-2137	0.0000	0.0000	0.0000
J-2141	0.0000	0.0000	0.0000
J-2143	0.0000	0.0000	0.0000
J-2145	0.0000	0.0000	0.0000
J-2146	0.0000	0.0000	0.0000
J-2167	0.0000	0.0000	0.0000
J-2168	0.0000	0.0000	0.0000
J-2316	0.0000	0.0000	0.0000
J-2337	0.0000	0.0000	0.0000
J-2344	0.1620	0.2269	0.3403
J-2552	0.7656	1.0719	1.6078
J-2563	0.7859	1.1002	1.6503
J-2566	0.0365	0.0510	0.0766
J-2592	0.0000	0.0000	0.0000
J-28	2.2442	3.1419	4.7128
J-2803	0.0000	0.0000	0.0000
J-2817	0.0000	0.0000	0.0000
J-2824	0.0000	0.0000	0.0000
J-2891	0.0000	0.0000	0.0000
J-2964	0.0000	0.0000	0.0000
J-318	0.0000	0.0000	0.0000
J-3270	0.0000	0.0000	0.0000
J-3344	0.2930	0.4101	0.6152
J-350	0.0000	0.0000	0.0000
J-3513	1.3085	1.8319	2.7479
J-3547	0.0000	0.0000	0.0000
J-3560	0.0000	0.0000	0.0000
J-388	0.0000	0.0000	0.0000
J-394	0.0000	0.0000	0.0000
J-3999	0.3906	0.5468	0.8202
J-4158	0.9277	1.2987	1.9481
J-4187	0.0486	0.0681	0.1021
J-4272	0.0000	0.0000	0.0000
J-4275	0.0000	0.0000	0.0000
J-4280	0.0000	0.0000	0.0000
J-43	5.9711	8.3595	12.5392
J-4339	0.5404	0.7565	1.1347
J-4342	0.0000	0.0000	0.0000
J-438	0.4051	0.5671	0.8507
J-4438	0.0000	0.0000	0.0000
J-4444	0.0000	0.0000	0.0000
J-4446	0.0716	0.1003	0.1504
J-455	0.0000	0.0000	0.0000
J-4642	0.0000	0.0000	0.0000
J-4651	0.0000	0.0000	0.0000
J-4660	0.0000	0.0000	0.0000
J-4663	0.0000	0.0000	0.0000
J-4702	1.6080	2.2512	3.3767
J-473	0.9682	1.3554	2.0332
J-4838	0.0000	0.0000	0.0000
J-4839	0.0000	0.0000	0.0000
J-4840	0.0000	0.0000	0.0000
J-4885	0.5247	0.7346	1.1019
J-4888	0.0000	0.0000	0.0000
J-4905	0.0000	0.0000	0.0000
J-4910	0.0000	0.0000	0.0000
J-582	0.4780	0.6692	1.0038
J-63	19.6875	27.5625	41.3438
J-746	0.0000	0.0000	0.0000
J-832	0.0000	0.0000	0.0000
J-870	0.0000	0.0000	0.0000
J-89	0.4740	0.6635	0.9953

Mid-Term

Node	ADD (L/s)	MDD (L/s)	PHD (L/s)
BBR	30.6285	42.8799	64.3198
J10011	0.3079	0.4310	0.6465
J10014	0.0000	0.0000	0.0000
J10015	0.7015	0.9821	1.4731
J10033	7.6219	10.6707	16.0060
J10034	6.7861	9.5006	14.2508
J10036	0.6015	0.8421	1.2631
J10068	0.1053	0.1475	0.2212
J10084	1.5783	2.2096	3.3144
J10089	0.1053	0.1475	0.2212
J10098	1.9242	2.6939	4.0408
J10099	0.1134	0.1588	0.2382
J10100	0.4537	0.6352	0.9528
J10101	1.7378	2.4330	3.6495
J10107	0.0250	0.0351	0.0526
J10110	0.3241	0.4537	0.6806
J10114	2.9061	4.0685	6.1028
J10117	0.3038	0.4253	0.6380
J10141	0.0000	0.0000	0.0000
J10143	0.2269	0.3176	0.4764
J10152	1.4744	2.0642	3.0963
J10158	3.4637	4.8492	7.2737
J10185	1.6447	2.3025	3.4538
J-1071	0.3711	0.5195	0.7792
J-1134	0.9765	1.3671	2.0507
J-115	0.9884	1.3838	2.0757
J-1198	0.0000	0.0000	0.0000
J-1219	0.0000	0.0000	0.0000
J-1227	0.0000	0.0000	0.0000
J-1292	0.0000	0.0000	0.0000
J-1342	0.0000	0.0000	0.0000
J-1405	0.3889	0.5444	0.8167
J-1450	0.4752	0.6653	0.9979
J-1548	0.0000	0.0000	0.0000
J-1564	0.8593	1.2031	1.8046
J-1582	0.9641	1.3498	2.0247
J-1800	1.9139	2.6795	4.0193
J-1844	0.0324	0.0454	0.0681
J-1887	0.4444	0.6221	0.9331
J-19	0.1944	0.2722	0.4083
J-1912	0.0456	0.0638	0.0957
J-1979	2.8415	3.9781	5.9671
J-1980	0.2006	0.2808	0.4213
J-2014	1.1343	1.5880	2.3819
J-2125	0.1001	0.1402	0.2103
J-2137	6.1843	8.6580	12.9870
J-2141	0.0000	0.0000	0.0000
J-2143	2.5653	3.5914	5.3871
J-2145	19.2215	26.9101	40.3651
J-2146	15.2480	21.3472	32.0208
J-2167	4.5798	6.4117	9.6176
J-2168	4.6597	6.5235	9.7853
J-2316	0.0000	0.0000	0.0000
J-2337	1.7500	2.4500	3.6750
J-2344	0.1620	0.2269	0.3403
J-2552	0.7656	1.0719	1.6078
J-2563	0.7859	1.1002	1.6503
J-2566	0.0365	0.0510	0.0766
J-2592	0.0000	0.0000	0.0000
J-28	2.2442	3.1419	4.7128
J-2803	0.4346	0.6084	0.9126
J-2817	0.0000	0.0000	0.0000
J-2824	0.4761	0.6665	0.9997
J-2891	0.0202	0.0283	0.0424
J-2964	10.5837	14.8172	22.2258
J-318	1.6562	2.3187	3.4781
J-3270	3.6773	5.1482	7.7223
J-3344	0.2930	0.4101	0.6152
J-350	0.3838	0.5373	0.8059
J-3513	1.3085	1.8319	2.7479
J-3547	0.0000	0.0000	0.0000
J-3560	0.3030	0.4242	0.6362
J-388	0.0000	0.0000	0.0000
J-394	1.9794	2.7712	4.1567
J-3999	0.3906	0.5468	0.8202
J-4158	0.9277	1.2987	1.9481
J-4187	0.0486	0.0681	0.1021
J-4272	0.0000	0.0000	0.0000
J-4275	0.8685	1.2159	1.8239
J-4280	0.0000	0.0000	0.0000
J-43	5.9711	8.3595	12.5392
J-4339	0.5404	0.7565	1.1347
J-4342	0.1212	0.1697	0.2545
J-438	0.4051	0.5671	0.8507
J-4438	0.6463	0.9049	1.3573
J-4444	0.4646	0.6504	0.9756
J-4446	0.0716	0.1003	0.1504
J-455	0.0000	0.0000	0.0000
J-4642	1.6045	2.2463	3.3694
J-4651	64.6852	90.5593	135.8389
J-4660	0.0250	0.0351	0.0526
J-4663	19.5896	27.4255	41.1382
J-4702	1.6080	2.2512	3.3767
J-473	0.9682	1.3554	2.0332
J-4838	0.3241	0.4537	0.6806
J-4839	0.0000	0.0000	0.0000
J-4840	0.0000	0.0000	0.0000
J-4885	0.5247	0.7346	1.1019
J-4888	9.1192	12.7668	19.1502
J-4905	0.2006	0.2808	0.4213
J-4910	1.8722	2.6210	3.9316
J-582	0.4780	0.6692	1.0038
J-63	67.7315	94.8241	142.2361
J-746	0.0404	0.0566	0.0848
J-832	0.0000	0.0000	0.0000
J-870	0.0000	0.0000	0.0000
J-89	0.4740	0.6635	0.9953

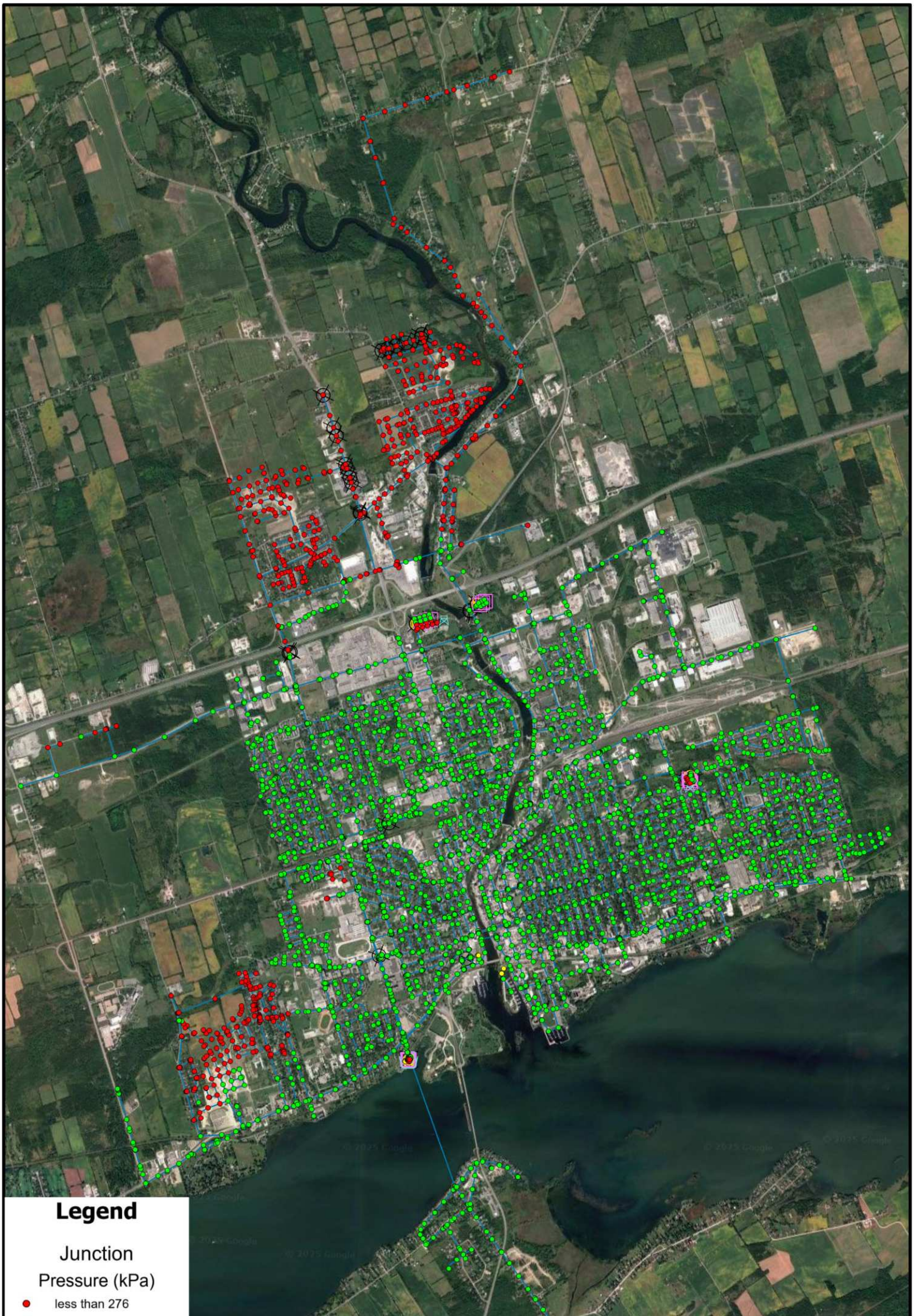
Long-Term

Node	ADD (L/s)	MDD (L/s)	PHD (L/s)
BBR	45.7587	64.0622	96.0932
J10011	0.3079	0.4310	0.6465
J10014	0.0000	0.0000	0.0000
J10015	0.7015	0.9821	1.4731
J10033	7.6219	10.6707	16.0060
J10034	6.7861	9.5006	14.2508
J10036	0.6015	0.8421	1.2631
J10068	0.1053	0.1475	0.2212
J10084	1.5783	2.2096	3.3144
J10089	0.1053	0.1475	0.2212
J10098	1.9242	2.6939	4.0408
J10099	0.1134	0.1588	0.2382
J10100	0.4537	0.6352	0.9528
J10101	1.7378	2.4330	3.6495
J10107	0.0250	0.0351	0.0526
J10110	0.3241	0.4537	0.6806
J10114	2.9061	4.0685	6.1028
J10117	0.3038	0.4253	0.6380
J10141	0.0000	0.0000	0.0000
J10143	0.2269	0.3176	0.4764
J10152	1.4744	2.0642	3.0963
J10158	3.4637	4.8492	7.2737
J10185	1.6447	2.3025	3.4538
J-1071	0.3711	0.5195	0.7792
J-1134	0.9765	1.3671	2.0507
J-115	0.9884	1.3838	2.0757
J-1198	0.0000	0.0000	0.0000
J-1219	0.0000	0.0000	0.0000
J-1227	0.0000	0.0000	0.0000
J-1292	0.0000	0.0000	0.0000
J-1342	0.0000	0.0000	0.0000
J-1405	0.3889	0.5444	0.8167
J-1450	0.4752	0.6653	0.9979
J-1548	0.0000	0.0000	0.0000
J-1564	0.8593	1.2031	1.8046
J-1582	0.9641	1.3498	2.0247
J-1800	1.9139	2.6795	4.0193
J-1844	0.0324	0.0454	0.0681
J-1887	0.4444	0.6221	0.9331
J-19	0.1944	0.2722	0.4083
J-1912	0.0456	0.0638	0.0957
J-1979	2.8415	3.9781	5.9671
J-1980	0.2006	0.2808	0.4213
J-2014	1.1343	1.5880	2.3819
J-2125	0.1001	0.1402	0.2103
J-2137	6.1843	8.6580	12.9870
J-2141	0.0000	0.0000	0.0000
J-2143	2.5653	3.5914	5.3871
J-2145	19.2215	26.9101	40.3651
J-2146	18.7156	26.2018	39.3028
J-2167	4.5798	6.4117	9.6176
J-2168	4.6597	6.5235	9.7853
J-2316	0.0000	0.0000	0.0000
J-2337	1.7500	2.4500	3.6750
J-2344	0.1620	0.2269	0.3403
J-2552	0.7656	1.0719	1.6078
J-2563	0.7859	1.1002	1.6503
J-2566	0.0365	0.0510	0.0766
J-2592	0.0000	0.0000	0.0000
J-28	2.2442	3.1419	4.7128
J-2803	0.4346	0.6084	0.9126
J-2817	0.0000	0.0000	0.0000
J-2824	0.4761	0.6665	0.9997
J-2891	0.0202	0.0283	0.0424
J-2964	10.5837	14.8172	22.2258
J-318	1.6562	2.3187	3.4781
J-3270	3.6773	5.1482	7.7223
J-3344	0.2930	0.4101	0.6152
J-350	0.3838	0.5373	0.8059
J-3513	1.3085	1.8319	2.7479
J-3547	0.0000	0.0000	0.0000
J-3560	0.3030	0.4242	0.6362
J-388	0.0000	0.0000	0.0000
J-394	1.9794	2.7712	4.1567
J-3999	0.3906	0.5468	0.8202
J-4158	0.9277	1.2987	1.9481
J-4187	0.0486	0.0681	0.1021
J-4272	0.0000	0.0000	0.0000
J-4275	0.8685	1.2159	1.8239
J-4280	0.0000	0.0000	0.0000
J-43	5.9711	8.3595	12.5392
J-4339	0.5404	0.7565	1.1347
J-4342	0.1212	0.1697	0.2545
J-438	0.4051	0.5671	0.8507
J-4438	0.6463	0.9049	1.3573
J-4444	0.4646	0.6504	0.9756
J-4446	0.0716	0.1003	0.1504
J-455	0.0000	0.0000	0.0000
J-4642	1.6045	2.2463	3.3694
J-4651	64.6852	90.5593	135.8389
J-4660	0.0250	0.0351	0.0526
J-4663	19.5896	27.4255	41.1382
J-4702	1.6080	2.2512	3.3767
J-473	0.9682	1.3554	2.0332
J-4838	0.3241	0.4537	0.6806
J-4839	0.0000	0.0000	0.0000
J-4840	0.0000	0.0000	0.0000
J-4885	0.5247	0.7346	1.1019
J-4888	9.1192	12.7668	19.1502
J-4905	0.2006	0.2808	0.4213
J-4910	1.8722	2.6210	3.9316
J-582	0.4780	0.6692	1.0038
J-63	104.9190	146.8866	220.3299
J-746	0.0404	0.0566	0.0848
J-832	0.0000	0.0000	0.0000
J-870	0.0000	0.0000	0.0000
J-89	0.4740	0.6635	0.9953

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

PEAK HOUR DEMAND PRESSURE RESULTS - SHORT-TERM GROWTH - SCENARIO 1 - NO WATER SUPPLY UPGRADES	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-1

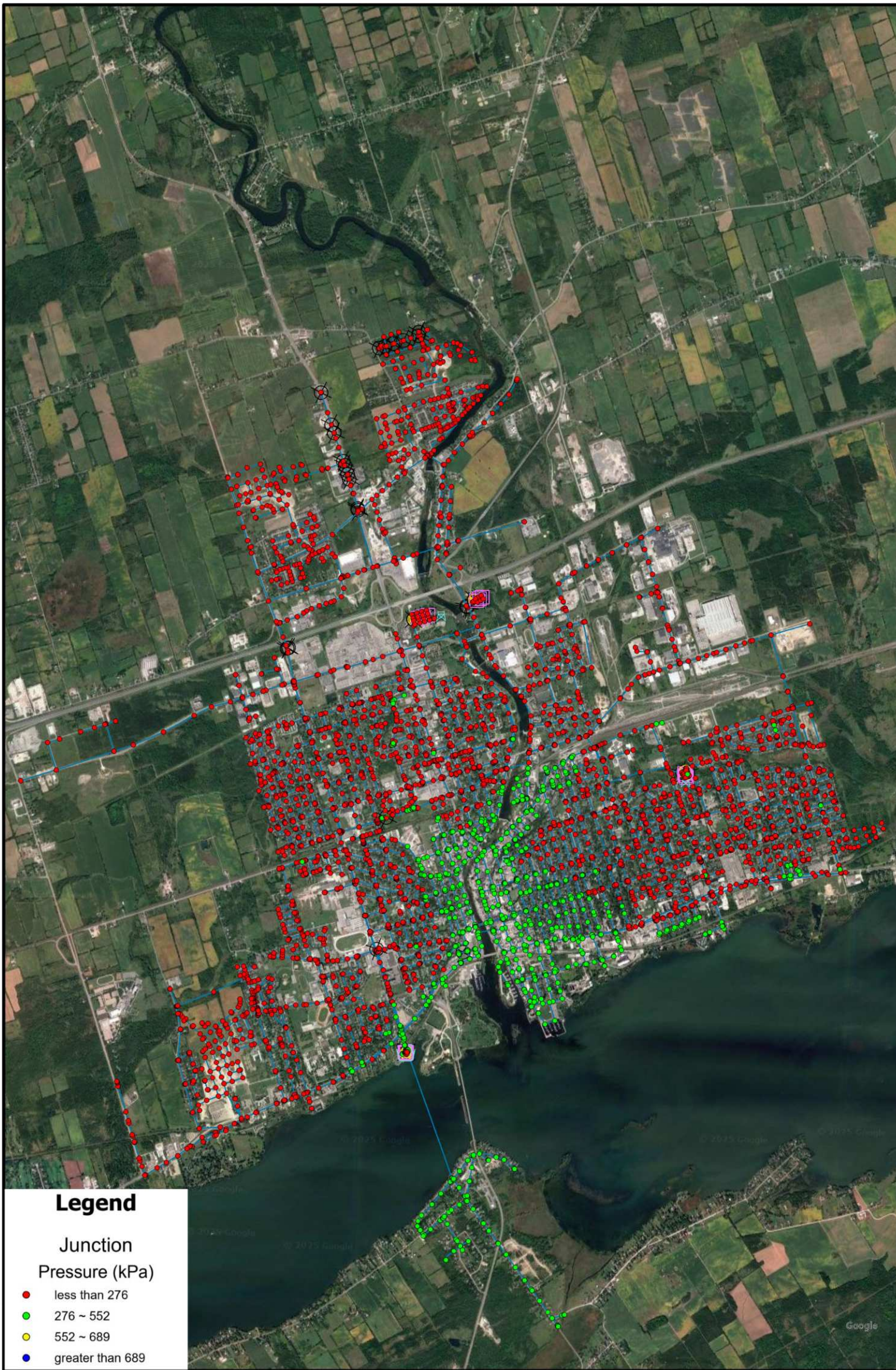
Plot Date: Friday, February 21, 2025 10:19 AM



PEAK HOUR DEMAND PRESSURE RESULTS - SHORT-TERM GROWTH - SCENARIO 2 - NO WATER SUPPLY UPGRADES	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS·ARCHITECTS·PLANNERS	32874-000 A-2

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

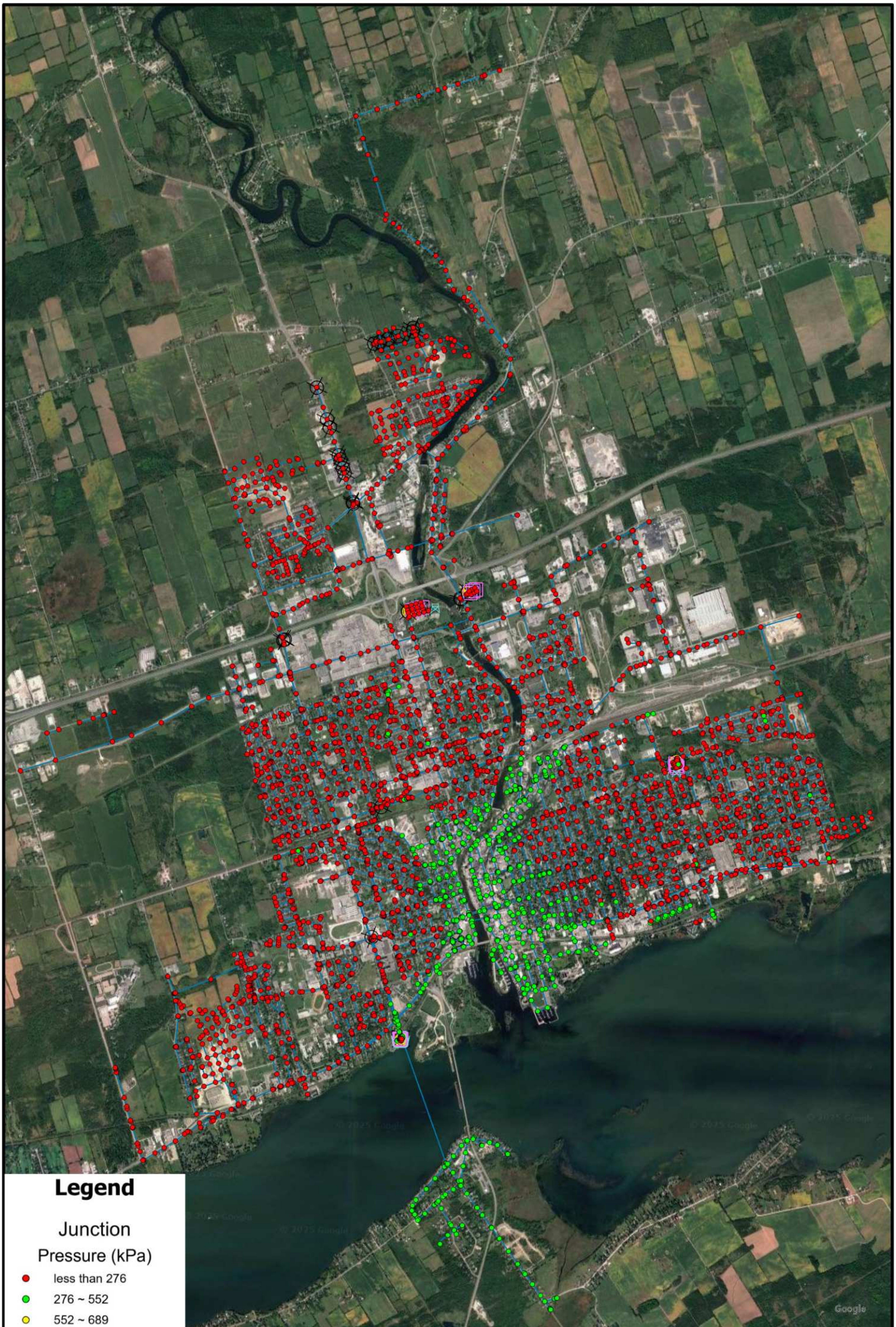
Plot Date: Friday, February 21, 2025 10:30 AM



PEAK HOUR DEMAND PRESSURE RESULTS - MID-TERM GROWTH - SCENARIO 1 - NO WATER SUPPLY UPGRADES	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-3

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

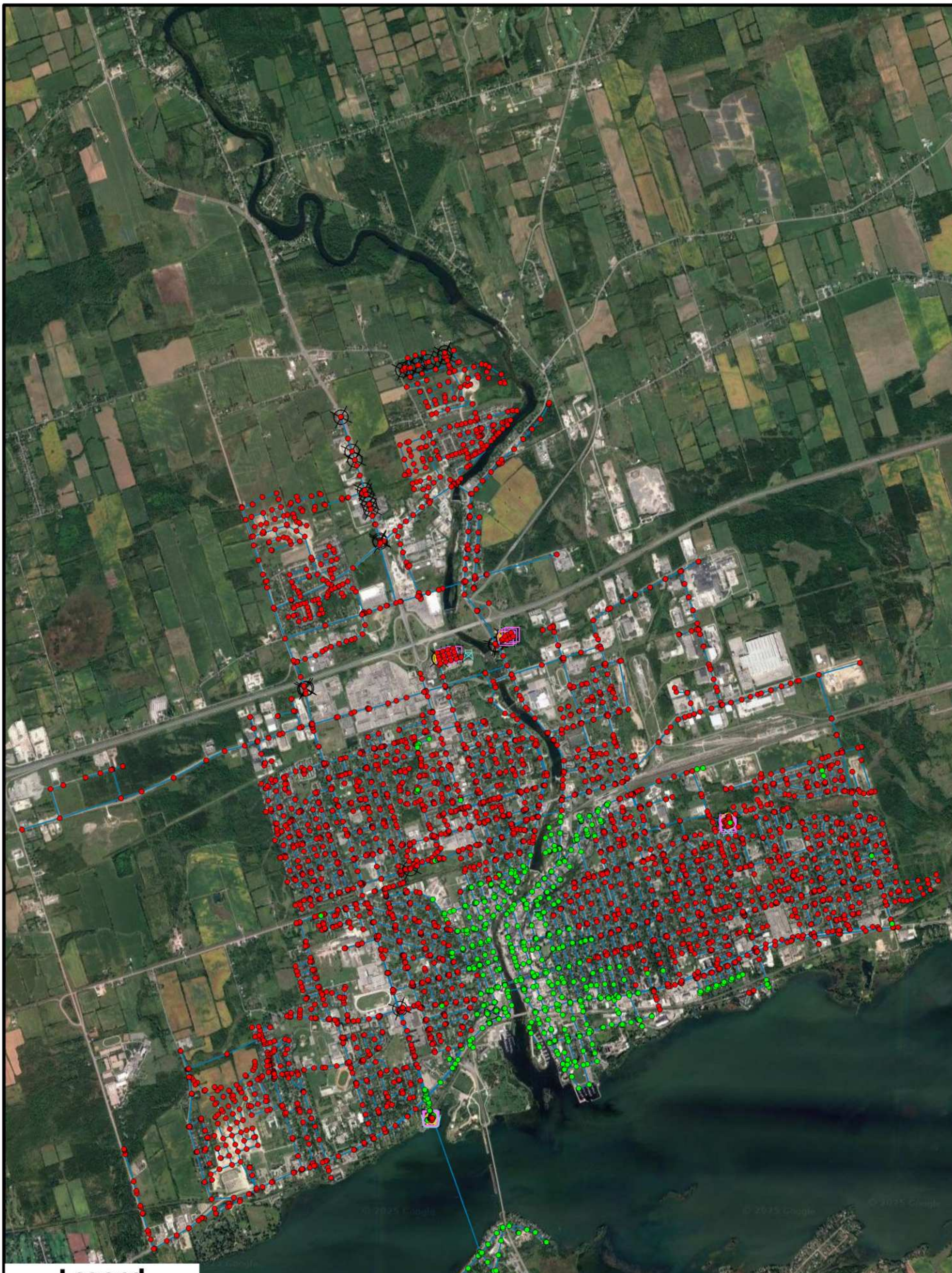
Plot Date: Friday, February 21, 2025 10:37 AM



PEAK HOUR DEMAND PRESSURE RESULTS - MID-TERM GROWTH - SCENARIO 2 - NO WATER SUPPLY UPGRADES	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-4

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

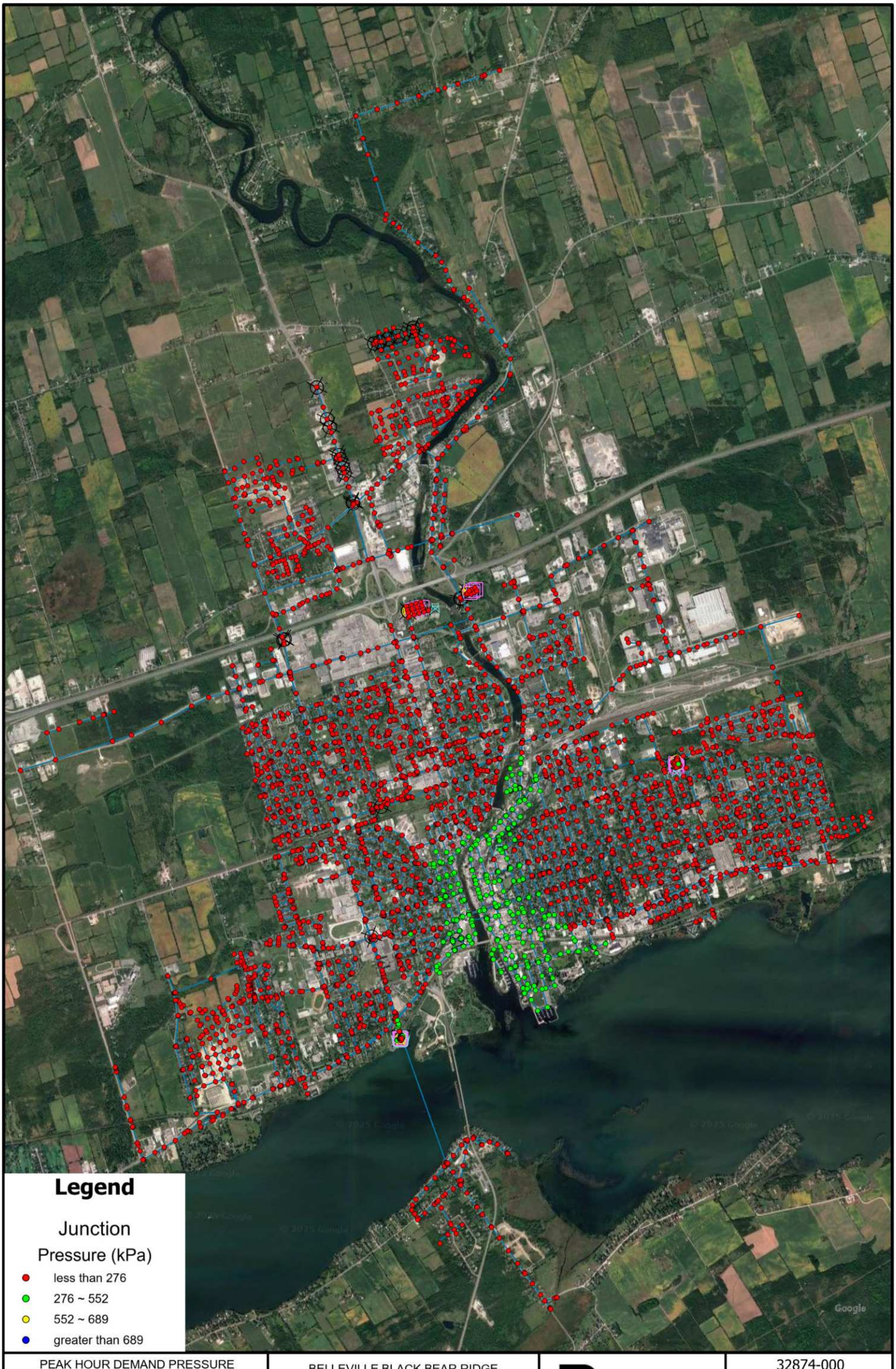
Plot Date: Friday, February 21, 2025 10:49 AM



PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - SCENARIO 1 - NO WATER SUPPLY UPGRADES	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-5

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 10:50 AM



PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - SCENARIO 2 - NO WATER SUPPLY UPGRADES

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

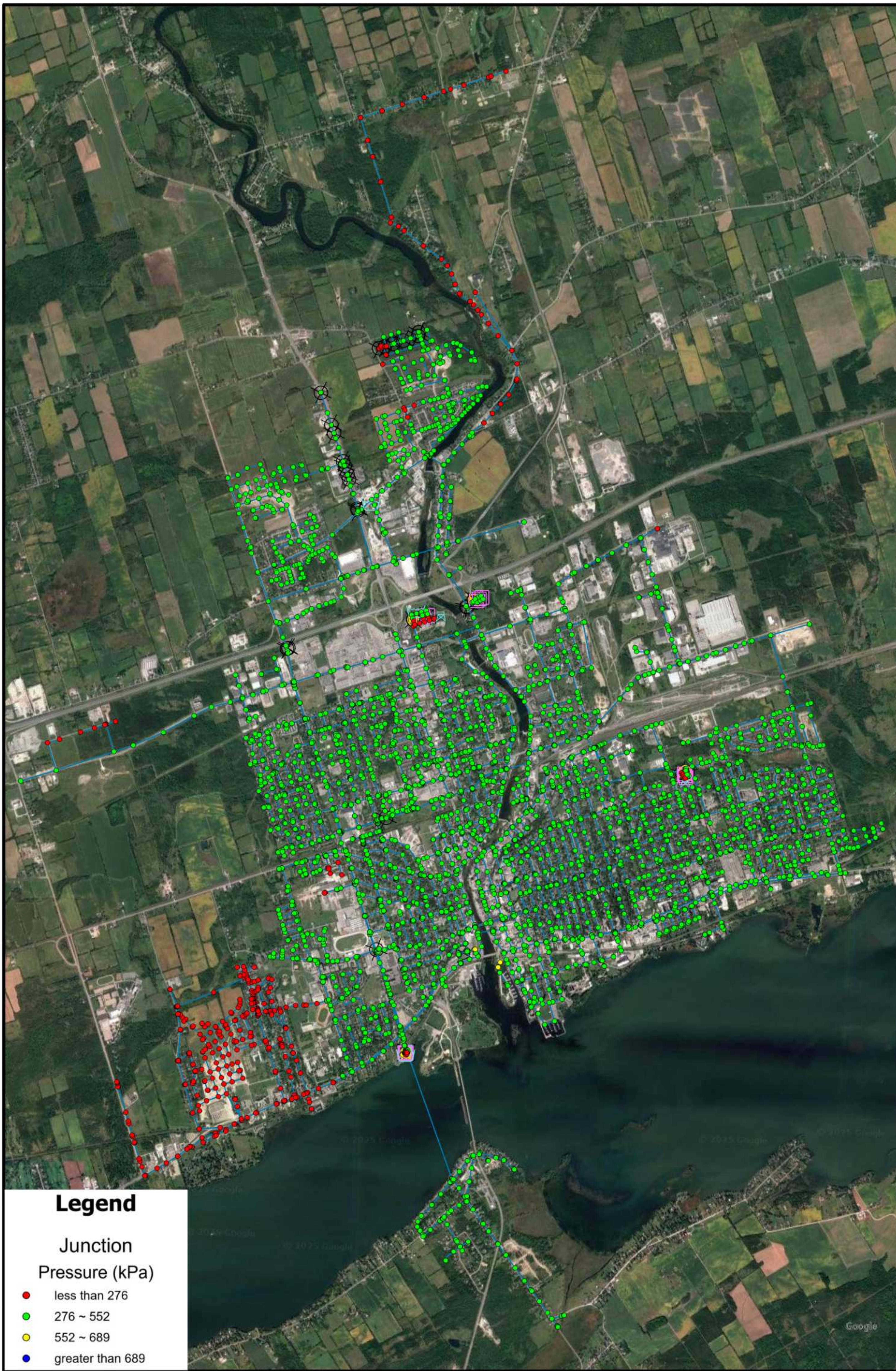
J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

32874-000

A-6

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 10:53 AM



PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - WATER SUPPLY UPGRADE CONFIGURATION 1

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

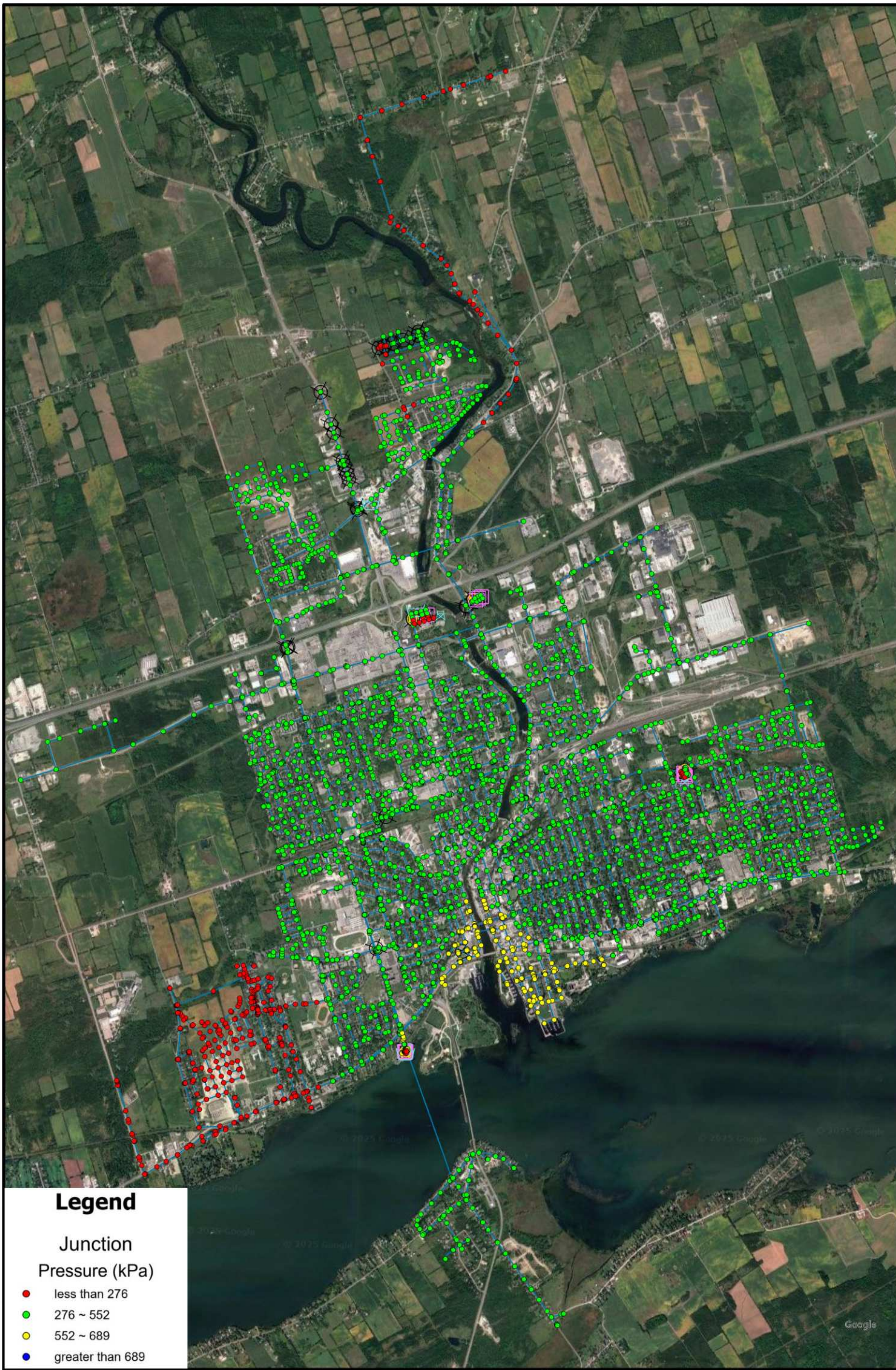
J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

32874-000

A-7

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:07 AM



PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - WATER SUPPLY UPGRADE CONFIGURATION 2	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-8

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:11 AM

PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - WATER SUPPLY UPGRADE CONFIGURATION 3	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-9

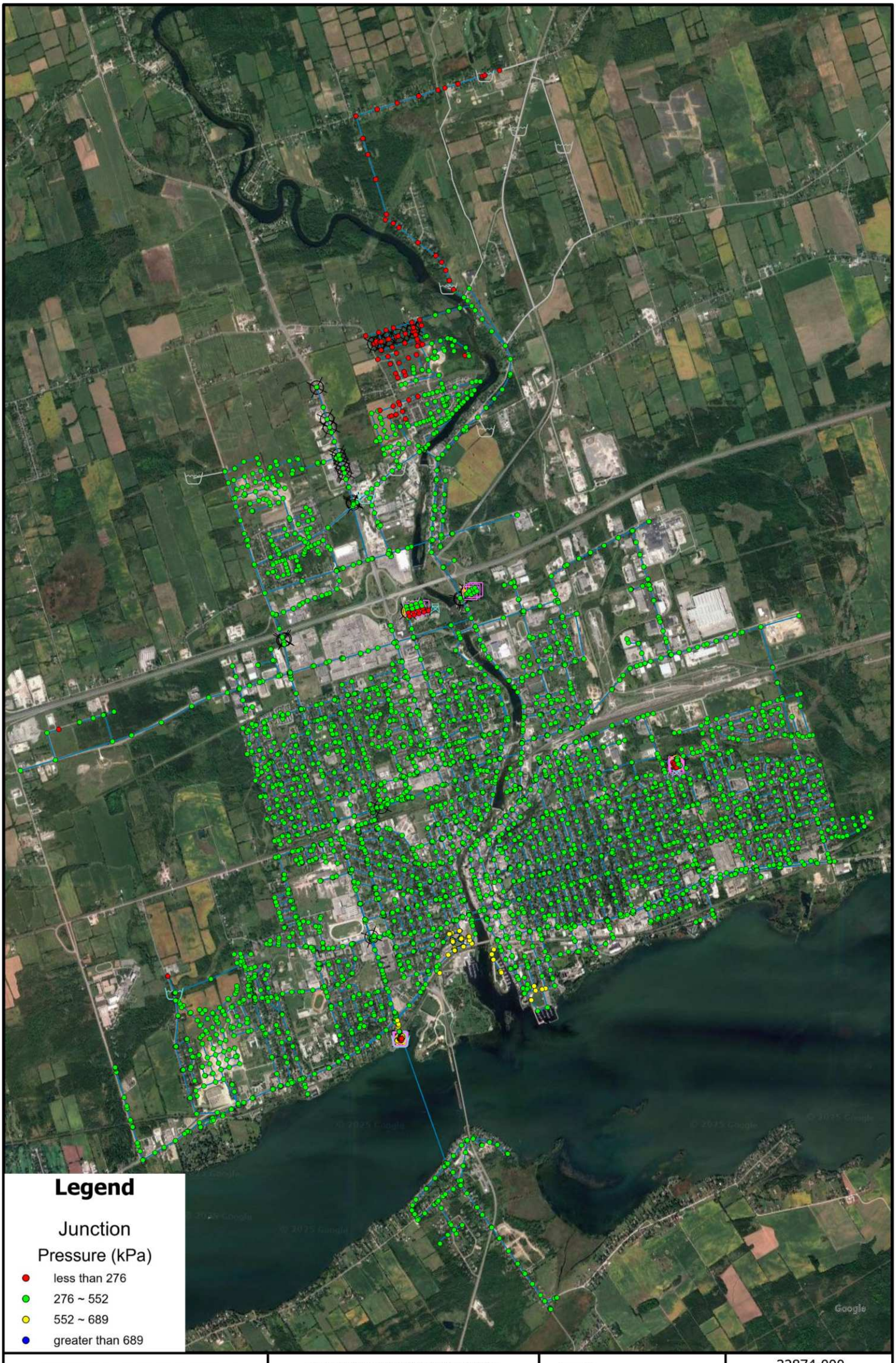
File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:21 AM

PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - UPGRADE OPTION 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-10

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:51 AM



PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - UPGRADE OPTION 2	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-11

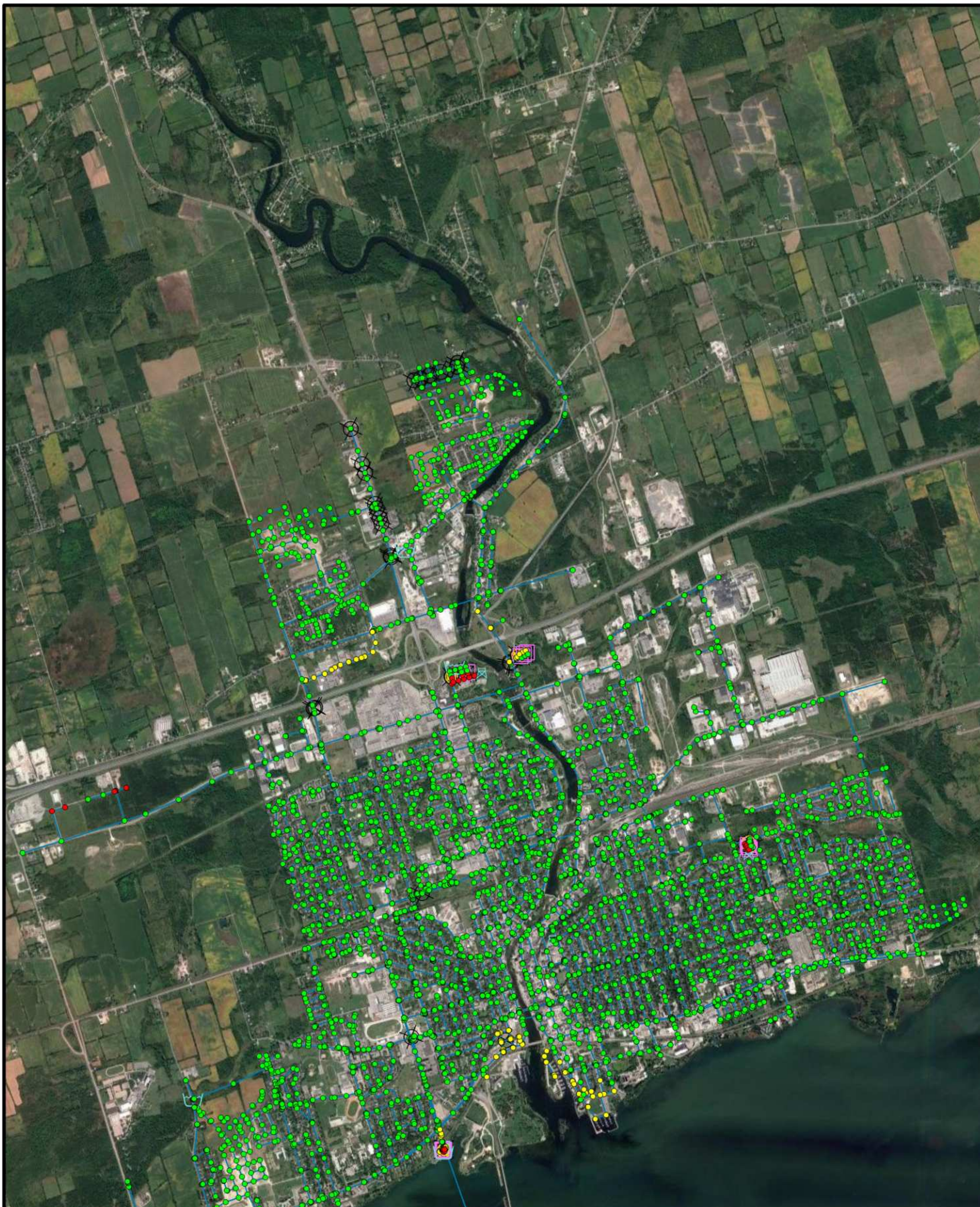
File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Monday, February 24, 2025 9:41 AM

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

PEAK HOUR DEMAND PRESSURE RESULTS - EXISTING CONDITIONS	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-12

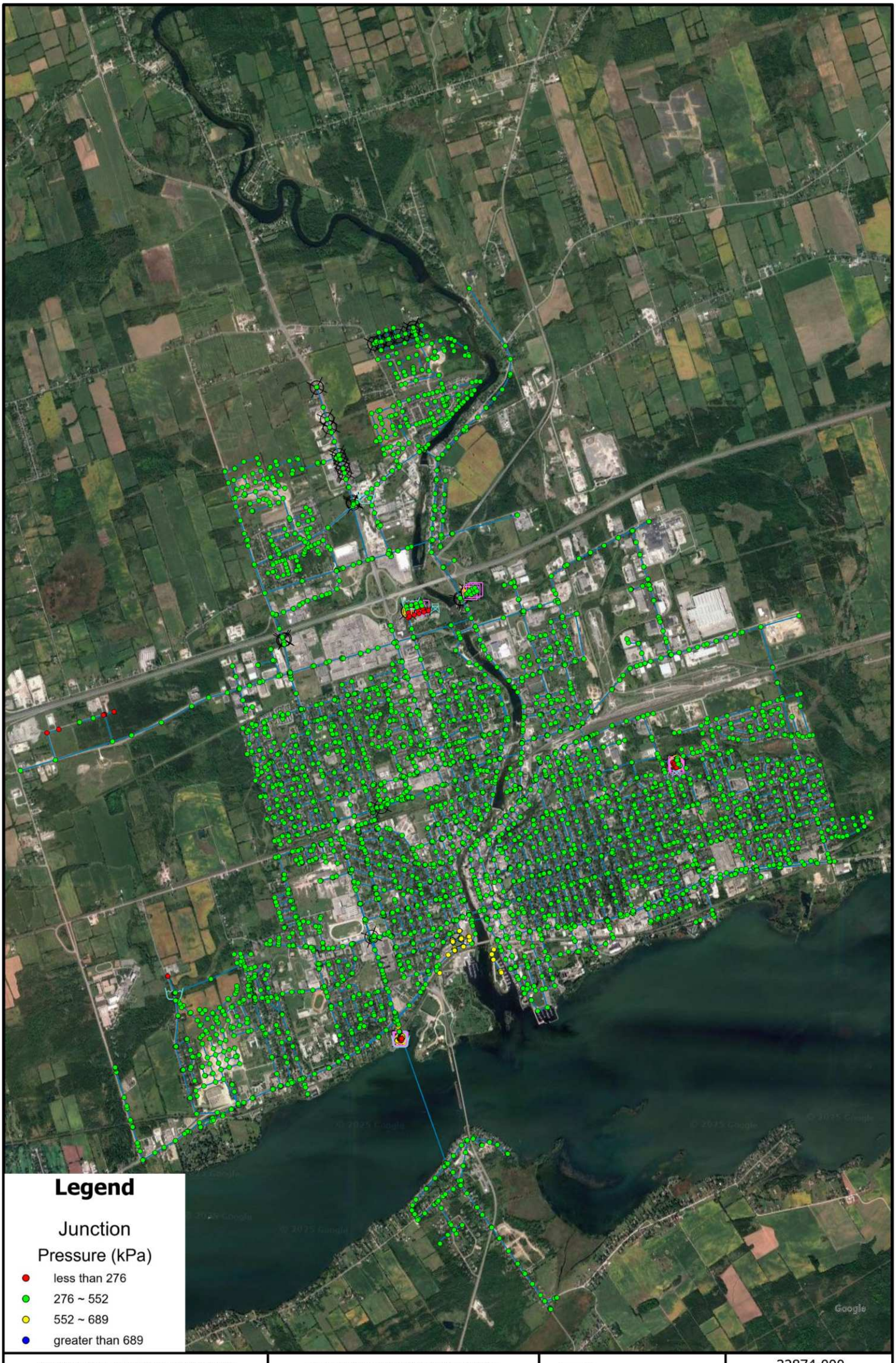
Plot Date: Monday, February 24, 2025 9:20 AM



File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

PEAK HOUR DEMAND PRESSURE RESULTS - SHORT-TERM GROWTH - SCENARIO 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-13

Plot Date: Friday, February 21, 2025 11:40 AM



File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

PEAK HOUR DEMAND PRESSURE RESULTS - MID-TERM GROWTH - SCENARIO 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-14

Plot Date: Friday, February 21, 2025 11:42 AM

Legend

Junction

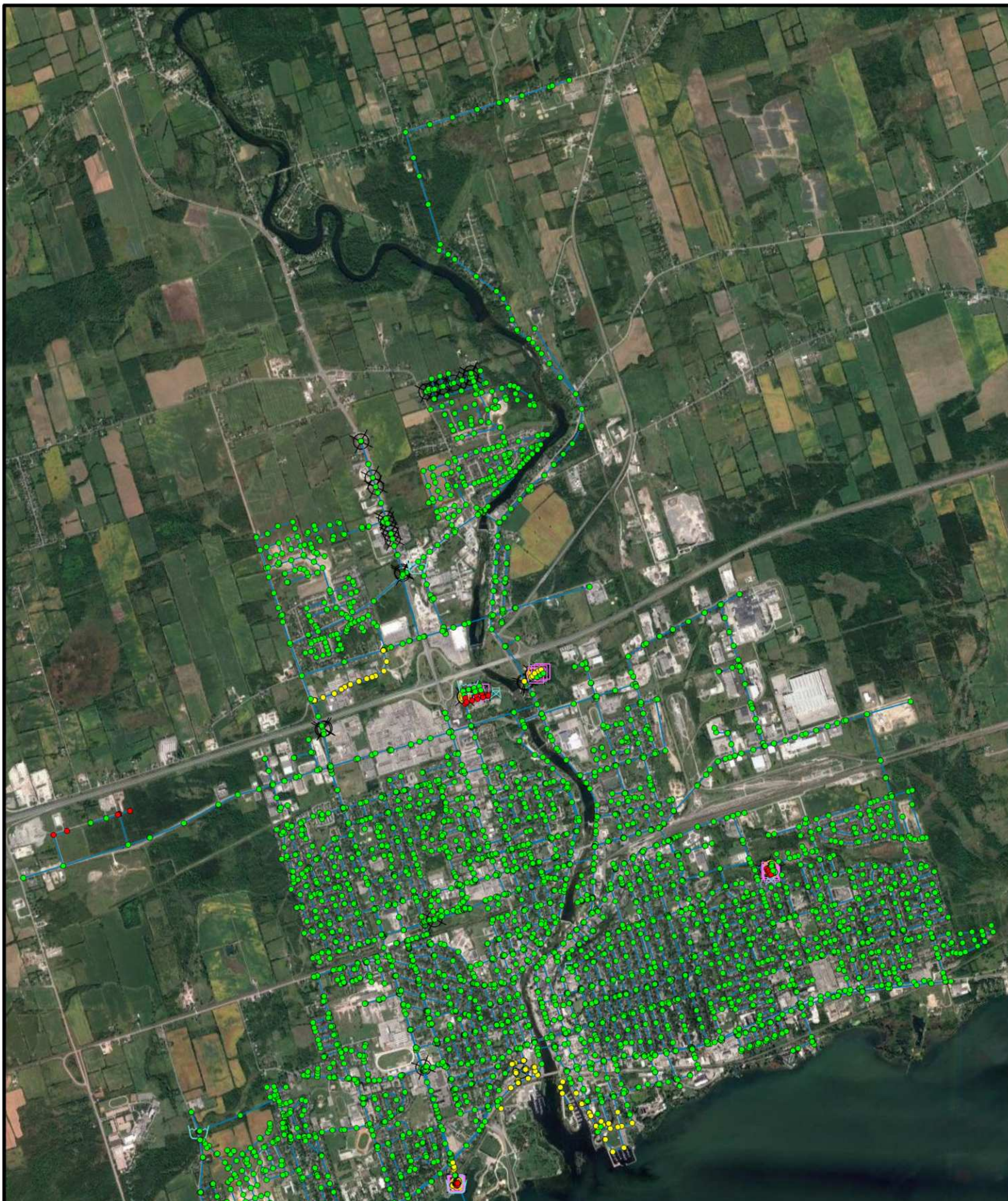
Pressure (kPa)

- less than 276
- 276 ~ 552
- 552 ~ 689
- greater than 689

PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - SCENARIO 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-15

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:43 AM



PEAK HOUR DEMAND PRESSURE RESULTS - SHORT-TERM GROWTH - SCENARIO 2	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-16

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:46 AM

PEAK HOUR DEMAND PRESSURE RESULTS - MID-TERM GROWTH - SCENARIO 2

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

32874-000

A-17

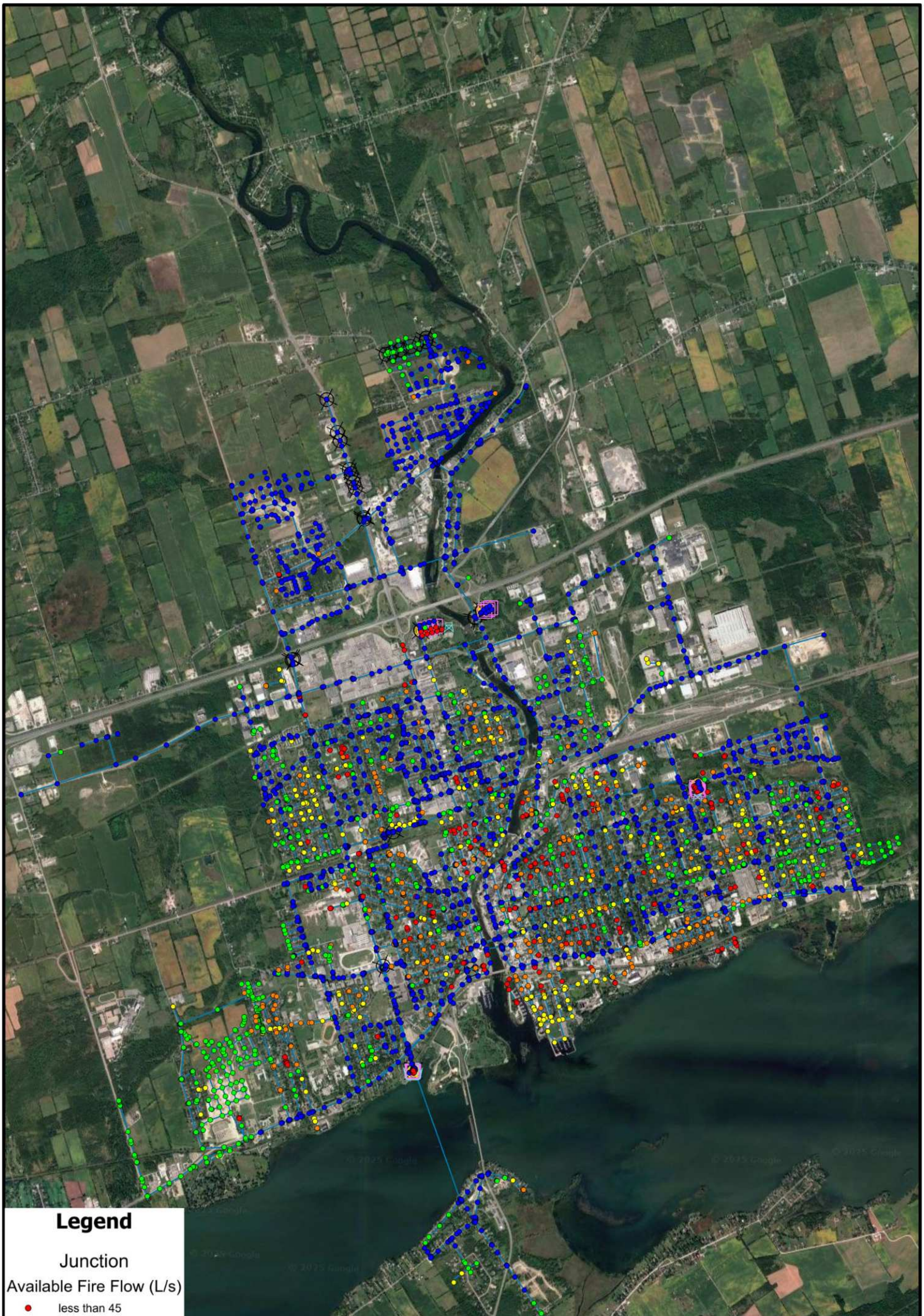
File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:47 AM

PEAK HOUR DEMAND PRESSURE RESULTS - LONG-TERM GROWTH - SCENARIO 2	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-18

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Friday, February 21, 2025 11:49 AM



Legend

Junction

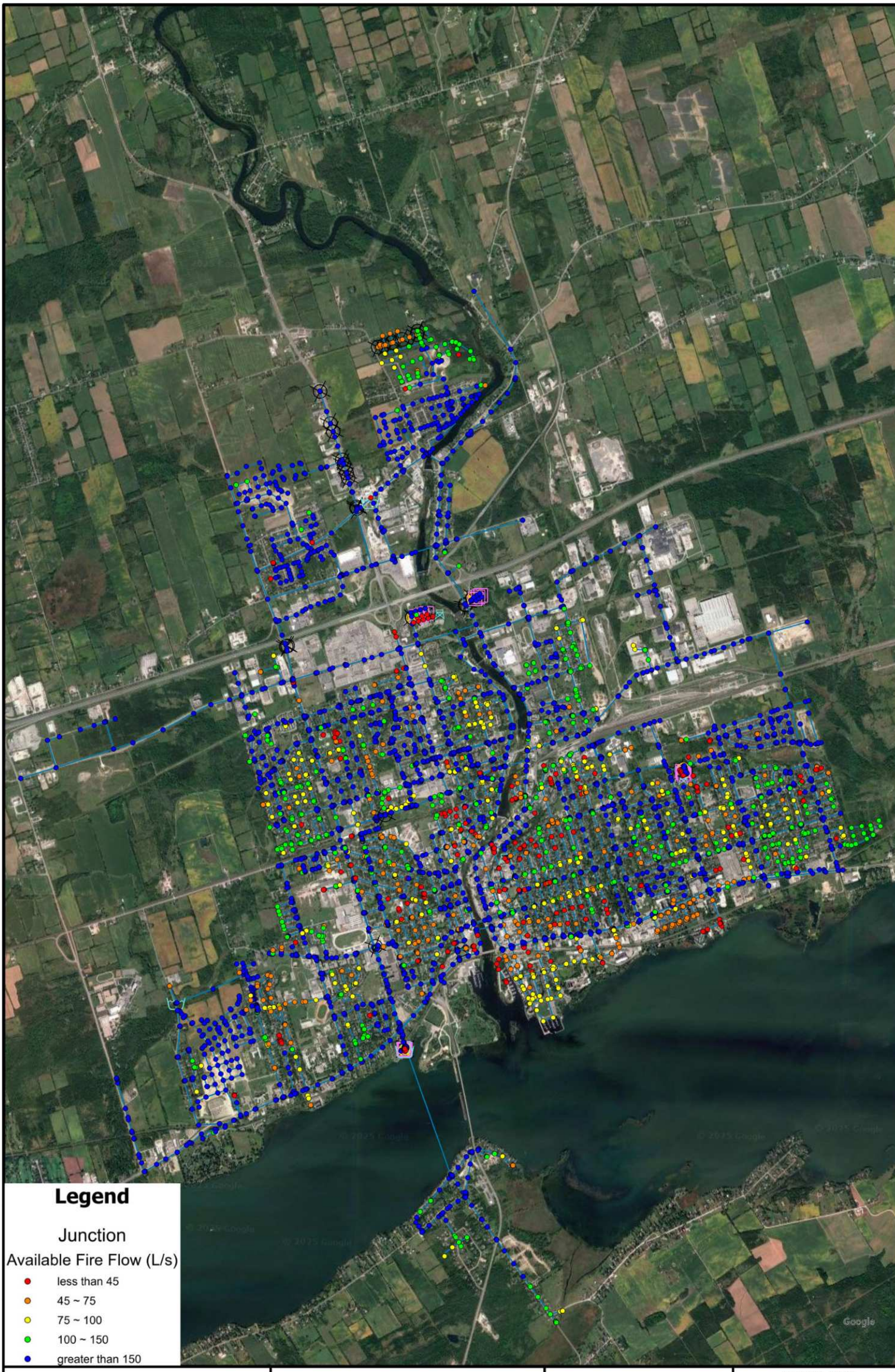
Available Fire Flow (L/s)

- less than 45
- 45 ~ 75
- 75 ~ 100
- 100 ~ 150
- greater than 150

MAXIMUM DAY PLUS FIRE FLOW RESULTS - EXISTING CONDITIONS	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-19

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

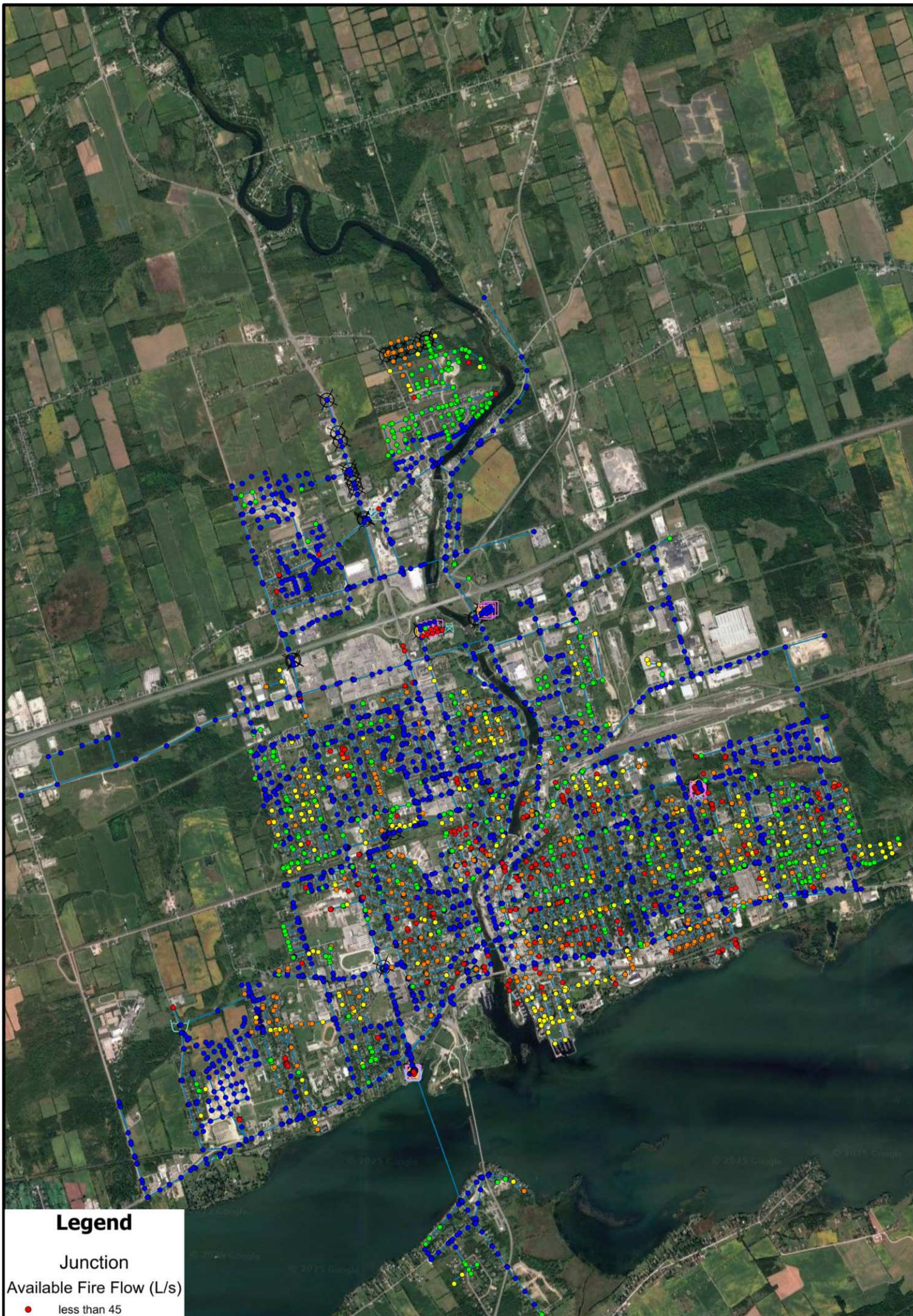
Plot Date: Friday, February 21, 2025 1:11 PM



MAXIMUM DAY PLUS FIRE FLOW RESULTS - SHORT-TERM GROWTH - SCENARIO 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-20

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

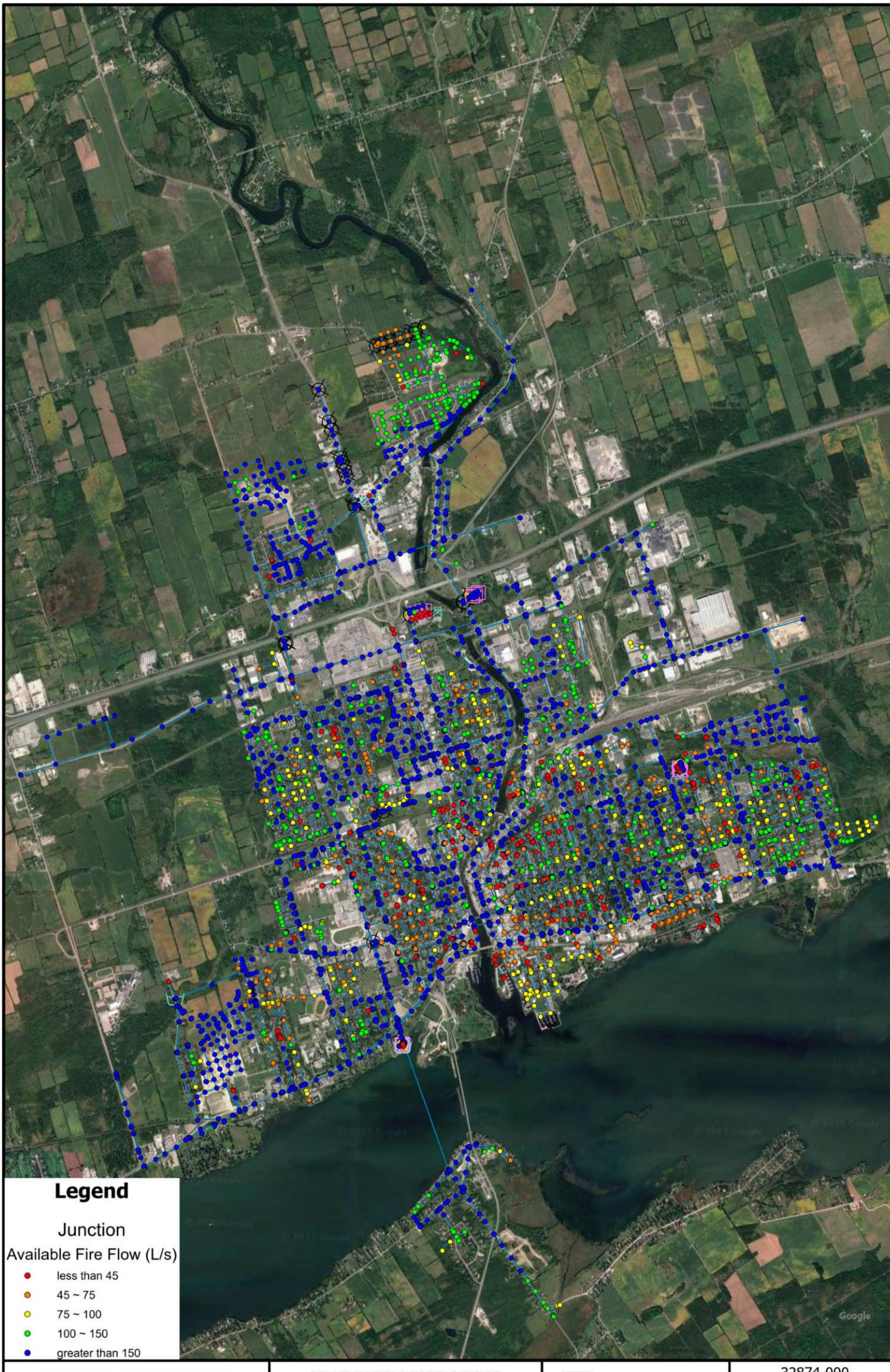
Plot Date: Tuesday, February 25, 2025 2:14 PM



File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Tuesday, February 25, 2025 2:15 PM

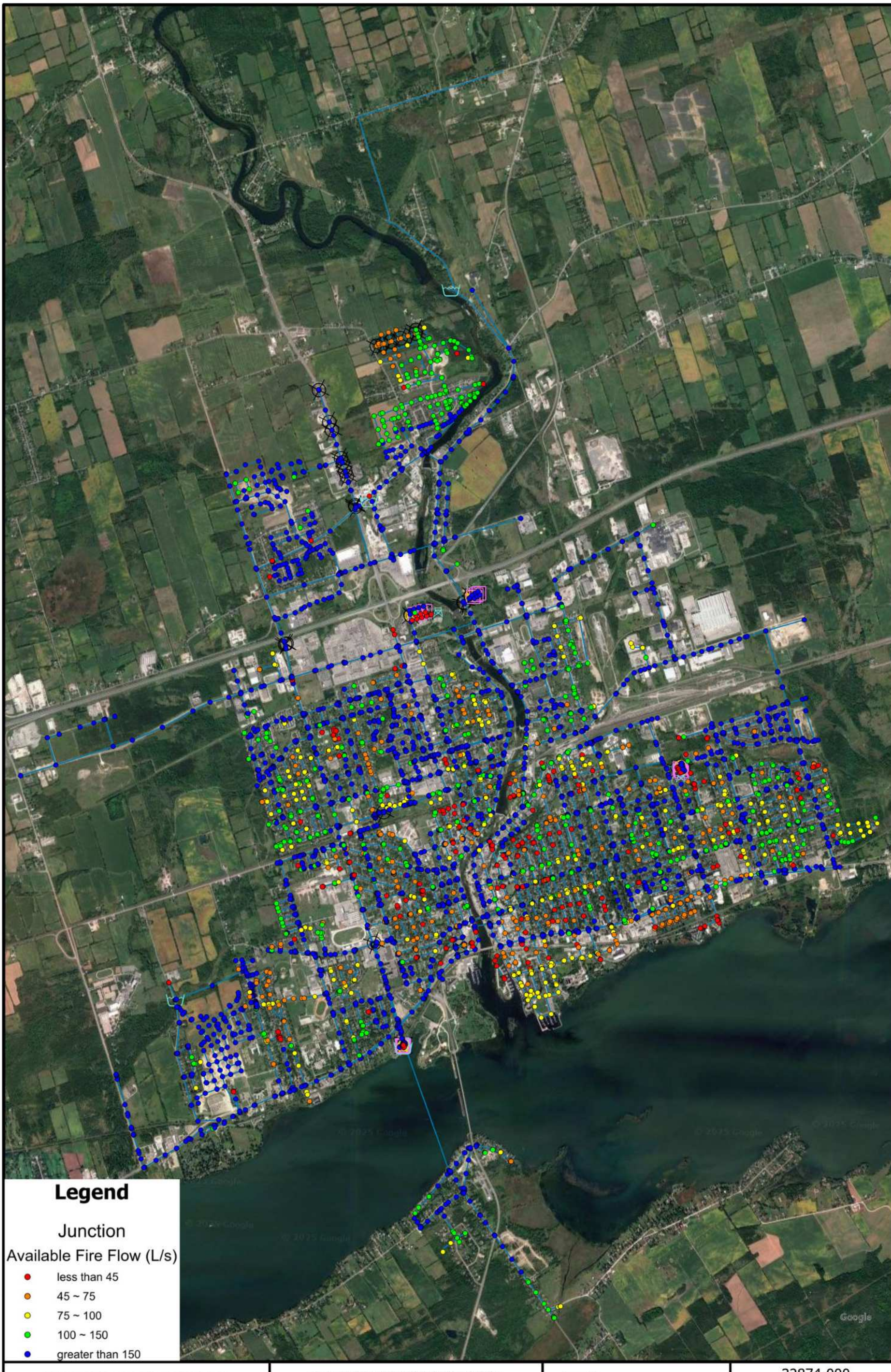
MAXIMUM DAY PLUS FIRE FLOW RESULTS - MID-TERM GROWTH - SCENARIO 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-21



MAXIMUM DAY PLUS FIRE FLOW RESULTS - LONG-TERM GROWTH - SCENARIO 1	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-22

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

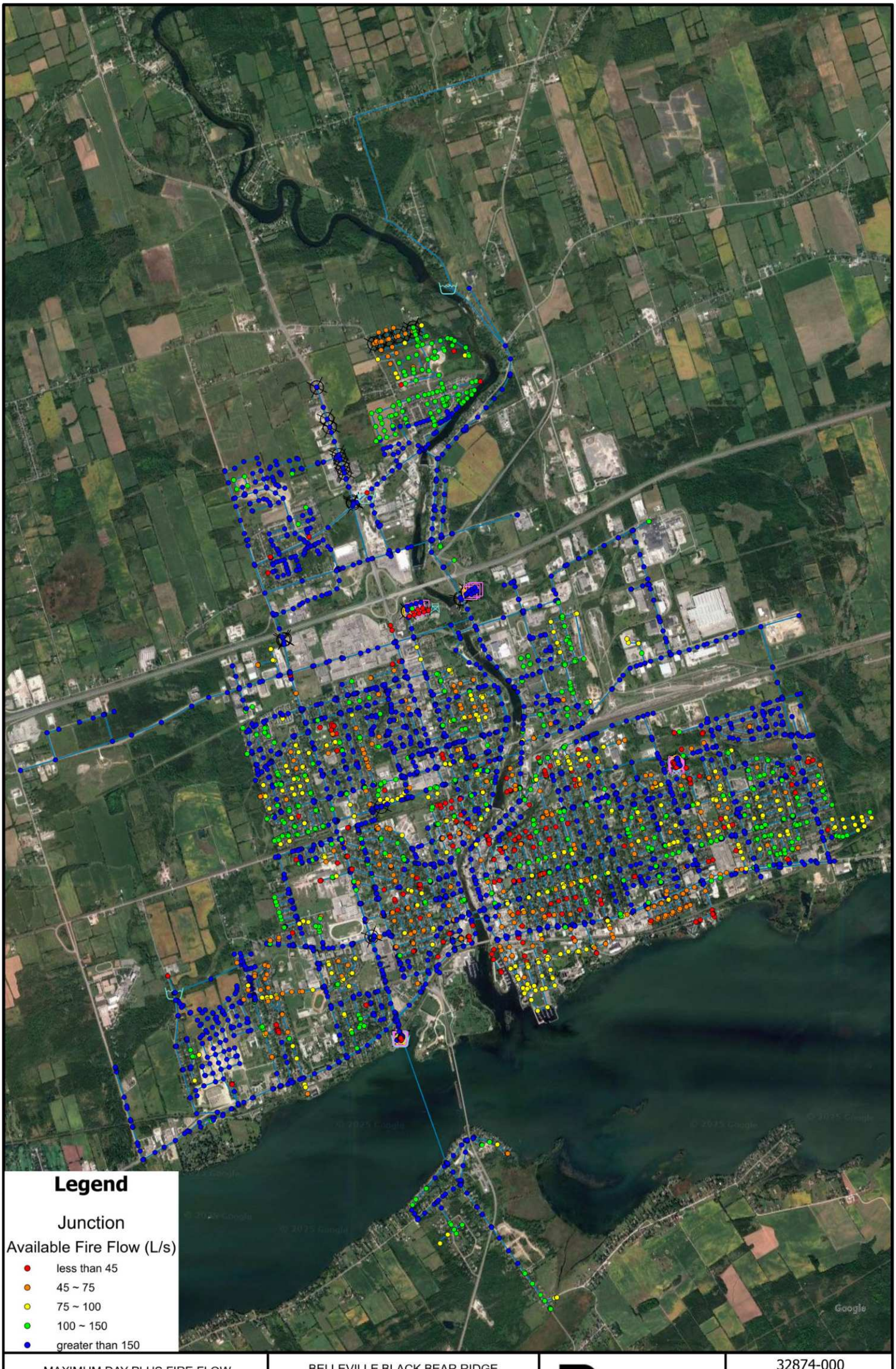
Plot Date: Tuesday, February 25, 2025 2:16 PM



MAXIMUM DAY PLUS FIRE FLOW RESULTS - SHORT-TERM GROWTH - SCENARIO 2	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-23

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Tuesday, February 25, 2025 2:18 PM



MAXIMUM DAY PLUS FIRE FLOW RESULTS - MID-TERM GROWTH - SCENARIO 2

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

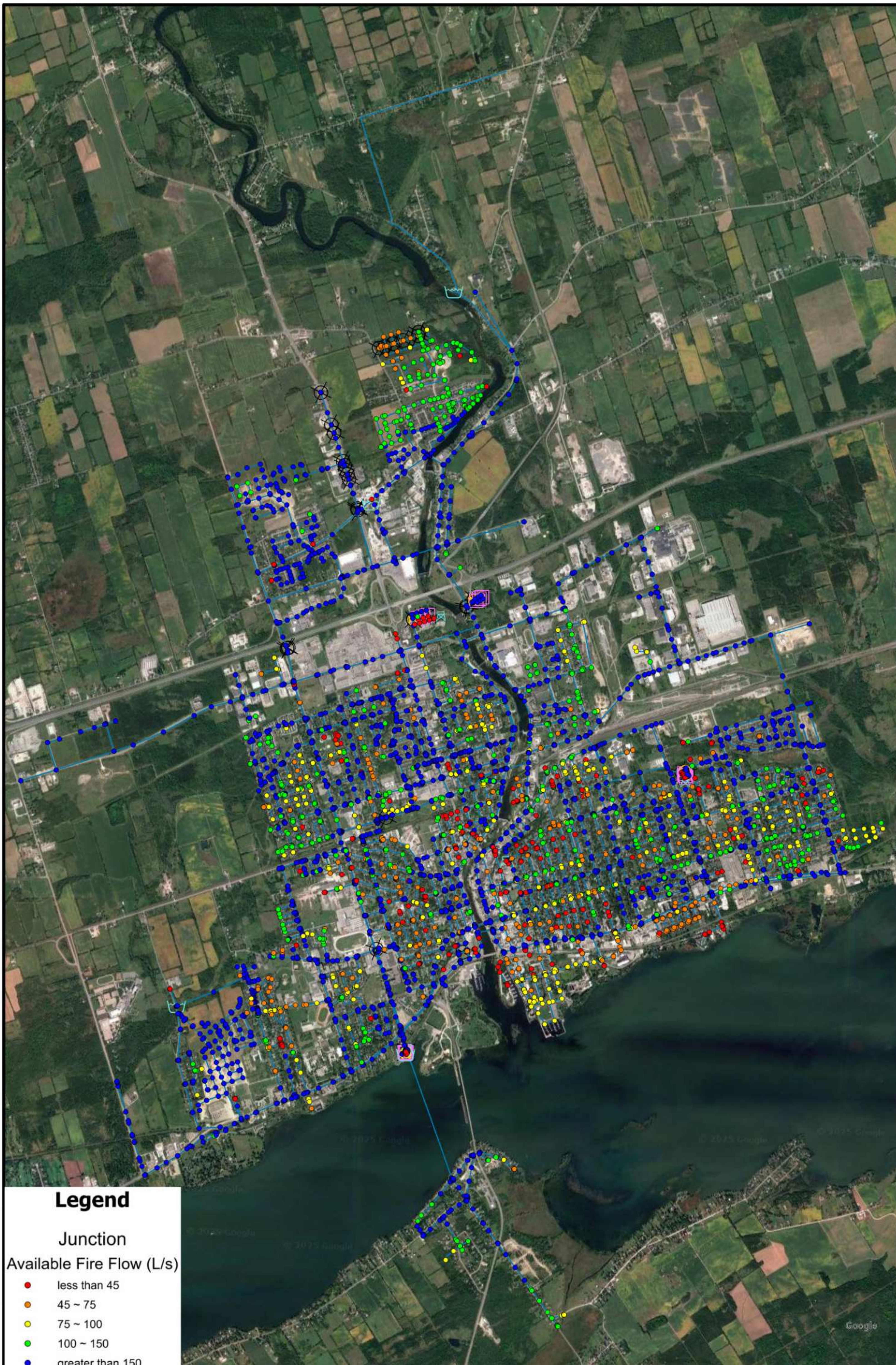
J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

32874-000

A-24

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

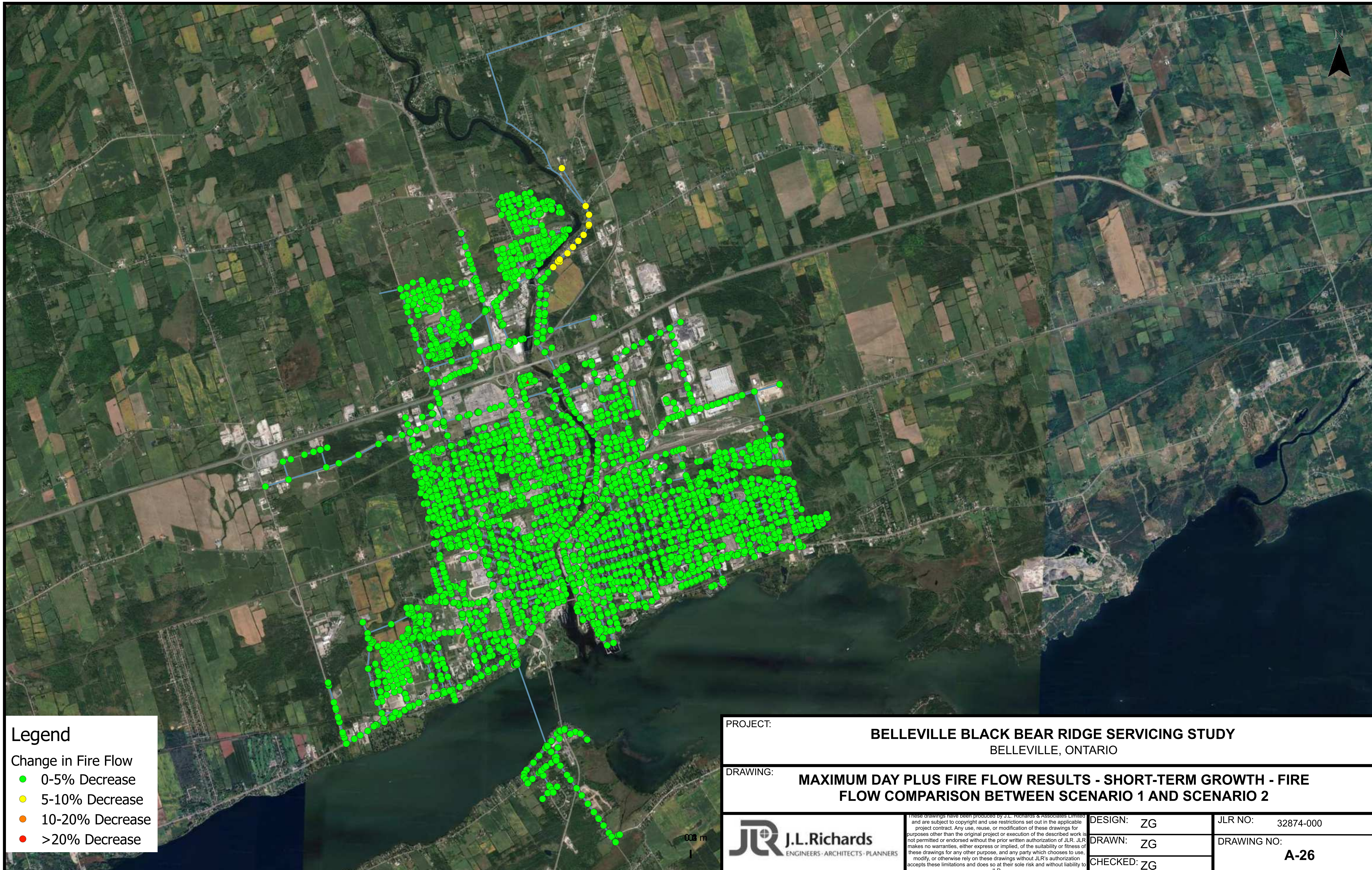
Plot Date: Tuesday, February 25, 2025 2:19 PM



MAXIMUM DAY PLUS FIRE FLOW RESULTS - LONG-TERM GROWTH - SCENARIO 2	BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY BELLEVILLE, ONTARIO	J.L.Richards ENGINEERS · ARCHITECTS · PLANNERS	32874-000 A-25

File Location: C:\Users\ZGeorgitsos\Documents\Projects\Belleville Black Bear Ridge\Belleville Water Model\Existing Model.aprx

Plot Date: Tuesday, February 25, 2025 2:20 PM



PROJECT:

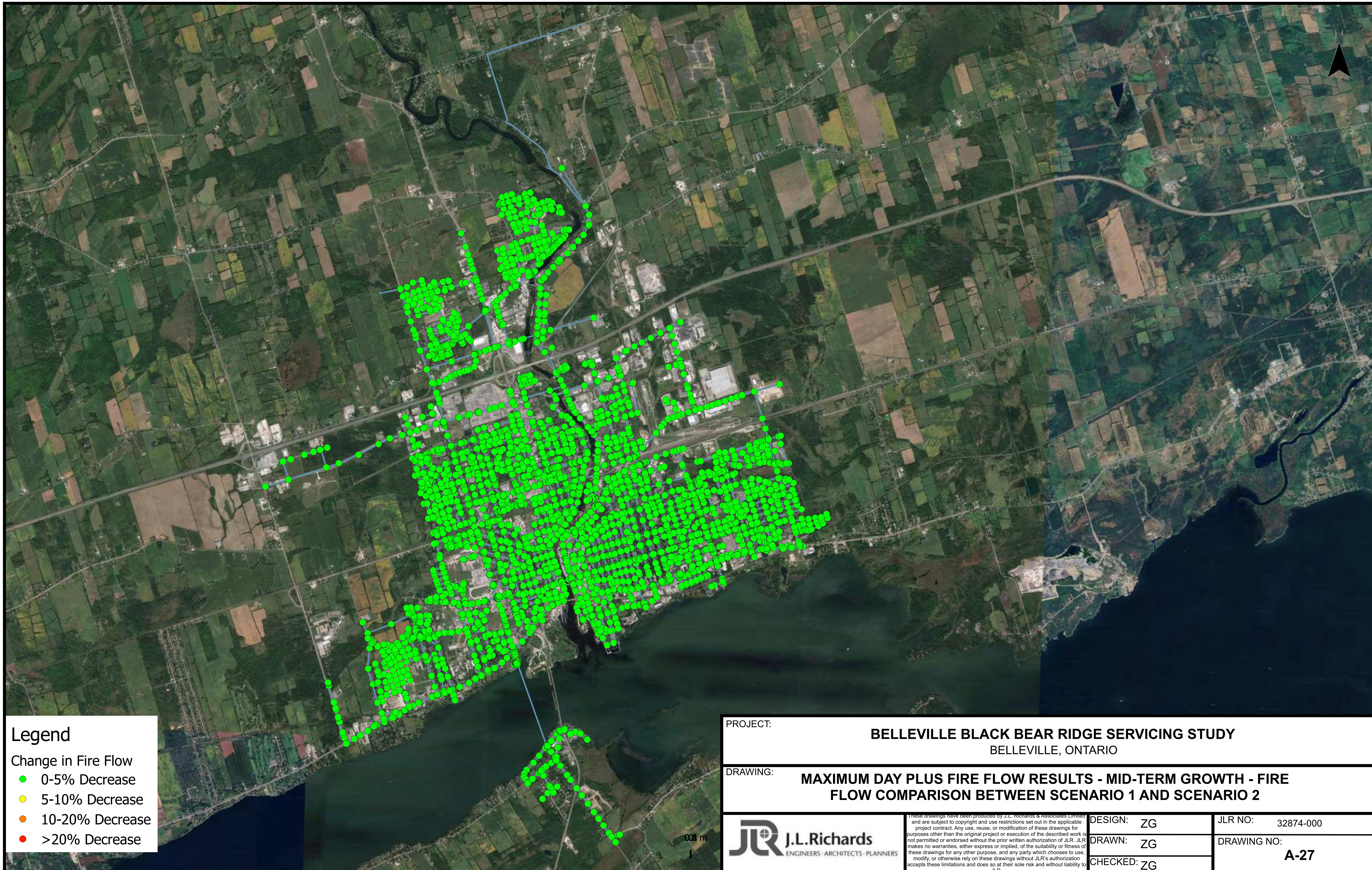
BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

DRAWING:

MAXIMUM DAY PLUS FIRE FLOW RESULTS - SHORT-TERM GROWTH - FIRE FLOW COMPARISON BETWEEN SCENARIO 1 AND SCENARIO 2

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

DESIGN:	ZG	JLR NO:	32874-000
DRAWN:	ZG	DRAWING NO:	A-26
CHECKED:	ZG		



PROJECT:

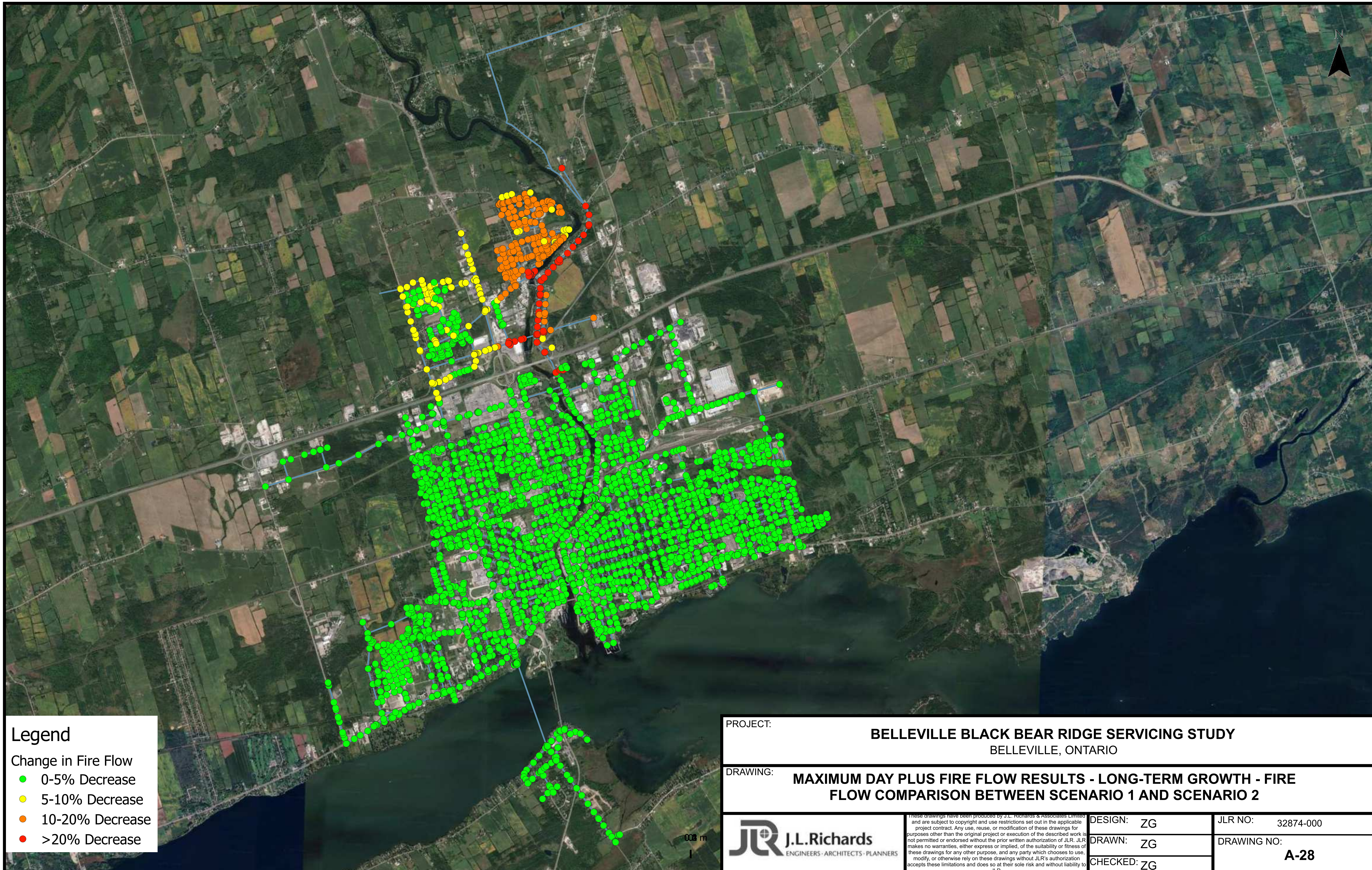
BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

DRAWING:

MAXIMUM DAY PLUS FIRE FLOW RESULTS - MID-TERM GROWTH - FIRE FLOW COMPARISON BETWEEN SCENARIO 1 AND SCENARIO 2

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

DESIGN:	ZG	JLR NO:	32874-000
DRAWN:	ZG	DRAWING NO:	A-27
CHECKED:	ZG		



PROJECT:

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY

BELLEVILLE, ONTARIO

DRAWING:

MAXIMUM DAY PLUS FIRE FLOW RESULTS - LONG-TERM GROWTH - FIRE FLOW COMPARISON BETWEEN SCENARIO 1 AND SCENARIO 2

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

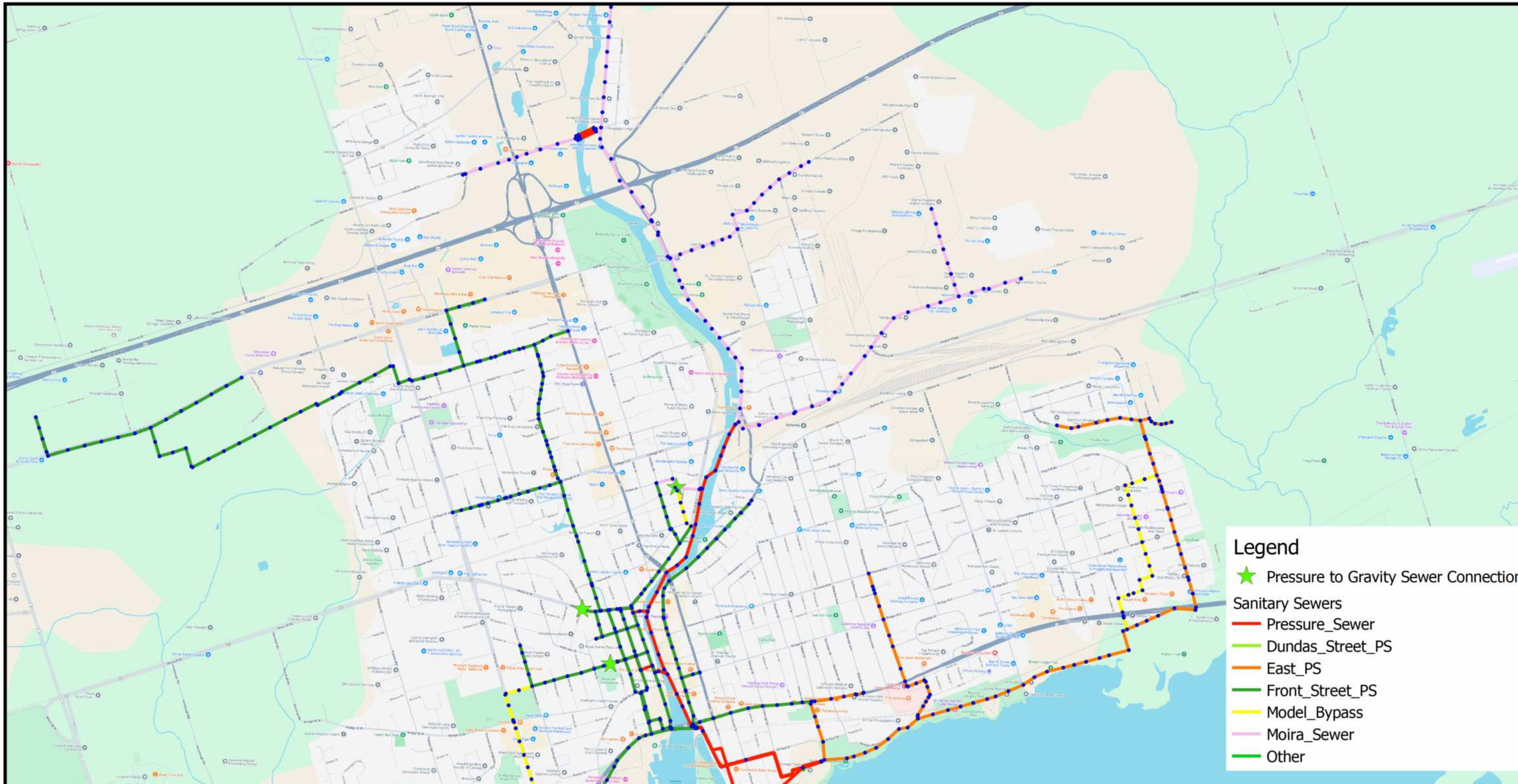
DESIGN: ZG
DRAWN: ZG
CHECKED: ZG

JLR NO: 32874-000

DRAWING NO: **A-28**

Appendix B

Sanitary Model Inputs and Results



PROJECT:

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

DRAWING:

GRAVITY SEWER TO PRESSURE SEWER CONNECTIONS

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

DESIGN:	ZG
DRAWN:	ZG
CHECKED:	ZG
JLR NO:	32874-000
DRAWING NO:	**Figure B-1**

Figure B-2	Scenario 1 - HGL Profile - Dry Weather Flow

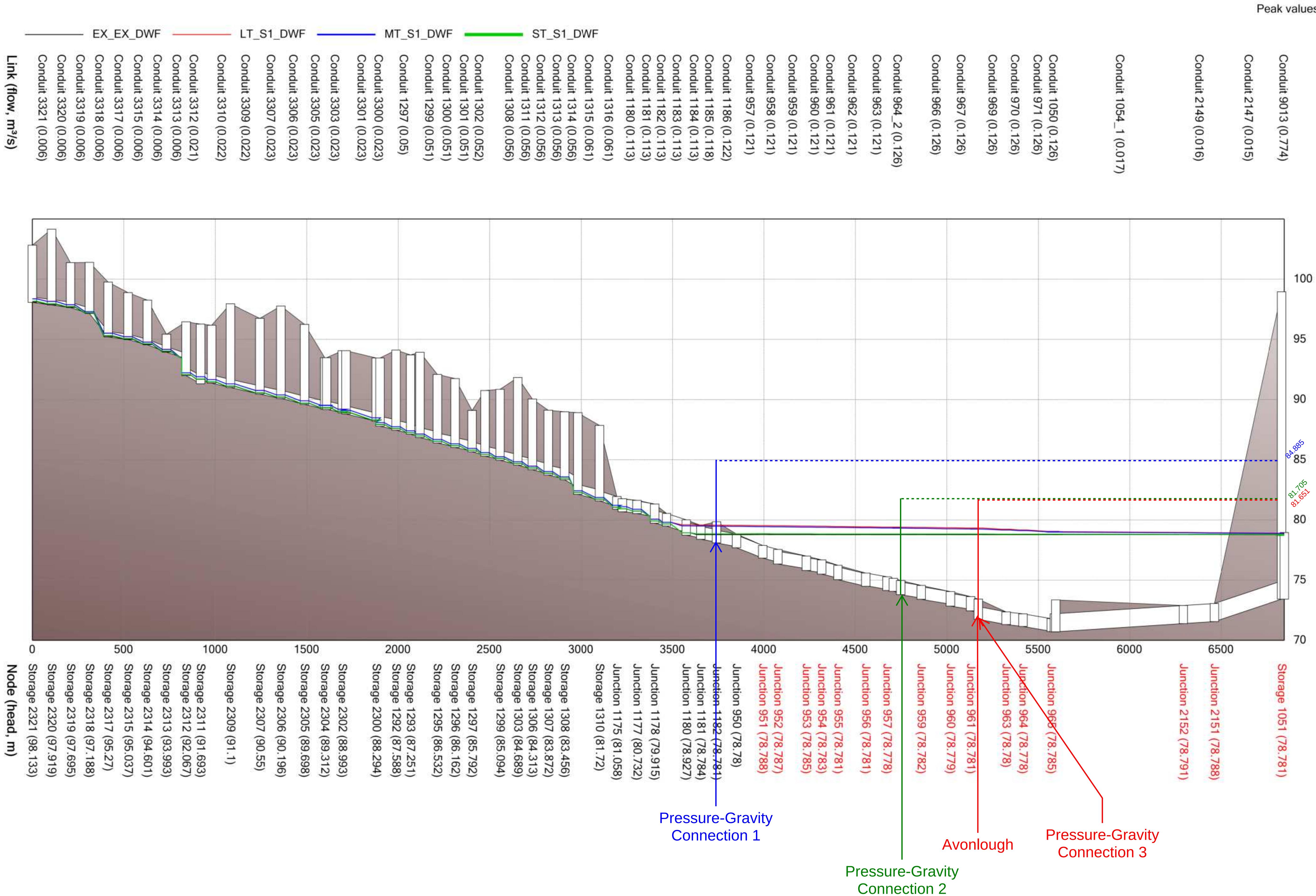


Figure B-3	Scenario 1 - HGL Profile - 1:10-Year Storm Event

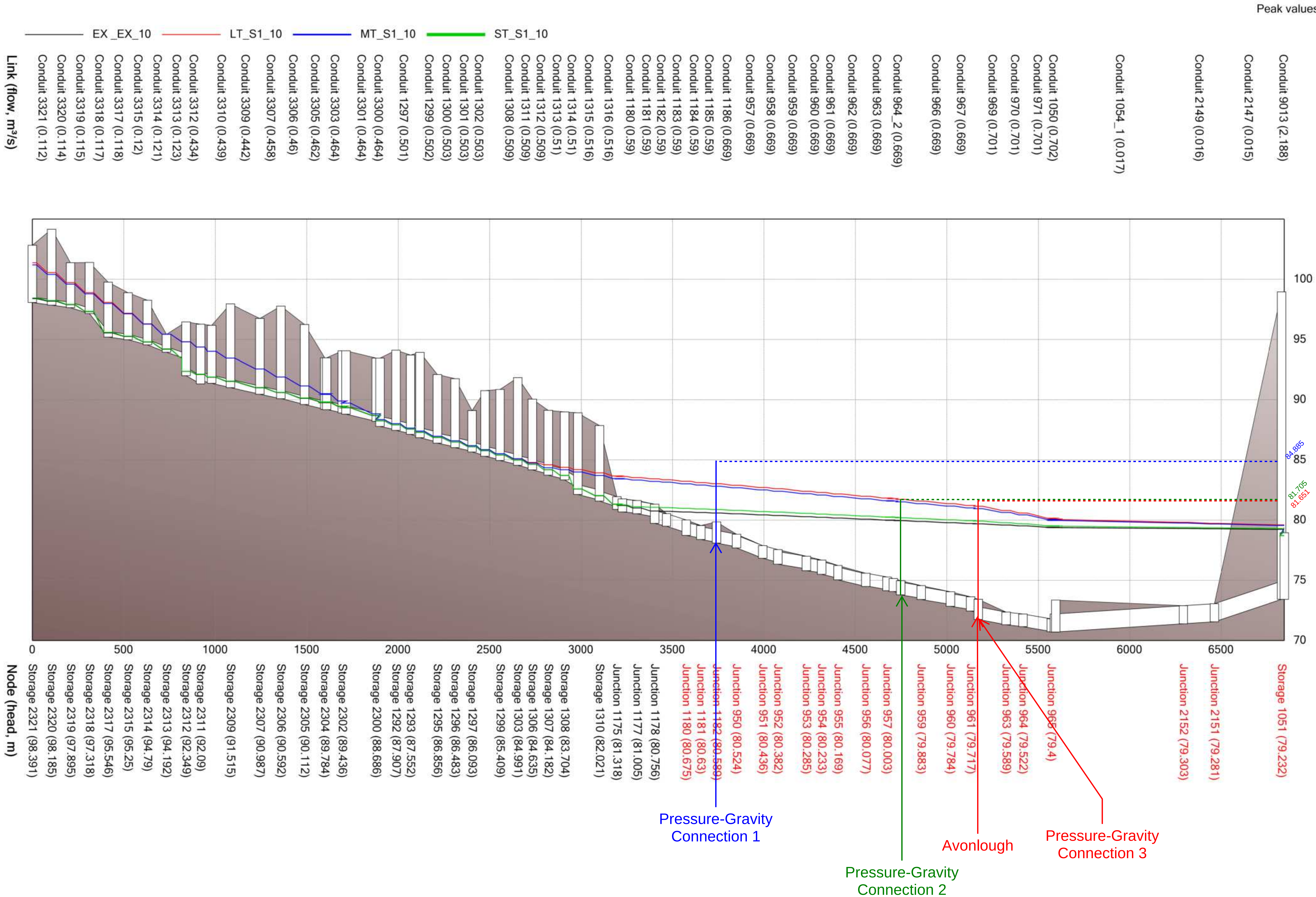


Figure B-4	Scenario 2A - HGL Profile - Dry Weather Flow

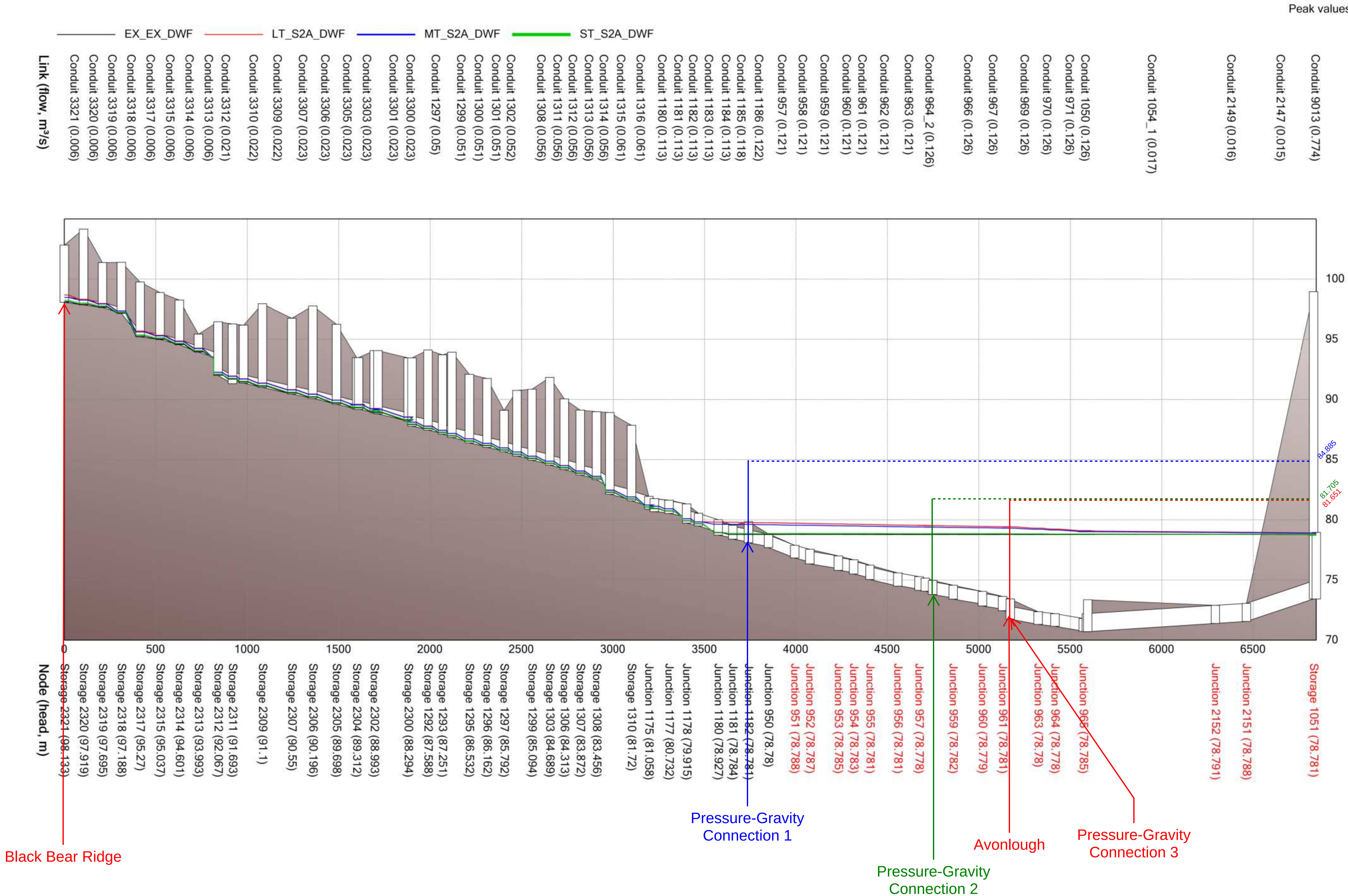


Figure B-5	Scenario 2A - HGL Profile - 1:10-Year Storm Event

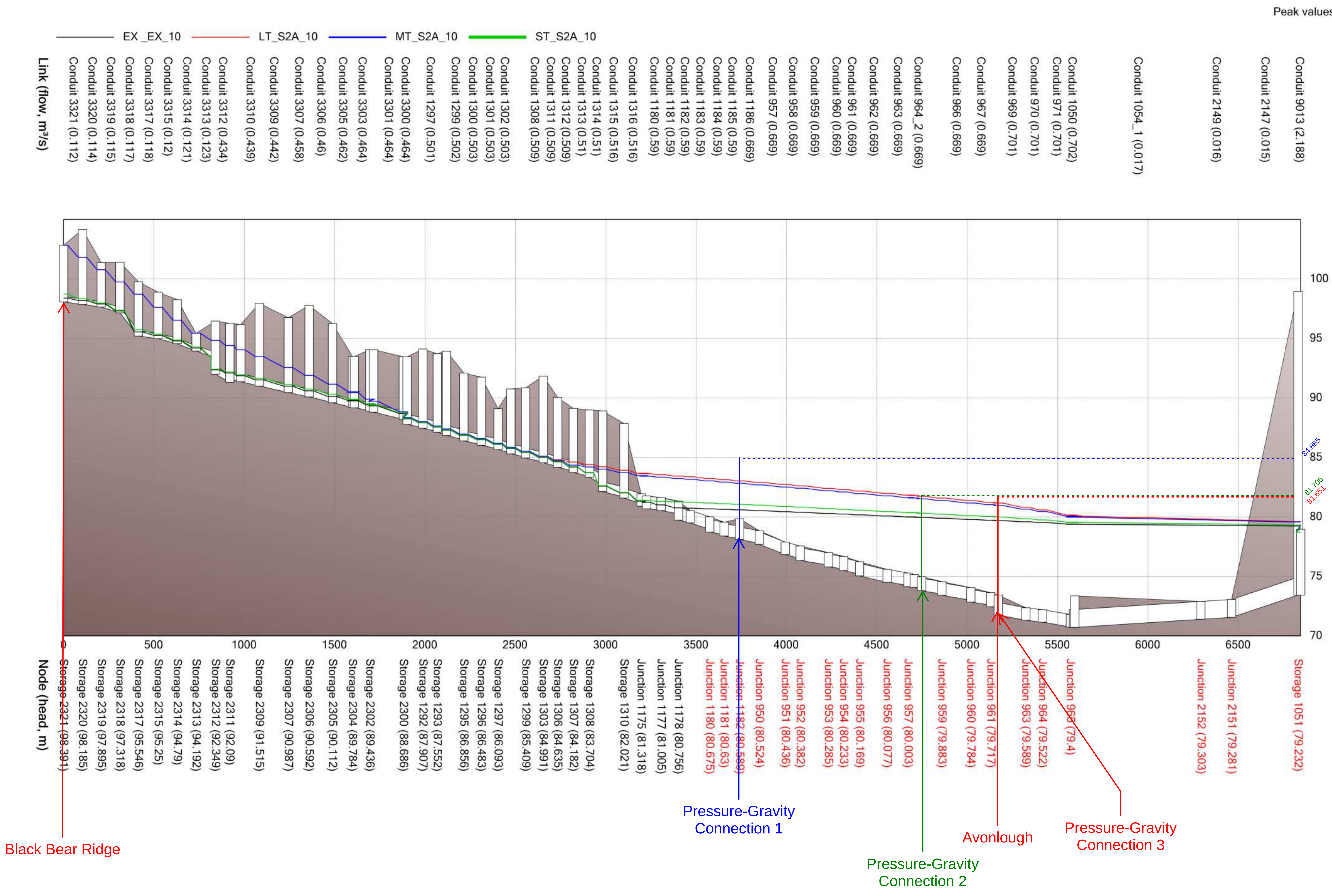


Figure B-6	Scenario 2B - HGL Profile - Dry Weather Flow

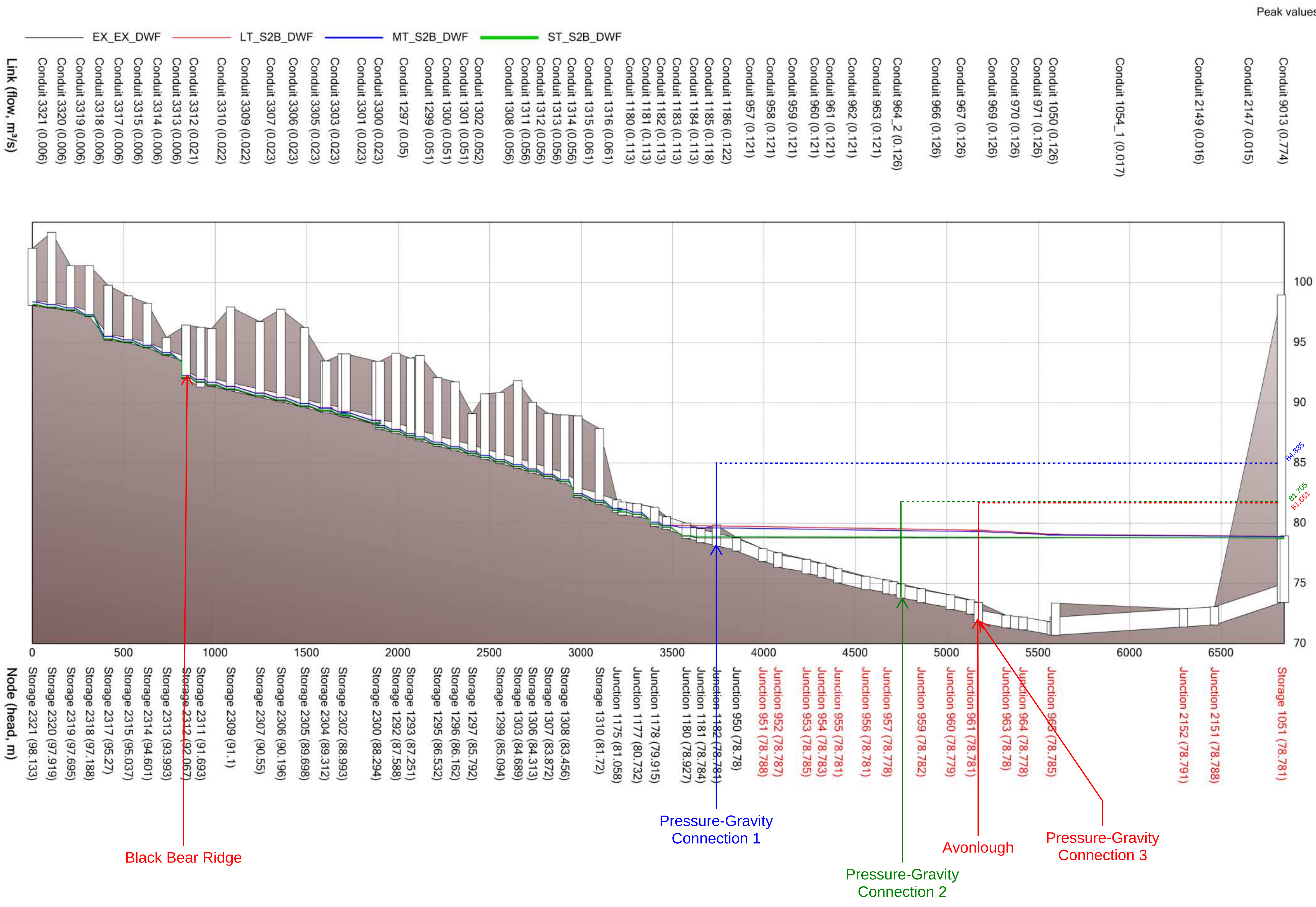


Figure B-7 | Scenario 2B - HGL Profile - 1:10-Year Storm Event

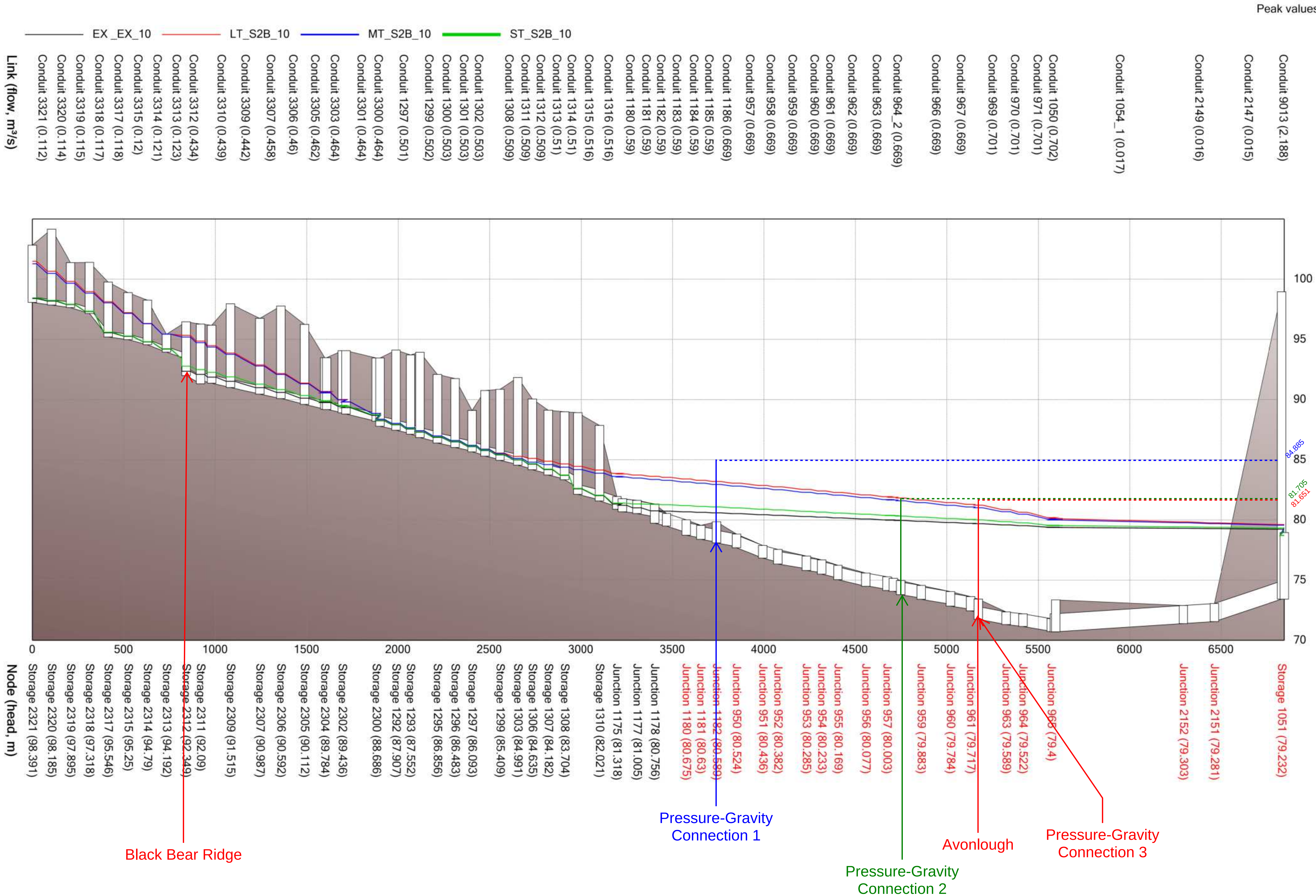


Figure B-8	Scenario 3 - HGL Profile - Dry Weather Flow

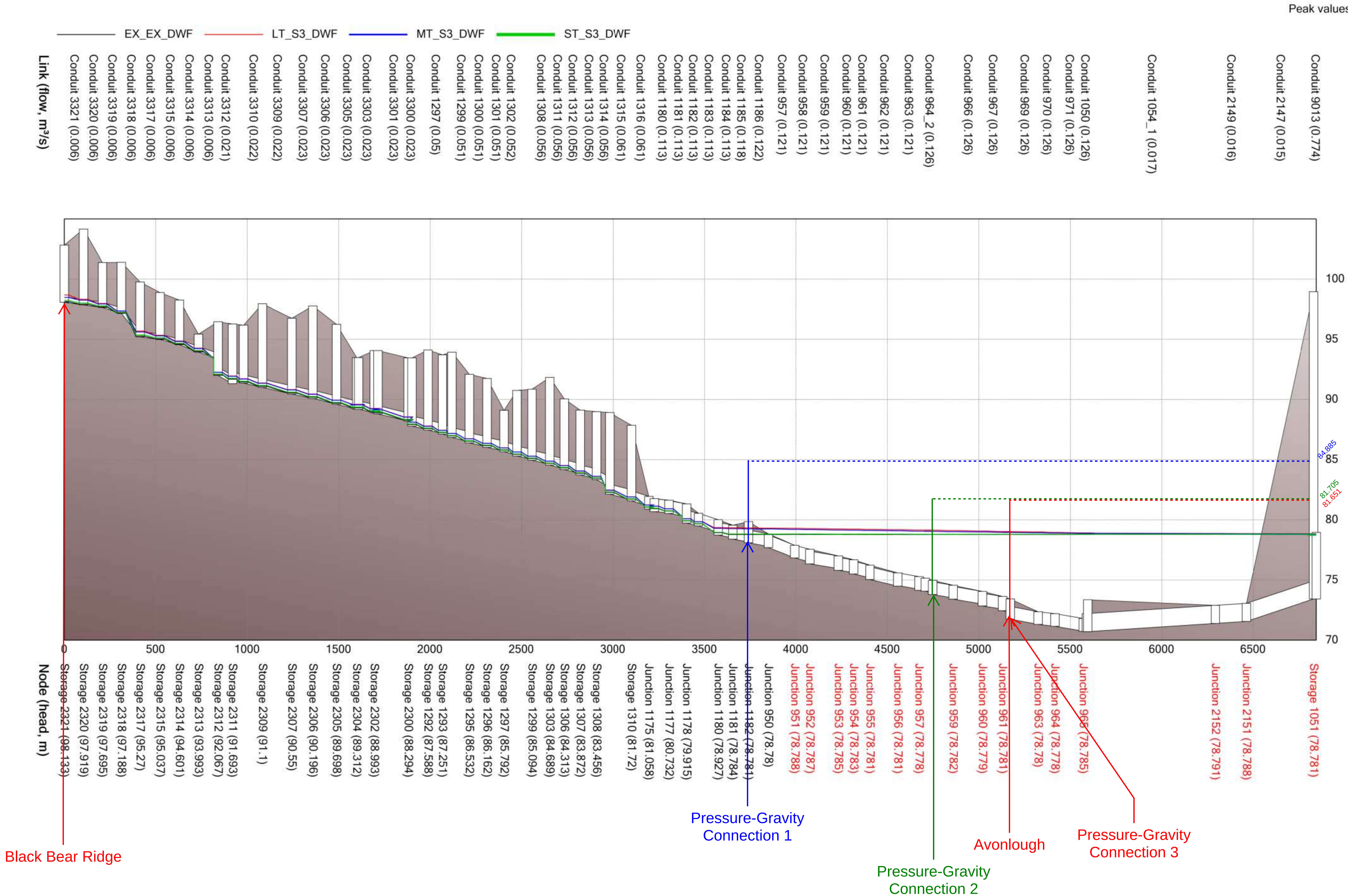
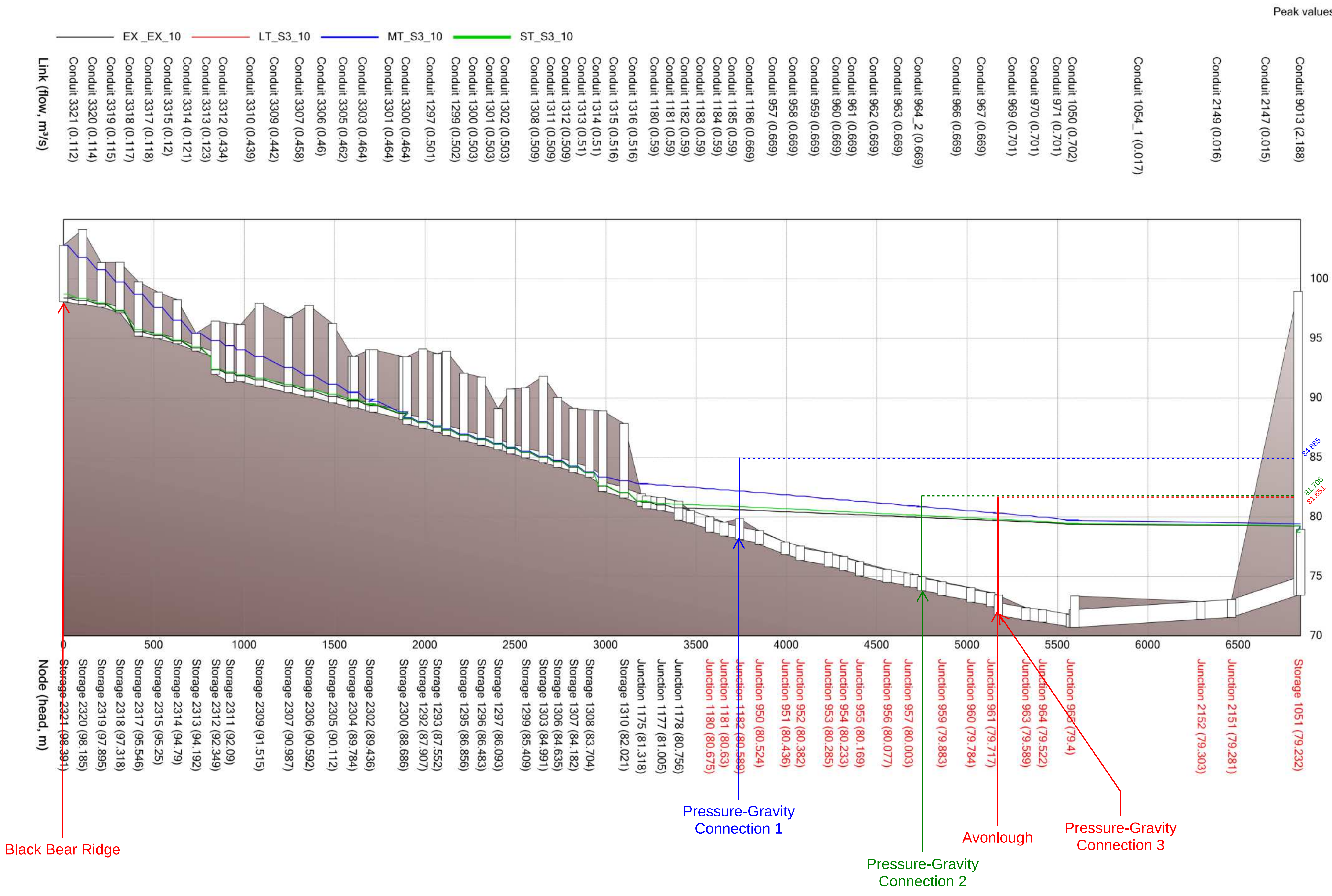
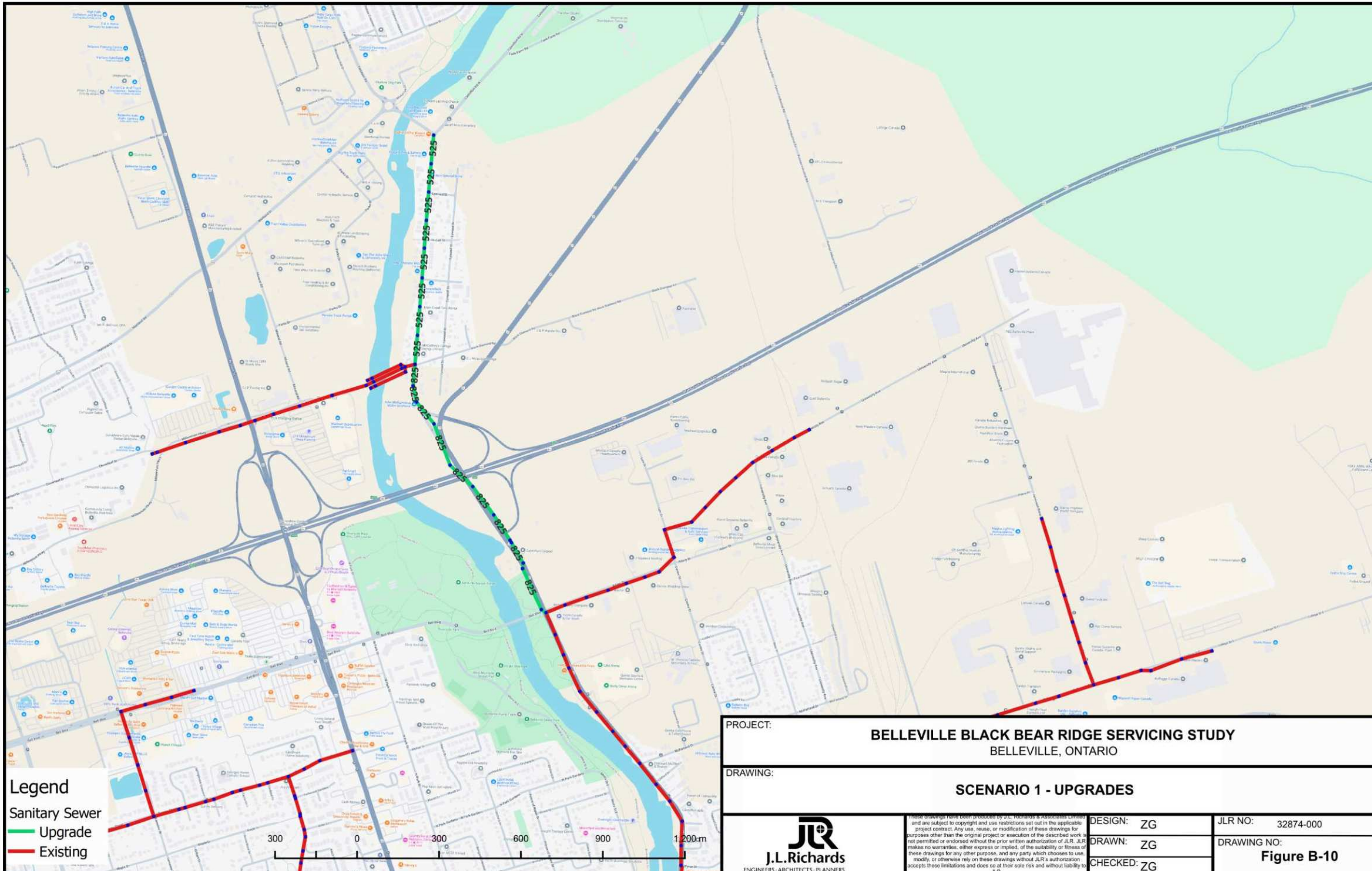


Figure B-9	Scenario 3 - HGL Profile - 1:10-Year Storm Event



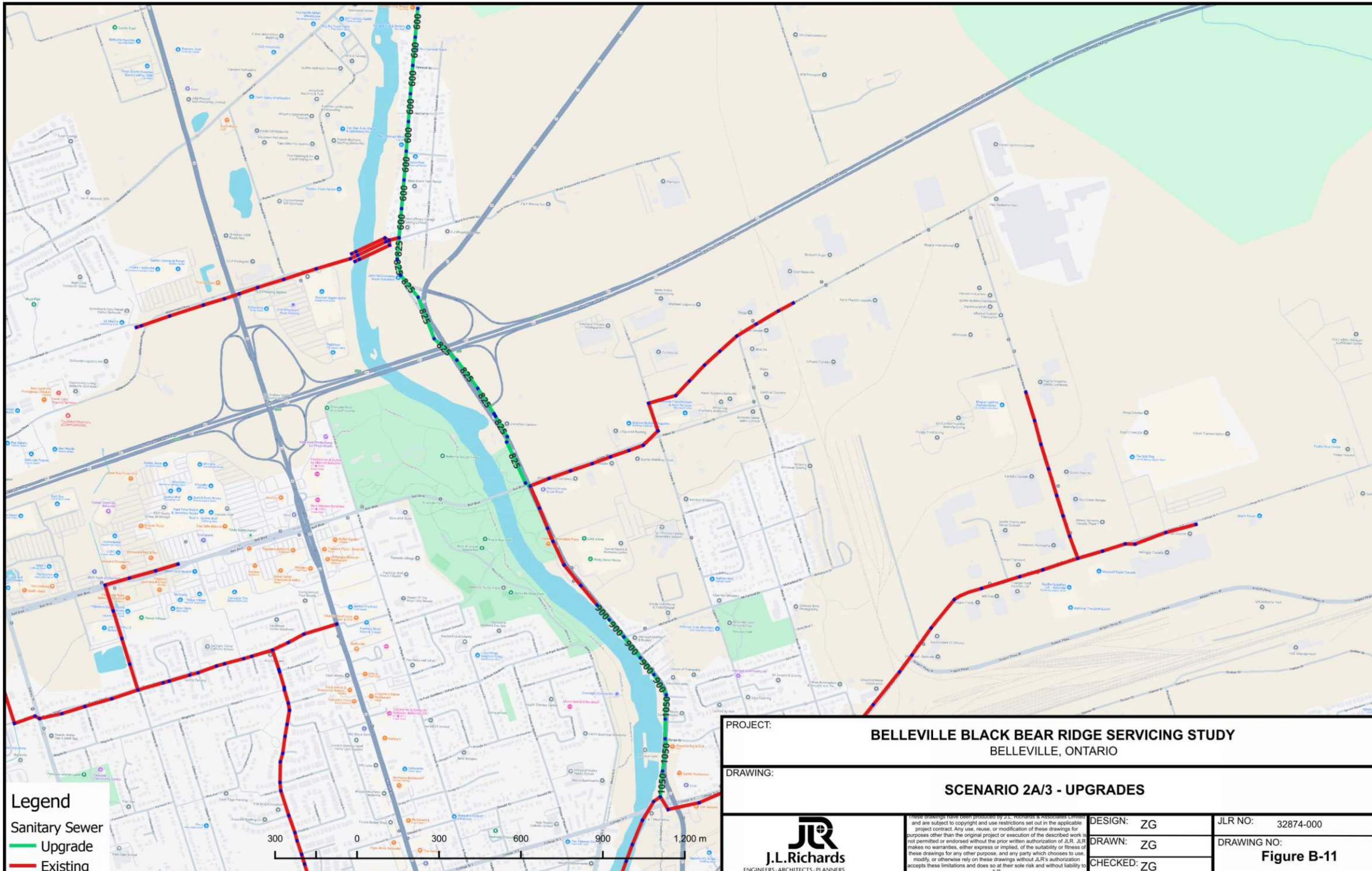


PROJECT:
BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO

DRAWING:
SCENARIO 1 - UPGRADES

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

DESIGN:	ZG	JLR NO:	32874-000
DRAWN:	ZG	DRAWING NO:	**Figure B-10**
CHECKED:	ZG		



PROJECT:

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY

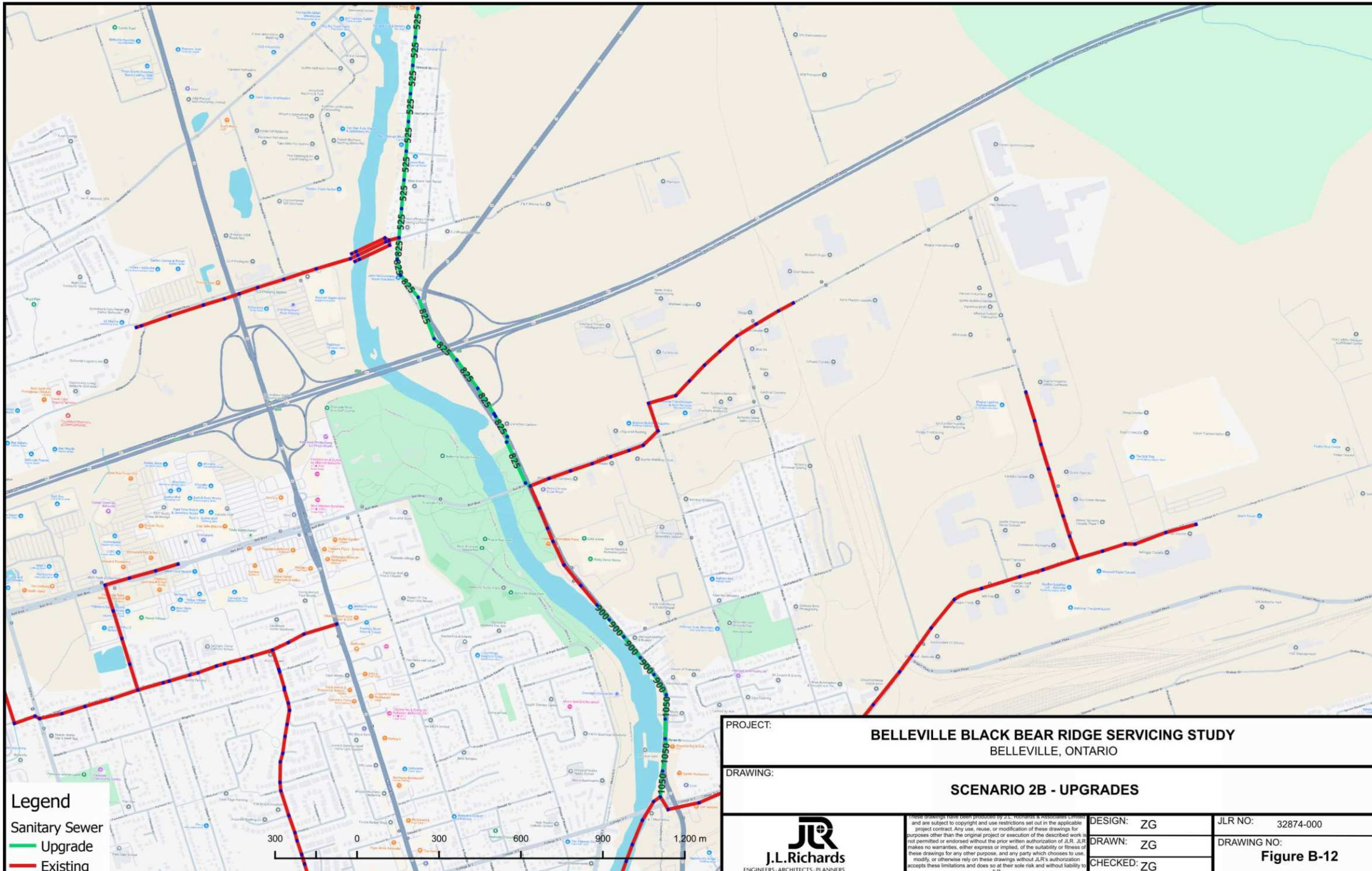
BELLEVILLE, ONTARIO

DRAWING:

SCENARIO 2A/3 - UPGRADES

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

DESIGN:	ZG
DRAWN:	ZG
CHECKED:	ZG
JLR NO:	32874-000
DRAWING NO:	**Figure B-11**



PROJECT:

BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY

BELLEVILLE, ONTARIO

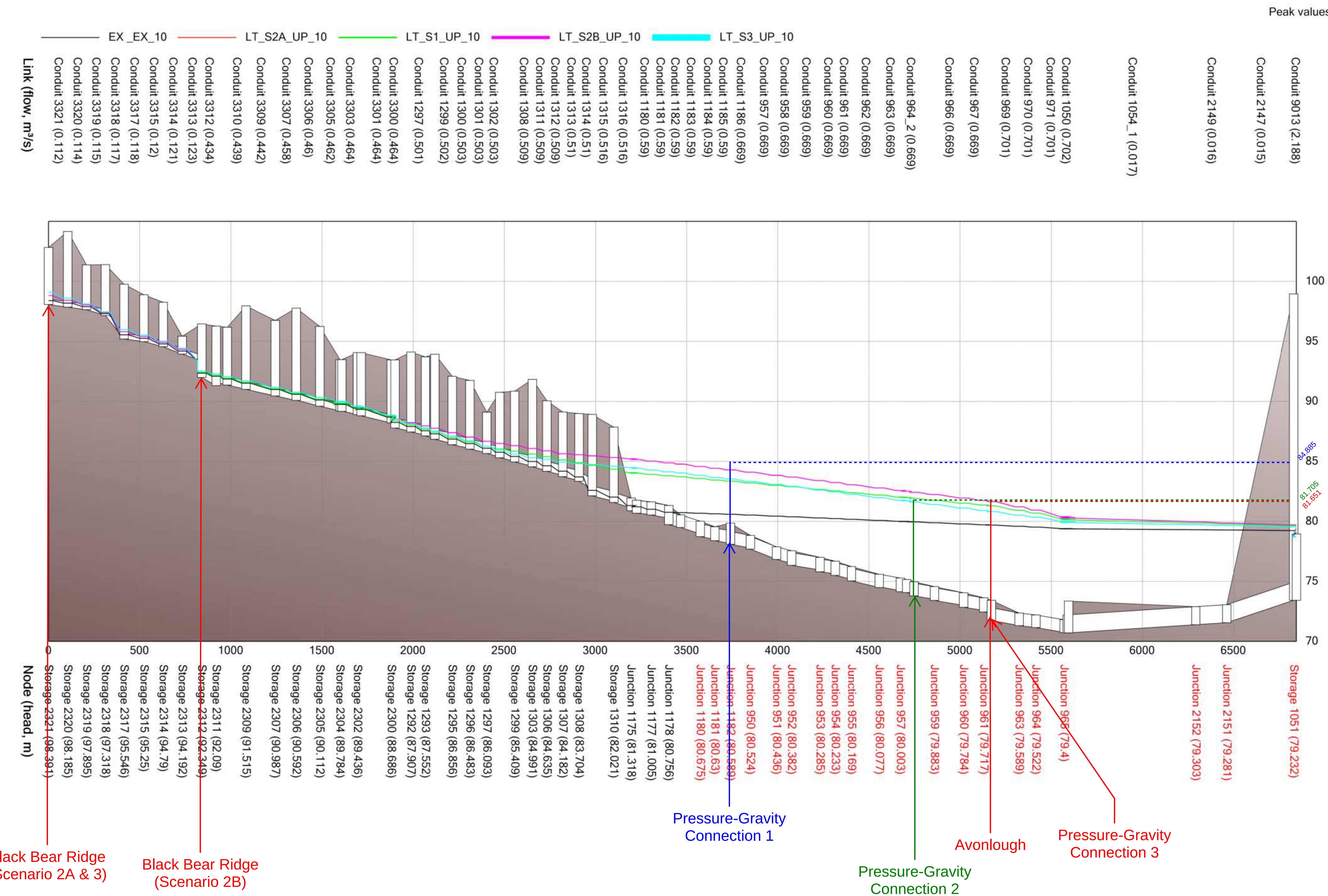
DRAWING:

SCENARIO 2B - UPGRADES

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

DESIGN:	ZG	JLR NO:	32874-000
DRAWN:	ZG	DRAWING NO:	
CHECKED:	ZG		**Figure B-12**

Figure B-13	All Scenarios with Upgrades - HGL Profile - 1:10-Year Storm Event



```
[TITLE]
;;Project Title/Notes
Existing Scenario Model Network. Model has been updated to account population up to 2023

[OPTIONS]
;;Option             Value
FLOW_UNITS           CMS
INFILTRATION         HORTON
FLOW_ROUTING         DYNWAVE
LINK_OFFSETS         ELEVATION
MIN_SLOPE            0
ALLOW_PONDING        NO
SKIP_STEADY_STATE    NO

START_DATE           03/13/2018
START_TIME           02:10:00
REPORT_START_DATE    03/13/2018
REPORT_START_TIME    02:10:00
END_DATE             03/17/2018
END_TIME             02:10:00
SWEEP_START          01/01
SWEEP_END            12/31
DRY_DAYS             0
REPORT_STEP          00:01:00
WET_STEP             00:05:00
DRY_STEP             00:05:00
ROUTING_STEP         1
RULE_STEP            00:00:00

INERTIAL_DAMPING     PARTIAL
NORMAL_FLOW_LIMITED  BOTH
FORCE_MAIN_EQUATION  H-W
VARIABLE_STEP        0.75
LENGTHENING_STEP     0
MIN_SURFAREA         0
MAX_TRIALS           8
HEAD_TOLERANCE       0.0015
SYS_FLOW_TOL         5
LAT_FLOW_TOL         5
MINIMUM_STEP         0.5
THREADS              24

[EVAPORATION]
;;Data Source    Parameters
;;-------------- ----------------
CONSTANT         0.0
DRY_ONLY         NO

[RAINGAGES]
;;Name           Format    Interval SCF      Source
;;-------------- --------- -------- -------- ----------
100yrSCS         INTENSITY 0:15     1.0      TIMESERIES 100yrSCS
CHI_3hr_100yr    INTENSITY 0:10     1.0      TIMESERIES CHI_3hr_100yr
Intensity        INTENSITY 0:05     1.0      TIMESERIES Intensity
SCS_24hr_100yr   INTENSITY 0:15     1.0      TIMESERIES SCS_24hr_100yr
SCS_24hr_10yr    INTENSITY 0:15     1.0      TIMESERIES SCS_24hr_10yr
Zero_Rainfall    INTENSITY 0:10     1.0      TIMESERIES Zero_Rainfall

[JUNCTIONS]
;;Name           Elevation  MaxDepth   InitDepth  SurDepth   Aponded
;;-------------- ---------- ---------- ---------- ---------- ----------
1048             70.7       1.5        8.012      13.8       0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
1050             69.495     6.655      4.265      24.723     0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
1050_1           74.446     1.704      4.266      34.363     0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
1050_2           74.446     0.679      4.266      25.148     0
1175             80.89      1.056      0          4.054      0
1176             80.68      1.08       0          4.24       0
1177             80.53      1.1        0          4.37       0
1178             79.73      1.59       0          4.68       0
1179             79.49      1.05       0          5.46       0
1180             78.73      1.28       0          5.99       0
1181             78.39      1.16       0.322      6.45       0
1182             78.093     1.757      0.619      6.15       0
2151             71.557     1.5        7.155      12.943     0
2152             71.392     1.5        7.32       13.108     0
2271             79.285     0.4        0          7.689      0
2272             77.419     1.625      1.293      6.924      0
2273             78.794     1.696      0          6.451      0
2275             77.585     0.466      1.127      8.54       0
2276             77.364     0.546      1.348      15.597     0
2277             76.163     1.068      2.549      15.532     0
2278             72.7       3.61       6.012      8.097      0
2279             77.118     0.409      1.594      7.473      0
;Valve chamber.
2280             74.072     1.078      4.64       10.85      0
;Syphon Outlet for Forcemain
2339             92.39      0.815      0          2.46       0
2339_1           90.6       0.55       0          10         0
2339_2           90.6       0.35       0          10         0
2339_3           90.6       0.35       0          10         0
;Syphon Inlet for Forcemain
;Bobby Pettigrew - 2018.03.12 Forcemain updated as per Drawings in Appendix D of the Cannifton Secondary
Plan Servicing Review and Update, Greer Galloway Group, Nov 2013
2340             93.51      1.115      0          5          0
2340_1           93.514     1.111      0          5          0
2340_2           93.515     1.11       0          5          0
2340_3           90.7       0.45       0          10         0
2340_4           90.7       0.25       0          10         0
2340_5           90.7       0.25       0          10         0
430              75.996     0.4        2.716      9.338      0
;Bobby Pettigrew - 2017.09.27 JLR Manhole
67               79.7       0.45       0          120        0
;Bobby Pettigrew - 2017.11.17 Elevations and approximate route from drawing set for Ontario Water
Commission Project 61-5-84, February 1962
902              75.276     0.45       3.436      23.059     0
902a             75.286     0.45       3.426      24.537     0
;Bobby Pettigrew - 2017.11.17 Elevations and approximate route from drawing set for Ontario Water
Commission Project 1-0004-66, August 1969
905              75.45      0.61       3.262      100        0
950              77.69      1.141      1.022      7.169      0
951              76.83      1.05       1.882      8.12       0
952              76.34      1.21       2.372      8.45       0
953              75.8       1.201      2.912      8.999      0
954              75.5       1.18       3.212      9.32       0
955              75.04      1.191      3.672      9.769      0
956              74.49      1.101      4.222      10.409     0
957              74.14      1.14       4.572      10.72      0
958              73.79      1.18       4.922      11.03      0
959              73.41      1.151      5.302      11.439     0
960              72.84      1.21       5.872      11.95      0
961              72.45      1.18       6.262      12.37      0
962              71.75      1.675      6.962      12.575     0
963              71.31      1.05       7.402      13.64      0
964              71.15      1.05       7.562      13.8       0
965              70.73      1.071      7.982      14.199     0
9914             70.708     2.65       8.004      12.642     0
9915             74.5       2.628      4.212      24.316     0
9916             74.5       2.628      4.212      24.316     0
DundasFM_1       82.1       0.45       0          8          0
DundasFM_2       79.95      0.45       0          10         0
DundasFM_3       79.96      0.45       0          15         0
EastFM_1         76.63      0.451      2.212      24.316     0
EastFM_2         76.63      0.451      2.212      34.316     0

[OUTFALLS]
;;Name           Elevation  Type       Stage Data       Gated    Route To
;;-------------- ---------- ---------- ---------------- -------- ----------------
;Bobby Pettigrew - 2018.01.11 Suggested by Project No. 61-5-84 Contract 1 Trunk Sewer from Moira River at
Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction Chamber but dimensions or
elevations not provided
Dundas_Street_Outfall 72.5  FIXED      74.8             NO
Dundas_Street_PS_Overflow_1 77 FIXED   74.8             NO
Front_St_PS_Overflow_1 74   FIXED      74.8             NO
WWTP             73.42      FIXED      78.712           NO

[STORAGE]
;;Name           Elev.    MaxDepth   InitDepth  Shape      Curve Name/Params            SurDepth Fevap
Psi      Ksat     IMD
;;-------------- -------- ---------- ----------- ---------- ---------------------------- -------- --------
-------- -------- --------
1005             76.819   6.218      0          FUNCTIONAL 0         0         1.13     0        0
1007             76.641   7.358      0          FUNCTIONAL 0         0         1.13     0        0
;Bobby Pettigrew - 2017.09.27 JLR revised SanMHID from 2011 to 1008 to reflect Conduit Layer
1008             76.4     7.856      0          FUNCTIONAL 0         0         1.13     0        0
1020             75.78    7.496      0          FUNCTIONAL 0         0         1.13     0        0
1022             75.73    7.47       0          FUNCTIONAL 0         0         1.13     0        0
1023             75.36    6.417      0          FUNCTIONAL 0         0         1.13     0        0
1024             74.84    7.34       0          FUNCTIONAL 0         0         1.13     0        0
1025             74.567   5.61       0          FUNCTIONAL 0         0         1.13     0        0
;Bobby Pettigrew - 2017.10.23 Node added from Drawing 6 of Project No. 1-0004-01 Main Trunk Sewer
Connection
1026             74.25    5.927      0          FUNCTIONAL 0         0         1.13     0        0
1029             75.52    6.722      0          FUNCTIONAL 0         0         1.13     0        0
1030             75.426   6.816      0          FUNCTIONAL 0         0         1.13     0        0
1031             74.959   5.44       0          FUNCTIONAL 0         0         1.13     0        0
1042             76.666   5.531      0          FUNCTIONAL 0         0         1.13     0        0
1044             80.958   3.549      0          FUNCTIONAL 0         0         1.13     0        0
1045             78.776   4.228      0          FUNCTIONAL 0         0         1.13     0        0
;Bobby Pettigrew - 2018.01.10 Wet well size from AECOM Front Street Sewage Pumping Station Operations and
Maintenance Manual June 2010
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
1049             69.495   10.682     1.3        FUNCTIONAL 0         0         21.09    0        0
1051             73.425   25.526     5.287      FUNCTIONAL 0         0         1.13     0        0
106              77.864   6.002      0          FUNCTIONAL 0         0         1.13     0        0
107              78.11    5.379      0          FUNCTIONAL 0         0         1.13     0        0
1085             82.281   3.493      0          FUNCTIONAL 0         0         1.13     0        0
1090             82.753   3.976      0          FUNCTIONAL 0         0         1.13     0        0
1091             82.482   3.996      0          FUNCTIONAL 0         0         1.13     0        0
1092             82.326   3.982      0          FUNCTIONAL 0         0         1.13     0        0
1093             82.805   3.77       0          FUNCTIONAL 0         0         1.13     0        0
1096             83.043   3.425      0          FUNCTIONAL 0         0         1.13     0        0
1101             83.11    3.931      0          FUNCTIONAL 0         0         1.13     0        0
1111             83.39    4.341      0          FUNCTIONAL 0         0         1.13     0        0
1114             83.265   4.466      0          FUNCTIONAL 0         0         1.13     0        0
1115             83.351   3.958      0          FUNCTIONAL 0         0         1.13     0        0
1116             83.216   3.009      0          FUNCTIONAL 0         0         1.13     0        0
1117             83.442   3.619      0          FUNCTIONAL 0         0         1.13     0        0
112              78.776   4.524      0          FUNCTIONAL 0         0         1.13     0        0
1131             82.098   4.594      0          FUNCTIONAL 0         0         1.13     0        0
1185             82.134   4.026      0          FUNCTIONAL 0         0         1.13     0        0
1186             82.092   4.068      0          FUNCTIONAL 0         0         1.13     0        0
1187             81.702   7.27       0          FUNCTIONAL 0         0         1.13     0        0
1190             81.363   6.637      0          FUNCTIONAL 0         0         1.13     0        0
1191             81.018   7.373      0          FUNCTIONAL 0         0         1.13     0        0
1192             85.134   6.104      0          FUNCTIONAL 0         0         1.13     0        0
1193             84.634   5.197      0          FUNCTIONAL 0         0         1.13     0        0
1195             84.34    6.248      0          FUNCTIONAL 0         0         1.13     0        0
1196             84.052   6.533      0          FUNCTIONAL 0         0         1.13     0        0
1199             83.076   5.701      0          FUNCTIONAL 0         0         1.13     0        0
1202             85.609   5.31       0          FUNCTIONAL 0         0         1.13     0        0
1203             85.978   5.226      0          FUNCTIONAL 0         0         1.13     0        0
1204             86.484   7.862      0          FUNCTIONAL 0         0         1.13     0        0
1205             86.999   8.788      0          FUNCTIONAL 0         0         1.13     0        0
1206             87.478   7.178      0          FUNCTIONAL 0         0         1.13     0        0
1208             89.687   3.34       0          FUNCTIONAL 0         0         1.13     0        0
1209             89.288   4.94       0          FUNCTIONAL 0         0         1.13     0        0
1210             88.901   5.148      0          FUNCTIONAL 0         0         1.13     0        0
1211             88.407   5.127      0          FUNCTIONAL 0         0         1.13     0        0
1212             87.932   5.651      0          FUNCTIONAL 0         0         1.13     0        0
1216             91.318   3.915      0          FUNCTIONAL 0         0         1.13     0        0
1217             90.66    5.2        0          FUNCTIONAL 0         0         1.13     0        0
1218             90.385   7.152      0          FUNCTIONAL 0         0         1.13     0        0
1219             90.093   8.596      0          FUNCTIONAL 0         0         1.13     0        0
1220             89.834   7.431      0          FUNCTIONAL 0         0         1.13     0        0
1221             89.517   5.281      0          FUNCTIONAL 0         0         1.13     0        0
```

```
1222  91.909  4.986   0      FUNCTIONAL  0  0  1.13  0  0
1241  92.915  3.809   0      FUNCTIONAL  0  0  1.13  0  0
1242  92.659  4.206   0      FUNCTIONAL  0  0  1.13  0  0
1243  92.153  4.883   0      FUNCTIONAL  0  0  1.13  0  0
1244  92.153  3.734   0      FUNCTIONAL  0  0  1.13  0  0
1245  91.842  3.477   0      FUNCTIONAL  0  0  1.13  0  0
1246  91.528  3.617   0      FUNCTIONAL  0  0  1.13  0  0
1247  91.178  3.322   0      FUNCTIONAL  0  0  1.13  0  0
1248  90.873  4.081   0      FUNCTIONAL  0  0  1.13  0  0
1249  90.526  3.758   0      FUNCTIONAL  0  0  1.13  0  0
1252  90.134  4.712   0      FUNCTIONAL  0  0  1.13  0  0
1253  89.758  4.894   0      FUNCTIONAL  0  0  1.13  0  0
1286  89.538  4.666   0      FUNCTIONAL  0  0  1.13  0  0
1287  89.322  5.713   0      FUNCTIONAL  0  0  1.13  0  0
1288  89.032  3.855   0      FUNCTIONAL  0  0  1.13  0  0
1289  88.776  5.379   0      FUNCTIONAL  0  0  1.13  0  0
1290  88.505  5.314   0      FUNCTIONAL  0  0  1.13  0  0
1291  87.78   5.675   0      FUNCTIONAL  0  0  1.13  0  0
1292  87.45   6.66    0      FUNCTIONAL  0  0  1.13  0  0
1293  87.12   6.586   0      FUNCTIONAL  0  0  1.13  0  0
1294  86.84   7.087   0      FUNCTIONAL  0  0  1.13  0  0
1295  86.39   5.699   0      FUNCTIONAL  0  0  1.13  0  0
1296  86.02   5.725   0      FUNCTIONAL  0  0  1.13  0  0
1297  85.66   3.433   0      FUNCTIONAL  0  0  1.13  0  0
1298  85.3    5.452   0      FUNCTIONAL  0  0  1.13  0  0
1299  84.95   5.9     0      FUNCTIONAL  0  0  1.13  0  0
1303  84.55   7.283   0      FUNCTIONAL  0  0  1.13  0  0
1306  84.17   5.874   0      FUNCTIONAL  0  0  1.13  0  0
1307  83.73   5.384   0      FUNCTIONAL  0  0  1.13  0  0
1308  83.34   5.643   0      FUNCTIONAL  0  0  1.13  0  0
1309  82.13   6.783   0      FUNCTIONAL  0  0  1.13  0  0
1310  81.58   6.273   0      FUNCTIONAL  0  0  1.13  0  0
1344  81.506  5.794   0      FUNCTIONAL  0  0  1.13  0  0
1345  81.341  6.137   0      FUNCTIONAL  0  0  1.13  0  0
1346  81.004  6.405   0      FUNCTIONAL  0  0  1.13  0  0
1347  80.82   6.937   0      FUNCTIONAL  0  0  1.13  0  0
1348  80.39   7.463   0      FUNCTIONAL  0  0  1.13  0  0
135   80.151  3.941   0      FUNCTIONAL  0  0  1.13  0  0
1352  79.898  7.34    0      FUNCTIONAL  0  0  1.13  0  0
136   80.482  3.386   0      FUNCTIONAL  0  0  1.13  0  0
137   81.14   4.388   0      FUNCTIONAL  0  0  1.13  0  0
138   82.381  3.186   0      FUNCTIONAL  0  0  1.13  0  0
1511  88.06   3.587   0      FUNCTIONAL  0  0  1.13  0  0
1514  87.895  3.41    0      FUNCTIONAL  0  0  1.13  0  0
157   80.894  3.227   0      FUNCTIONAL  0  0  1.13  0  0
158   81.5    2.621   0      FUNCTIONAL  0  0  1.13  0  0
159   80.693  3.673   0      FUNCTIONAL  0  0  1.13  0  0
1593  87.435  5.159   0      FUNCTIONAL  0  0  1.13  0  0
161   87.161  2.058   0      FUNCTIONAL  0  0  1.13  0  0
162   85.789  1.806   0      FUNCTIONAL  0  0  1.13  0  0
163   82.39   4.784   0      FUNCTIONAL  0  0  1.13  0  0
164   84.11   1.686   0      FUNCTIONAL  0  0  1.13  0  0
165   88.438  2.396   0      FUNCTIONAL  0  0  1.13  0  0
166   89.922  1.471   0      FUNCTIONAL  0  0  1.13  0  0
167   91.135  2.339   0      FUNCTIONAL  0  0  1.13  0  0
168   91.638  1.155   0      FUNCTIONAL  0  0  1.13  0  0
169   92.296  1.218   0      FUNCTIONAL  0  0  1.13  0  0
170   92.565  2.944   0      FUNCTIONAL  0  0  1.13  0  0
1705  82.308  3.192   0      FUNCTIONAL  0  0  1.13  0  0
171   93.244  3       0      FUNCTIONAL  0  0  1.13  0  0
1718  84.189  2.947   0      FUNCTIONAL  0  0  1.13  0  0
1719  83.652  3.602   0      FUNCTIONAL  0  0  1.13  0  0
172   93.223  3       0      FUNCTIONAL  0  0  1.13  0  0
1720  83.293  4.488   0      FUNCTIONAL  0  0  1.13  0  0
1721  82.82   3.976   0      FUNCTIONAL  0  0  1.13  0  0
1725  84.543  3.881   0      FUNCTIONAL  0  0  1.13  0  0
173   93.028  1.849   0      FUNCTIONAL  0  0  1.13  0  0
174   92.766  2.743   0      FUNCTIONAL  0  0  1.13  0  0
1742  84.569  3.083   0      FUNCTIONAL  0  0  1.13  0  0
1743  84.235  4.547   0      FUNCTIONAL  0  0  1.13  0  0
1745  82.134  3.64    0      FUNCTIONAL  0  0  1.13  0  0
1746  82.037  3.509   0      FUNCTIONAL  0  0  1.13  0  0
1747  81.738  2.648   0      FUNCTIONAL  0  0  1.13  0  0
1748  81.659  2.727   0      FUNCTIONAL  0  0  1.13  0  0
1749  81.406  3.306   0      FUNCTIONAL  0  0  1.13  0  0
175   92.711  2.798   0      FUNCTIONAL  0  0  1.13  0  0
1750  81.028  3.105   0      FUNCTIONAL  0  0  1.13  0  0
1754  81.967  3.928   0      FUNCTIONAL  0  0  1.13  0  0
1755  81.699  3.509   0      FUNCTIONAL  0  0  1.13  0  0
1756  81.449  2.705   0      FUNCTIONAL  0  0  1.13  0  0
1757  81.321  3.147   0      FUNCTIONAL  0  0  1.13  0  0
1758  81.11   3.724   0      FUNCTIONAL  0  0  1.13  0  0
1759  80.775  4.289   0      FUNCTIONAL  0  0  1.13  0  0
1763  80.098  5.299   0      FUNCTIONAL  0  0  1.13  0  0
1768  79.693  4.122   0      FUNCTIONAL  0  0  1.13  0  0
1769  79.428  4.004   0      FUNCTIONAL  0  0  1.13  0  0
1770  78.946  4.486   0      FUNCTIONAL  0  0  1.13  0  0
1771  77.809  4.039   0      FUNCTIONAL  0  0  1.13  0  0
1772  79.98   3.513   0      FUNCTIONAL  0  0  1.13  0  0
1773  78.904  3.933   0      FUNCTIONAL  0  0  1.13  0  0
1774  76.675  5.173   0      FUNCTIONAL  0  0  1.13  0  0
1794  75.121  4.043   0      FUNCTIONAL  0  0  1.13  0  0
1795  74.841  3.246   0      FUNCTIONAL  0  0  1.13  0  0
1796  74.758  3.773   0      FUNCTIONAL  0  0  1.13  0  0
1797  74.697  1.583   0      FUNCTIONAL  0  0  1.13  0  0
1798  74.563  5.736   0      FUNCTIONAL  0  0  1.13  0  0
1799  74.46   4.027   0      FUNCTIONAL  0  0  1.13  0  0
1800  74.347  4.225   0      FUNCTIONAL  0  0  1.13  0  0
1801  74.222  3.598   0      FUNCTIONAL  0  0  1.13  0  0
1812  74.17   6.439   0      FUNCTIONAL  0  0  1.13  0  0
1866  74.124  5.954   0      FUNCTIONAL  0  0  1.13  0  0
1867  74.002  5.463   0      FUNCTIONAL  0  0  1.13  0  0
1868  74.018  5.82    0      FUNCTIONAL  0  0  1.13  0  0
1869  73.765  5.375   0      FUNCTIONAL  0  0  1.13  0  0
1870  73.673  7.569   0      FUNCTIONAL  0  0  1.13  0  0
1871  73.609  8.024   0      FUNCTIONAL  0  0  1.13  0  0
1872  73.512  8.092   0      FUNCTIONAL  0  0  1.13  0  0
1873  73.356  7.012   0.12   FUNCTIONAL  0  0  1.13  0  0
1874  73.292  8.608   0.184  FUNCTIONAL  0  0  1.13  0  0
1875  73.243  9.874   0.233  FUNCTIONAL  0  0  1.13  0  0
1876  73.012  10.114  0.464  FUNCTIONAL  0  0  1.13  0  0
```

```
1877  87.164  3.433   0      FUNCTIONAL  0  0  1.13  0  0
1880  86.975  2.288   0      FUNCTIONAL  0  0  1.13  0  0
1881  86.774  1.772   0      FUNCTIONAL  0  0  1.13  0  0
1898  84.28   1.988   0      FUNCTIONAL  0  0  1.13  0  0
1899  84.247  2.021   0      FUNCTIONAL  0  0  1.13  0  0
1913  83.872  2.01    0      FUNCTIONAL  0  0  1.13  0  0
1914  83.814  2.068   0      FUNCTIONAL  0  0  1.13  0  0
1915  83.479  1.686   0      FUNCTIONAL  0  0  1.13  0  0
1916  82.903  2.232   0      FUNCTIONAL  0  0  1.13  0  0
1917  81.979  3.486   0      FUNCTIONAL  0  0  1.13  0  0
1918  81.711  3.754   0      FUNCTIONAL  0  0  1.13  0  0
1919  81.186  3.402   0      FUNCTIONAL  0  0  1.13  0  0
1920  81.433  3.692   0      FUNCTIONAL  0  0  1.13  0  0
1923  81.497  3.102   0      FUNCTIONAL  0  0  1.13  0  0
1927  81.232  4.372   0      FUNCTIONAL  0  0  1.13  0  0
1931  79.199  3.766   0      FUNCTIONAL  0  0  1.13  0  0
1932  77.252  4.446   0      FUNCTIONAL  0  0  1.13  0  0
1933  72.74   7.579   0.736  FUNCTIONAL  0  0  1.13  0  0
1938  72.649  11.361  0.827  FUNCTIONAL  0  0  1.13  0  0
1939  72.878  7.854   0.598  FUNCTIONAL  0  0  1.13  0  0
1940  72.731  11.82   0.745  FUNCTIONAL  0  0  1.13  0  0
1941  72.591  8.264   0.885  FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.03.13 No East End Pump Station overflow as per email of March 12, 2018 from Stan
Czyczyro
1942  71.628  5.872   1.08   FUNCTIONAL  0  0  20.8  0  0
1943  81.744  3.721   0      FUNCTIONAL  0  0  1.13  0  0
1968  87.508  4.806   0      FUNCTIONAL  0  0  1.13  0  0
1969  87.883  3.587   0      FUNCTIONAL  0  0  1.13  0  0
1970  87.998  3.122   0      FUNCTIONAL  0  0  1.13  0  0
2029  84.066  3.575   0      FUNCTIONAL  0  0  1.13  0  0
2030  84.138  4.382   0      FUNCTIONAL  0  0  1.13  0  0
2031  84.225  4.424   0      FUNCTIONAL  0  0  1.13  0  0
2032  83.9    3.039   0      FUNCTIONAL  0  0  1.13  0  0
2033  84.311  3.978   0      FUNCTIONAL  0  0  1.13  0  0
2034  84.391  4.478   0      FUNCTIONAL  0  0  1.13  0  0
2035  84.502  3.985   0      FUNCTIONAL  0  0  1.13  0  0
2036  84.668  4.4     0      FUNCTIONAL  0  0  1.13  0  0
2061  86.947  2.175   0      FUNCTIONAL  0  0  1.13  0  0
2062  81.5    3.629   0      FUNCTIONAL  0  0  1.13  0  0
2063  81.574  3.555   0      FUNCTIONAL  0  0  1.13  0  0
2096  79.548  3.56    0      FUNCTIONAL  0  0  1.13  0  0
2097  79.706  5.976   0      FUNCTIONAL  0  0  1.13  0  0
2105  87.328  5.605   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.08.23 Elevation taken from Yeomans Street As-builts Project No. 10-13079 Dwg No.
110 North East Feedermain and Road Reconstruction
211   91.693  2.367   0      FUNCTIONAL  0  0  1.13  0  0
212   92.156  1.48    0      FUNCTIONAL  0  0  1.13  0  0
213   91.474  0.647   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2140  78.65   4.05    0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2140_1  78.77  4.52   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2140_2  78.86  5.11   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2140_3  78.96  4.78   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2140_4  79.02  5.08   0      FUNCTIONAL  0  0  1.13  0  0
2141  73.426  5.638   0      FUNCTIONAL  0  0  1.13  0  0
2146  89.892  3.135   0      FUNCTIONAL  0  0  1.13  0  0
2147  90.415  3.004   0      FUNCTIONAL  0  0  1.13  0  0
2148  90.853  2.114   0      FUNCTIONAL  0  0  1.13  0  0
2154  77.898  3.117   0      FUNCTIONAL  0  0  1.13  0  0
2155  76.81   5.961   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.08.23 Elevation raised to surrounding nodes level
216   91.303  0.877   0      FUNCTIONAL  0  0  1.13  0  0
2176  83.55   3.99    0      FUNCTIONAL  0  0  1.13  0  0
2177  83.61   3.397   0      FUNCTIONAL  0  0  1.13  0  0
2178  83.68   3.949   0      FUNCTIONAL  0  0  1.13  0  0
2179  83.76   3.143   0      FUNCTIONAL  0  0  1.13  0  0
2180  83.79   2.388   0      FUNCTIONAL  0  0  1.13  0  0
2217  86.78   6.837   0      FUNCTIONAL  0  0  1.13  0  0
2218  86.62   5.787   0      FUNCTIONAL  0  0  1.13  0  0
2219  86.46   5.706   0      FUNCTIONAL  0  0  1.13  0  0
222   90.98   1.2     0      FUNCTIONAL  0  0  1.13  0  0
2220  85.95   7.459   0      FUNCTIONAL  0  0  1.13  0  0
2221  86.08   7.457   0      FUNCTIONAL  0  0  1.13  0  0
2222  85.57   7.31    0      FUNCTIONAL  0  0  1.13  0  0
2223  85.41   5.808   0      FUNCTIONAL  0  0  1.13  0  0
2224  85.16   5.819   0      FUNCTIONAL  0  0  1.13  0  0
2259  87.054  7.713   0      FUNCTIONAL  0  0  1.13  0  0
2264  84.885  3.22    0      FUNCTIONAL  0  0  1.13  0  0
2265  81.871  6.234   0      FUNCTIONAL  0  0  1.13  0  0
2266  81.183  4.976   0      FUNCTIONAL  0  0  1.13  0  0
2267  78.897  7.177   0      FUNCTIONAL  0  0  1.13  0  0
;Bobby Pettigrew - 2018.02.13 Elevation assumed from Project No. I-0004-01 Contract No,4 Drawing No.4
2268  85.457  4.357   0      FUNCTIONAL  0  0  1.13  0  0
2269  81.25   4.533   0      FUNCTIONAL  0  0  1.13  0  0
2270  80.007  6.039   0      FUNCTIONAL  0  0  1.13  0  0
;Junction chamber.
;Bobby Pettigrew - 2018.01.11 Dimensions as per Project No. 61-5-84 Contract 1 Trunk Sewer from Moira
River at Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction Chamber
2282  71.009  8.055   0      FUNCTIONAL  0  0  2.25  0  0
;Junction chamber.
;Bobby Pettigrew - 2018.01.11 Section of Junction Chamber as per Project No. 61-5-84 Contract 1 Trunk
Sewer from Moira River at Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction
Chamber
2282_1  71.009  8.055  0     FUNCTIONAL  0  0  2.25  0  0
;Junction Chamber
;Bobby Pettigrew - 2018.01.11 Dimensions as per Project No. 61-5-84 Contract 1 Trunk Sewer from Moira
River at Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction Chamber
2282_2  73.304  5.76   0     FUNCTIONAL  0  0  6.69  0  0
;was 1967
2286  86.624  2.839   0      FUNCTIONAL  0  0  1.13  0  0
2300  88.2    5.255   0      FUNCTIONAL  0  0  1.13  0  0
2301  88.8    5.259   0      FUNCTIONAL  0  0  1.13  0  0
```

```
2302             88.9     5.159    0          FUNCTIONAL  0          0          1.13     0        0
2303             89.17    4.305    0          FUNCTIONAL  0          0          1.13     0        0
2304             89.2     4.275    0          FUNCTIONAL  0          0          1.13     0        0
2305             89.6     6.647    0          FUNCTIONAL  0          0          1.13     0        0
2306             90.08    7.691    0          FUNCTIONAL  0          0          1.13     0        0
2307             90.45    6.294    0          FUNCTIONAL  0          0          1.13     0        0
2309             91       6.953    0          FUNCTIONAL  0          0          1.13     0        0
231              90.638   0.5      0          FUNCTIONAL  0          0          1.13     0        0
2310             91.36    4.809    0          FUNCTIONAL  0          0          1.13     0        0
2311             91.31    4.959    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.12 Forcemain updated as per Drawings in Appendix D of the Cannifton Secondary
Plan Servicing Review and Update, Greer Galloway Group, Nov 2013
2312             91.99    4.469    0          FUNCTIONAL  0          0          1.13     0        0
2313             93.94    1.485    0          FUNCTIONAL  0          0          1.13     0        0
2314             94.55    3.707    0          FUNCTIONAL  0          0          1.13     0        0
2315             94.98    3.902    0          FUNCTIONAL  0          0          1.13     0        0
2317             95.2     4.563    0          FUNCTIONAL  0          0          1.13     0        0
2318             97.15    4.244    0          FUNCTIONAL  0          0          1.13     0        0
2319             97.64    3.734    0          FUNCTIONAL  0          0          1.13     0        0
2320             97.85    6.305    0          FUNCTIONAL  0          0          1.13     0        0
2321             98.07    4.752    0          FUNCTIONAL  0          0          1.13     0        0
2341             93.87    2.99     0          FUNCTIONAL  0          0          1.13     0        0
2342             94.15    3.645    0          FUNCTIONAL  0          0          1.13     0        0
2343             94.36    4.001    0          FUNCTIONAL  0          0          1.13     0        0
2344             94.5     3.499    0          FUNCTIONAL  0          0          1.13     0        0
2345             94.6     3.4      0          FUNCTIONAL  0          0          1.13     0        0
2346             94.79    3.54     0          FUNCTIONAL  0          0          1.13     0        0
2347             95.25    3.605    0          FUNCTIONAL  0          0          1.13     0        0
2348             95.56    4.753    0          FUNCTIONAL  0          0          1.13     0        0
;connects to 200mm forcemain
2349             95.74    4.573    0          FUNCTIONAL  0          0          1.13     0        0
236              89.7     1.537    0          FUNCTIONAL  0          0          1.13     0        0
2363             89.17    5.05     0          FUNCTIONAL  0          0          1.13     0        0
2364             89.3     4.92     0          FUNCTIONAL  0          0          1.13     0        0
2365             89.63    4.896    0          FUNCTIONAL  0          0          1.13     0        0
2366             89.93    4.646    0          FUNCTIONAL  0          0          1.13     0        0
2367             90.29    3.856    0          FUNCTIONAL  0          0          1.13     0        0
2368             90.37    3.776    0          FUNCTIONAL  0          0          1.13     0        0
2369             90.53    4.102    0          FUNCTIONAL  0          0          1.13     0        0
2370             90.83    3.293    0          FUNCTIONAL  0          0          1.13     0        0
2371             90.89    3.233    0          FUNCTIONAL  0          0          1.13     0        0
2372             91.22    3.42     0          FUNCTIONAL  0          0          1.13     0        0
2373             91.53    6.206    0          FUNCTIONAL  0          0          1.13     0        0
2374             91.83    5.565    0          FUNCTIONAL  0          0          1.13     0        0
2375             92.14    4.356    0          FUNCTIONAL  0          0          1.13     0        0
2376             92.44    3.882    0          FUNCTIONAL  0          0          1.13     0        0
2377             92.74    5.383    0          FUNCTIONAL  0          0          1.13     0        0
2378             93.05    3.522    0          FUNCTIONAL  0          0          1.13     0        0
2379             93.37    3.787    0          FUNCTIONAL  0          0          1.13     0        0
2380             93.42    3.737    0          FUNCTIONAL  0          0          1.13     0        0
2381             93.78    4.142    0          FUNCTIONAL  0          0          1.13     0        0
2382             94.08    4.707    0          FUNCTIONAL  0          0          1.13     0        0
2383             94.32    3.412    0          FUNCTIONAL  0          0          1.13     0        0
2384             94.64    3.79     0          FUNCTIONAL  0          0          1.13     0        0
2385             94.91    4.33     0          FUNCTIONAL  0          0          1.13     0        0
2386             95.27    3.7      0          FUNCTIONAL  0          0          1.13     0        0
2387             95.58    3.879    0          FUNCTIONAL  0          0          1.13     0        0
2388             95.88    5.127    0          FUNCTIONAL  0          0          1.13     0        0
2389             96.19    4.921    0          FUNCTIONAL  0          0          1.13     0        0
2390             96.49    3.714    0          FUNCTIONAL  0          0          1.13     0        0
2391             96.86    4.201    0          FUNCTIONAL  0          0          1.13     0        0
2392             97.01    4.184    0          FUNCTIONAL  0          0          1.13     0        0
2393             98.13    4.063    0          FUNCTIONAL  0          0          1.13     0        0
2394             98.33    3.347    0          FUNCTIONAL  0          0          1.13     0        0
2395             98.53    3.334    0          FUNCTIONAL  0          0          1.13     0        0
2397             95.36    5.264    0          FUNCTIONAL  0          0          1.13     0        0
2398             95.67    4.437    0          FUNCTIONAL  0          0          1.13     0        0
2399             95.97    6.561    0          FUNCTIONAL  0          0          1.13     0        0
2400             96.27    6.399    0          FUNCTIONAL  0          0          1.13     0        0
2401             96.65    4.581    0          FUNCTIONAL  0          0          1.13     0        0
2402             96.95    3.829    0          FUNCTIONAL  0          0          1.13     0        0
;No profile found for this MH
2453             86.38    5.967    0          FUNCTIONAL  0          0          1.13     0        0
2474             75.543   6.169    0          FUNCTIONAL  0          0          1.13     0        0
2475             75.17    6.925    0          FUNCTIONAL  0          0          1.13     0        0
2476             74.767   8.263    0          FUNCTIONAL  0          0          1.13     0        0
2477             74.495   6.367    0          FUNCTIONAL  0          0          1.13     0        0
284              78.388   3.188    0          FUNCTIONAL  0          0          1.13     0        0
285              78.34    2.699    0          FUNCTIONAL  0          0          1.13     0        0
286              77.876   3.691    0          FUNCTIONAL  0          0          1.13     0        0
287              75.987   6.892    0          FUNCTIONAL  0          0          1.13     0        0
;RIM elevation updated from 78.784 to 80.267
288              75.743   4.524    0          FUNCTIONAL  0          0          1.13     0        0
289              75.377   7.394    0          FUNCTIONAL  0          0          1.13     0        0
290              75.255   6.26     0          FUNCTIONAL  0          0          1.13     0        0
300              92.784   0.576    0          FUNCTIONAL  0          0          1.13     0        0
3000             77.83    6.672    0          FUNCTIONAL  0          0          1.13     0        0
3000A            77.76    6.725    0          FUNCTIONAL  0          0          1.13     0        0
301              92.263   1.28     0          FUNCTIONAL  0          0          1.13     0        0
302              93.43    0.5      0          FUNCTIONAL  0          0          1.13     0        0
303              93.141   0.513    0          FUNCTIONAL  0          0          1.13     0        0
360              81.287   4.496    0          FUNCTIONAL  0          0          1.13     0        0
;Ivan DZeparoski - 2018.08.28 RIM elevation raised from 76.516 m to 80 m based on the MH location along
the Dundas Street West
401              75.072   6.089    0          FUNCTIONAL  0          0          1.13     0        0
;Ivan DZeparoski - 2018.08.28 RIM elevation raised from 76.82 m to 80.1 m based on the MH location along
the Dundas Street West
402              74.7     5.592    0          FUNCTIONAL  0          0          1.13     0        0
403              74.371   8.104    0          FUNCTIONAL  0          0          1.13     0        0
404              73.64    9.633    0          FUNCTIONAL  0          0          1.13     0        0
405              73.457   9.625    0          FUNCTIONAL  0          0          1.13     0        0
406              73.155   7.763    0          FUNCTIONAL  0          0          1.13     0        0
409              74.109   8.159    0          FUNCTIONAL  0          0          1.13     0        0
411              73.679   9.351    0          FUNCTIONAL  0          0          1.13     0        0
;Ivan DZeparoski - 2018.08.28 RIM elevation increased from 76.043 to 79.043
413              74.423   6.077    0          FUNCTIONAL  0          0          1.13     0        0
414              73.981   5.083    0          FUNCTIONAL  0          0          1.13     0        0
418              75.715   6.851    0          FUNCTIONAL  0          0          1.13     0        0
419              75.856   5.529    0          FUNCTIONAL  0          0          1.13     0        0
421              74.786   6.926    0          FUNCTIONAL  0          0          1.13     0        0
424              75.325   8.202    0          FUNCTIONAL  0          0          1.13     0        0
;RIM elevation updated from 77.913 to 81.741
425              74.164   7.577    0          FUNCTIONAL  0          0          1.13     0        0
426              73.451   7.052    0          FUNCTIONAL  0          0          1.13     0        0
427              73.451   5.613    0          FUNCTIONAL  0          0          1.13     0        0
428              76.986   5.062    0          FUNCTIONAL  0          0          1.13     0        0
429              75.788   5.522    0          FUNCTIONAL  0          0          1.13     0        0
431              75.956   5.429    0          FUNCTIONAL  0          0          1.13     0        0
432              76.584   5.827    0          FUNCTIONAL  0          0          1.13     0        0
433              77.157   7.418    0          FUNCTIONAL  0          0          1.13     0        0
434              77.172   7.403    0          FUNCTIONAL  0          0          1.13     0        0
435              87.395   0.5      0          FUNCTIONAL  0          0          1.13     0        0
436              79.224   4.471    0          FUNCTIONAL  0          0          1.13     0        0
437              76.85    7.836    0          FUNCTIONAL  0          0          1.13     0        0
438              77.837   6.849    0          FUNCTIONAL  0          0          1.13     0        0
439              76.724   5.849    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
44               78.55    4.43     0          FUNCTIONAL  0          0          1.13     0        0
446              80.388   5.276    0          FUNCTIONAL  0          0          1.13     0        0
447              80.175   5.489    0          FUNCTIONAL  0          0          1.13     0        0
448              79.629   4.131    0          FUNCTIONAL  0          0          1.13     0        0
449              77.084   7.795    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
45               78.33    4.77     0          FUNCTIONAL  0          0          1.13     0        0
451              78.044   6.146    0          FUNCTIONAL  0          0          1.13     0        0
452              77.255   7.32     0          FUNCTIONAL  0          0          1.13     0        0
453              77.992   6.342    0          FUNCTIONAL  0          0          1.13     0        0
454              77.517   6.7      0          FUNCTIONAL  0          0          1.13     0        0
455              80.104   5.942    0          FUNCTIONAL  0          0          1.13     0        0
456              80.921   5.576    0          FUNCTIONAL  0          0          1.13     0        0
457              78.032   8.014    0          FUNCTIONAL  0          0          1.13     0        0
458              77.727   6.253    0          FUNCTIONAL  0          0          1.13     0        0
459              78.849   7.122    0          FUNCTIONAL  0          0          1.13     0        0
460              77.486   8.096    0          FUNCTIONAL  0          0          1.13     0        0
461              78.681   7.693    0          FUNCTIONAL  0          0          1.13     0        0
462              78.51    7.864    0          FUNCTIONAL  0          0          1.13     0        0
463              78.51    4.171    0          FUNCTIONAL  0          0          1.13     0        0
464              78.328   5.275    0          FUNCTIONAL  0          0          1.13     0        0
465              78.349   7.376    0          FUNCTIONAL  0          0          1.13     0        0
468              78.446   5.744    0          FUNCTIONAL  0          0          1.13     0        0
469              78.593   6.054    0          FUNCTIONAL  0          0          1.13     0        0
473              78.166   7.744    0          FUNCTIONAL  0          0          1.13     0        0
477              79.733   5.417    0          FUNCTIONAL  0          0          1.13     0        0
478              79.339   6.562    0          FUNCTIONAL  0          0          1.13     0        0
479              82.089   5.692    0          FUNCTIONAL  0          0          1.13     0        0
480              81.513   5.738    0          FUNCTIONAL  0          0          1.13     0        0
481              80.303   5.884    0          FUNCTIONAL  0          0          1.13     0        0
501              78.903   5.179    0          FUNCTIONAL  0          0          1.13     0        0
502              78.83    5.592    0          FUNCTIONAL  0          0          1.13     0        0
503              78.547   7.178    0          FUNCTIONAL  0          0          1.13     0        0
506              79.322   5.613    0          FUNCTIONAL  0          0          1.13     0        0
507              79.92    4.543    0          FUNCTIONAL  0          0          1.13     0        0
508              79.575   5.117    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
51               78.21    4.44     0          FUNCTIONAL  0          0          1.13     0        0
;Ivan DZeparoski - 2018.09.07 RIM elevation updated from 84.523 to 85.127
511              80.894   5.465    0          FUNCTIONAL  0          0          1.13     0        0
512              80.334   5.454    0          FUNCTIONAL  0          0          1.13     0        0
513              80.806   4.923    0          FUNCTIONAL  0          0          1.13     0        0
514              81.034   6.627    0          FUNCTIONAL  0          0          1.13     0        0
516              81.162   5.983    0          FUNCTIONAL  0          0          1.13     0        0
521              81.107   6.554    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
54               78.08    5.09     0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
55_1             78.01    5.2      0          FUNCTIONAL  0          0          1.13     0        0
553              88.78    4.669    0          FUNCTIONAL  0          0          1.13     0        0
554              88.191   6.052    0          FUNCTIONAL  0          0          1.13     0        0
555              88.087   7.147    0          FUNCTIONAL  0          0          1.13     0        0
556              87.889   7.878    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
56               77.92    4.78     0          FUNCTIONAL  0          0          1.13     0        0
563              88.55    5.553    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
63               77.84    4.55     0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
64               77.72    4.55     0          FUNCTIONAL  0          0          1.13     0        0
649              87.764   8.215    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
65               77.56    4.71     0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
65_1             77.51    4.76     0          FUNCTIONAL  0          0          1.13     0        0
650              87.664   6.652    0          FUNCTIONAL  0          0          1.13     0        0
652              87.575   7.4      0          FUNCTIONAL  0          0          1.13     0        0
653              87.542   6.066    0          FUNCTIONAL  0          0          1.13     0        0
654              87.374   5.559    0          FUNCTIONAL  0          0          1.13     0        0
;Bobby Pettigrew - 2018.07.06 Levels taken from drawing on page 82 of the Palmer Road SPS Operation and
Maintenance Manual (stop/start elevations on this drawing ignored)
66               72.15    10       0          FUNCTIONAL  0          0          10.8     0        0
666              89.45    4.46     0          FUNCTIONAL  0          0          1.13     0        0
667              89.102   4.95     0          FUNCTIONAL  0          0          1.13     0        0
668              88.828   7.17     0          FUNCTIONAL  0          0          1.13     0        0
669              88.474   7.527    0          FUNCTIONAL  0          0          1.13     0        0
670              88.316   5.833    0          FUNCTIONAL  0          0          1.13     0        0
671              88.154   4.808    0          FUNCTIONAL  0          0          1.13     0        0
672              88.014   5.743    0          FUNCTIONAL  0          0          1.13     0        0
673              87.215   7.378    0          FUNCTIONAL  0          0          1.13     0        0
675              87.173   6.11     0          FUNCTIONAL  0          0          1.13     0        0
676              87.106   7.661    0          FUNCTIONAL  0          0          1.13     0        0
678              86.917   7.796    0          FUNCTIONAL  0          0          1.13     0        0
```

```
68               77.786   5.684    0          FUNCTIONAL  0       0        1.13     0        0
682              88.91    4.769    0          FUNCTIONAL  0       0        1.13     0        0
684              88.587   6.489    0          FUNCTIONAL  0       0        1.13     0        0
685              86.79    6.827    0          FUNCTIONAL  0       0        1.13     0        0
686              86.61    5.797    0          FUNCTIONAL  0       0        1.13     0        0
689              86.5     6.053    0          FUNCTIONAL  0       0        1.13     0        0
690              86.3     4.148    0          FUNCTIONAL  0       0        1.13     0        0
708              89.236   5.428    0          FUNCTIONAL  0       0        1.13     0        0
780              86.18    6.092    0          FUNCTIONAL  0       0        1.13     0        0
781              85.88    5.964    0          FUNCTIONAL  0       0        1.13     0        0
782              85.72    5.335    0          FUNCTIONAL  0       0        1.13     0        0
783              85.56    6.65     0          FUNCTIONAL  0       0        1.13     0        0
796              91.986   3.01     0          FUNCTIONAL  0       0        1.13     0        0
852              91.316   2.836    0          FUNCTIONAL  0       0        1.13     0        0
853              90.648   3.483    0          FUNCTIONAL  0       0        1.13     0        0
859              89.276   3.533    0          FUNCTIONAL  0       0        1.13     0        0
860              89.964   3.814    0          FUNCTIONAL  0       0        1.13     0        0
861              89.771   4.007    0          FUNCTIONAL  0       0        1.13     0        0
864              87.814   3.704    0          FUNCTIONAL  0       0        1.13     0        0
865              88.457   3.198    0          FUNCTIONAL  0       0        1.13     0        0
866              87.659   2.516    0          FUNCTIONAL  0       0        1.13     0        0
877              86.55    4.226    0          FUNCTIONAL  0       0        1.13     0        0
878              87.346   2.829    0          FUNCTIONAL  0       0        1.13     0        0
879              86.06    4.716    0          FUNCTIONAL  0       0        1.13     0        0
880              85.646   3.207    0          FUNCTIONAL  0       0        1.13     0        0
881              85.266   5.048    0          FUNCTIONAL  0       0        1.13     0        0
882              84.88    4.81     0          FUNCTIONAL  0       0        1.13     0        0
883              85.3     5.2      0          FUNCTIONAL  0       0        1.13     0        0
884              85.18    5.799    0          FUNCTIONAL  0       0        1.13     0        0
885              84.96    4.73     0          FUNCTIONAL  0       0        1.13     0        0
886              84.119   6.088    0          FUNCTIONAL  0       0        1.13     0        0
887              83.515   5.341    0          FUNCTIONAL  0       0        1.13     0        0
9001             84.485   2.503    0          FUNCTIONAL  0       0        1.13     0        0
9002             84.272   1.898    0          FUNCTIONAL  0       0        1.13     0        0
9003             84.242   3.237    0          FUNCTIONAL  0       0        1.13     0        0
9004             84.202   3.379    0          FUNCTIONAL  0       0        1.13     0        0
9005             84.174   3.407    0          FUNCTIONAL  0       0        1.13     0        0
9006             84.049   3.024    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9050             86.448   3.477    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9051             86.338   3.464    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9052             85.928   4.09     0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9053             85.518   4.5      0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9054             85.377   4.668    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9055             82.513   4.935    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9056             79.667   3.777    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9057             77.26    4.764    0          FUNCTIONAL  0       0        1.13     0        0
9058             76.564   5.16     0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9059             76.248   5.224    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9060             75.747   4.503    0          FUNCTIONAL  0       0        1.13     0        0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9061             75.632   4.618    0          FUNCTIONAL  0       0        1.13     0        0
924              87.5     3.466    0          FUNCTIONAL  0       0        1.13     0        0
940              83.561   3.541    0          FUNCTIONAL  0       0        1.13     0        0
941              86.783   3.691    0          FUNCTIONAL  0       0        1.13     0        0
942              81.5     5.086    0          FUNCTIONAL  0       0        1.13     0        0
945              81.583   6.307    0          FUNCTIONAL  0       0        1.13     0        0
946              81.379   6.638    0          FUNCTIONAL  0       0        1.13     0        0
948              83.037   4.963    0          FUNCTIONAL  0       0        1.13     0        0
978              79.315   3.967    0          FUNCTIONAL  0       0        1.13     0        0
984              78.73    4.27     0          FUNCTIONAL  0       0        1.13     0        0
985              78.504   4.496    0          FUNCTIONAL  0       0        1.13     0        0
986              78.25    6.061    0          FUNCTIONAL  0       0        1.13     0        0
987              77.94    6.673    0          FUNCTIONAL  0       0        1.13     0        0
988              77.534   6.953    0          FUNCTIONAL  0       0        1.13     0        0
9902             70.782   9.491    0.013      FUNCTIONAL  0       0        1.13     0        0
991              77.5     7.031    0          FUNCTIONAL  0       0        1.13     0        0
996              77.09    4.97     0          FUNCTIONAL  0       0        1.13     0        0
997              76.77    7.306    0          FUNCTIONAL  0       0        1.13     0        0
999              76.51    8.021    0          FUNCTIONAL  0       0        1.13     0        0

[CONDUITS]
;;Name          From Node        To Node          Length     Roughness  InOffset   OutOffset  InitFlow
MaxFlow
;;-------------- ---------------- ---------------- ---------- ---------- ---------- ---------- ----------
----------
1001             997              999              65.75      0.013      76.8       76.53      0
0
1009             1005             1007             49.19      0.013      76.819     76.641     0
0
1010             1007             1008             82.5       0.013      76.641     76.418     0
0
;11.48m of 50cm Clay pipe at Bridge street end.
1011             999              1008             69.86      0.013      76.51      76.42      0
0
1023             1008             1020             91.33      0.013      76.4       75.81      0
0
1025             1020             1022             4.19       0.013      75.78      75.77      0
0
1026             1022             1023             83.38      0.013      75.73      75.4       0
0
1027             1023             1024             98.29      0.013      75.36      74.88      0
0
1028             1024             1025             57.21      0.013      74.84      74.567     0
0
;Bobby Pettigrew - 2017.10.23 Added to reflect drawing 6 of Project No. 1-0004-01 Main Trunk Sewer
Connection
1029             1025             1026             9.92       0.013      74.567     74.469     0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
103              106              68               65.004     0.013      77.864     77.826     0
0
;Bobby Pettigrew - 2017.12.12 Revised to match Project No. 1-0004-01 Main Trunk Sewer Connection and
elevations added
1030             1026             9902             11.5       0.013      74.25      74.02      0
0
;Material assumed. Relined in 1994.
1032             1029             1030             2.72       0.013      75.52      75.49      0
0
;Material assumed. Relined in 1994.
1033             1030             1031             96.95      0.013      75.426     74.959     0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
104              107              106              63.853     0.013      78.11      77.894     0
0
;Material assumed. Relined in 1994.
1045             1042             1029             125.1      0.013      76.666     75.52      0
0
;Material assumed. Relined in 1994.
1046             1044             1045             100.88     0.013      80.958     79.556     0
0
;Material assumed. Relined in 1994.
1048             1045             1042             125.59     0.013      78.776     76.895     0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1050             965              1048             16.98      0.013      70.73      70.7       0
0
;Bobby Pettigrew - 2017.10.23 Revised to match Project No. 1-0004-01 Main Trunk Sewer Connection and
elevations added
1052             1031             1026             49.563     0.013      74.959     74.769     0
0
;Material assumed.
1054_1           2152             9914             698.033    0.013      71.392     70.708     0
0
;Material assumed.
1054_2           9914             1048             7.67       0.013      70.708     70.7       0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
109              112              107              78.995     0.013      78.776     78.14      0
0
1090             1090             1091             68.19      0.013      82.753     82.482     0
0
1091             1091             1092             99.61      0.013      82.482     82.326     0
0
1092             1092             1085             69.02      0.013      82.326     82.281     0
0
;Bobby Pettigrew - 2017.09.27 Elevations dropped from surface to connecting conduits
1093             1093             1090             91.1       0.013      82.805     82.753     0
0
1096             1096             1093             87.11      0.013      83.043     82.805     0
0
1103             1101             1096             79.51      0.013      83.11      83.043     0
0
1116             1111             1114             19.62      0.013      83.39      83.265     0
0
1117             1114             1115             20.11      0.013      83.265     83.351     0
0
;Bobby Pettigrew - 2017.09.27 Inlet elevation dropped to connecting conduit
1118             1115             1116             115.8      0.013      83.351     83.216     0
0
1119             1116             1101             9.22       0.013      83.216     83.11      0
0
1120             1117             1111             42.22      0.013      83.442     83.39      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1179             1175             1176             29.98      0.013      80.89      80.71      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1180             1176             1177             79.65      0.013      80.68      80.58      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1181             1177             1178             96.11      0.013      80.53      80.27      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1182             1178             1179             65.11      0.013      79.73      79.49      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1183             1179             1180             108.08     0.013      79.49      78.96      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
1184             1180             1181             79.83      0.013      78.73      78.5       0
0
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
;Bobby Pettigrew - 2017.09.27 Outlet Elevation on Project 1-0004-01, Drawing 1
1185             1181             1182             85.47      0.013      78.39      78.166     0
0
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
;Bobby Pettigrew - 2017.09.27 Inlet Elevation on Project 1-0004-01, Drawing 1
```

```
1186            1182            950             109.03     0.013     78.093     77.78      0
0
1189            1185            1186            13.09      0.013     82.134     82.092     0
0
1190            1186            1187            125.65     0.013     82.092     81.702     0
0
1193            1187            1190            130.87     0.013     81.702     81.386     0
0
1194            1190            1191            115.64     0.013     81.363     81.018     0
0
;Material and Install Year assumed
;Bobby Pettigrew - 2017.09.28 Elevations estimated based on upstream and downstream sewers
1195            1191            1175            54.64      0.013     81.018     80.89      0
0
;Bobby Pettigrew - 2018.02.13 Outlet lowered to connect to downstream manhole with no negative slope
1196            1192            1193            95.49      0.013     85.134     84.634     0
0
1198            1193            1195            76.45      0.013     84.634     84.36      0
0
1199            1195            1196            65.3       0.013     84.34      84.052     0
0
1202            1196            1199            125.57     0.013     84.052     83.076     0
0
;Bobby Pettigrew - 2018.02.13 Outlet lowered to connect to downstream manhole
1203            1199            1185            122.93     0.013     83.076     82.207     0
0
1206            1202            1192            154.45     0.013     85.609     85.134     0
0
1207            1203            1202            75.86      0.013     85.978     85.609     0
0
1208            1204            1203            121.91     0.013     86.484     85.978     0
0
1209            1205            1204            134.59     0.013     86.999     86.484     0
0
1210            1206            1205            107.84     0.013     87.478     86.999     0
0
1212            1208            1209            86.93      0.013     89.687     89.288     0
0
1213            1209            1210            94.66      0.013     89.288     89.197     0
0
1214            1210            1211            134.14     0.013     88.901     88.407     0
0
1215            1211            1212            89.18      0.013     88.407     87.932     0
0
;pipe in dwg goes to MH 1206 for measurements
1216            1212            1206            145.95     0.013     87.932     87.478     0
0
1220            1216            1217            90.08      0.013     91.318     90.724     0
0
1221            1217            1218            93.83      0.013     90.66      90.385     0
0
1222            1218            1219            102.28     0.013     90.385     90.093     0
0
1223            1219            1220            77.89      0.013     90.093     89.834     0
0
1224            1220            1221            78.86      0.013     89.834     89.517     0
0
1225            1221            1210            85.7       0.013     89.517     89.197     0
0
1226            1222            1216            108.37     0.013     91.909     91.318     0
0
1245            1241            1242            61.38      0.013     92.915     92.659     0
0
1246            1242            1243            94.72      0.013     92.659     92.153     0
0
1247            1243            1244            83.16      0.013     92.409     92.153     0
0
1248            1244            1245            83.4       0.013     92.153     91.842     0
0
1249            1245            1246            75.95      0.013     91.842     91.528     0
0
1250            1246            1247            79.99      0.013     91.528     91.178     0
0
1251            1247            1248            72.93      0.013     91.178     90.873     0
0
1252            1248            1249            103.33     0.013     90.873     90.526     0
0
1255            1249            1252            106.52     0.013     90.538     90.135     0
0
;Missing Data
;Bobby Pettigrew - 2017.09.27 Outlet elevation assumed based on inlet of downstream sewer
1256            1252            1253            75.71      0.013     90.134     89.758     0
0
;Year assumed.
1290            1253            1286            55.58      0.013     89.758     89.538     0
0
;Year assumed.
1291            1286            1287            71.43      0.013     89.538     89.322     0
0
;Year assumed.
1292            1287            1288            71.76      0.013     89.322     89.032     0
0
;Year assumed.
1293            1288            1289            83.27      0.013     89.032     88.776     0
0
;Year assumed.
1294            1289            1290            83.3       0.013     88.776     88.505     0
0
;Year assumed.
1295            1290            1291            74.58      0.013     88.505     87.828     0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1296            1291            1292            87.54      0.013     87.78      87.5       0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1297            1292            1293            79.56      0.013     87.45      87.18      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1298            1293            1294            51.9       0.013     87.12      86.9       0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1299            1294            1295            95.38      0.013     86.84      86.49      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1300            1295            1296            96.54      0.013     86.39      86.08      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1301            1296            1297            92.58      0.013     86.02      85.72      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1302            1297            1298            70.71      0.013     85.66      85.36      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1303            1298            1299            82.44      0.013     85.3       85.02      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1308            1299            1303            97.28      0.013     84.95      84.61      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1311            1303            1306            79.25      0.013     84.55      84.23      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1312            1306            1307            86.55      0.013     84.17      83.84      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1313            1307            1308            89         0.013     83.73      83.4       0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1314            1308            1309            72.06      0.013     83.34      82.69      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1315            1309            1310            120.23     0.013     82.13      81.67      0
0
;Bobby Pettigrew - 2017.09.28 Elevation data taken from as-built data Project No. 1-0220-70
1316            1310            1175            94.43      0.013     81.58      81.12      0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
132             135             112             107.874    0.013     80.151     78.806     0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
133             136             135             69.139     0.013     80.482     80.271     0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
134             137             136             140.981    0.013     81.14      80.512     0
0
1348            1344            1345            32.29      0.013     81.506     81.341     0
0
1349            1345            1346            81.95      0.013     81.341     81.004     0
0
1350            1346            1347            57.1       0.013     81.006     80.856     0
0
1351            1347            1348            103.93     0.013     80.82      80.425     0
0
;Missing data. Install Year assumed from 'M-24-25-5-Dundas_Street_West.pdf'.
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
154             138             157             99.1       0.013     82.445     82.25      0
0
155             158             157             22.035     0.013     81.5       81.104     0
0
156             157             159             12.23      0.013     80.894     80.717     0
0
158             2061            162             76.716     0.013     86.953     85.789     0
0
159             162             163             89.361     0.013     85.789     82.39      0
0
160             163             164             81.787     0.013     84.734     84.11      0
0
161             164             158             79.576     0.013     84.11      81.5       0
0
;Missing TG and Up invert -- Poor drawing
162             165             161             106.012    0.013     88.438     87.161     0
0
;Missing Down invert -- poor drawing
163             166             165             87.294     0.013     89.922     88.438     0
0
164             167             166             89.853     0.013     91.135     89.922     0
0
165             168             167             99.236     0.013     91.638     91.135     0
0
166             169             168             94.22      0.013     92.296     91.647     0
0
167             170             169             44.742     0.013     92.565     92.296     0
0
168             171             172             8.801      0.013     93.494     93.241     0
0
169             172             173             77.379     0.013     93.223     93.028     0
0
170             173             174             107.177    0.013     93.028     92.79      0
0
1703            1705            1131            85.332     0.013     82.311     82.192     0
0
171             174             175             6.973      0.013     92.766     92.79      0
0
1716            1718            1719            75.37      0.013     84.189     83.652     0
0
1717            1719            1720            90.119     0.013     83.652     83.293     0
0
1718            1720            1721            81.367     0.013     83.293     82.82      0
0
1719            1721            1705            94.02      0.013     82.82      82.308     0
0
172             175             170             8.612      0.013     92.711     92.577     0
0
1742            1742            1718            73.315     0.013     84.585     84.189     0
0
```

```
;Connexion to a newer MH
1743            1743            2176            88.734     0.013      84.255     83.55      0
0
1745            1725            1743            91.235     0.013      84.543     84.235     0
0
1746            1725            1742            49.908     0.013      84.543     84.569     0
0
1747            1085            1745            19.02      0.013      82.281     82.134     0
0
1748            1745            1746            99.6       0.013      82.134     82.037     0
0
1749            1746            1747            98.37      0.013      82.037     81.738     0
0
1750            1747            1748            17.76      0.013      81.738     81.659     0
0
1751            1748            1749            146.97     0.013      81.659     81.406     0
0
1752            1749            1750            124.13     0.013      81.406     81.028     0
0
1755            1131            1754            87.146     0.013      82.098     81.967     0
0
1756            1754            1755            72.46      0.013      81.967     81.729     0
0
1757            1755            1756            93.296     0.013      81.699     81.458     0
0
1759            1756            1757            75.369     0.013      81.449     81.324     0
0
1760            1757            1758            64.876     0.013      81.321     81.11      0
0
1761            1758            1759            37.438     0.013      81.11      80.949     0
0
;Missing Info due to Qual. of Drawing
1766            1759            1763            73.764     0.013      80.775     80.546     0
0
;Designed 1963
1772            1763            1768            102.1      0.013      80.098     80.135     0
0
1773            1768            1769            25.818     0.013      79.693     79.428     0
0
1774            1769            1770            12.253     0.013      79.428     78.946     0
0
1775            1770            1771            85.222     0.013      78.946     77.809     0
0
1776            1750            1772            87.59      0.013      81.028     79.98      0
0
1777            1772            1773            74.48      0.013      79.98      78.904     0
0
1778            1773            1771            74.48      0.013      78.904     77.812     0
0
1779            1771            1774            30.07      0.013      77.812     76.675     0
0
1802            1774            1794            138.65     0.013      76.675     75.121     0
0
1803            1794            1795            141.66     0.013      75.121     74.841     0
0
1804            1795            1796            68.82      0.013      74.841     74.758     0
0
;Bobby Pettigrew - 2017.09.27 Outlet elevation dropped to meet connecting conduit
1805            1796            1797            96.75      0.013      74.758     74.697     0
0
1806            1797            1798            85.8       0.013      74.697     74.563     0
0
1807            1798            1799            77.82      0.013      74.563     74.46      0
0
1808            1799            1800            116.8      0.013      74.46      74.347     0
0
1809            1800            1801            94.64      0.013      74.347     74.222     0
0
1821            1801            1812            95.56      0.013      74.222     74.17      0
0
1877            1812            1866            112.46     0.013      74.17      74.124     0
0
1878            1866            1867            96.19      0.013      74.124     74.002     0
0
1879            1867            1868            61.3       0.013      74.002     74.018     0
0
1880            1868            1869            100.34     0.013      74.018     73.765     0
0
1881            1869            1870            91.34      0.013      73.765     73.673     0
0
1882            1870            1871            90.99      0.013      73.673     73.609     0
0
1883            1871            1872            109.07     0.013      73.609     73.512     0
0
1884            1872            1873            107.71     0.013      73.512     73.356     0
0
1885            1873            1874            94.6       0.013      73.448     73.292     0
0
1886            1874            1875            61.24      0.013      73.292     73.243     0
0
1887            1875            1876            102.59     0.013      73.243     73.067     0
0
1888            1593            1877            118.28     0.013      87.435     87.164     0
0
1891            1877            1880            79.84      0.013      87.164     86.978     0
0
1893            1880            1881            163.8      0.013      86.975     86.774     0
0
1905            1881            2286            94.06      0.013      86.774     86.624     0
0
;Material assumed. Relined in 1995.
1912            1898            1899            5.97       0.013      84.28      84.271     0
0
;Material assumed. Relined in 1995.
1925            1899            1913            46.13      0.013      84.247     83.881     0
0
;Material assumed. Relined in 1995.
1926            1913            1914            7.47       0.013      83.872     83.857     0
0
;Material assumed. Relined in 1994.
1927            1914            1915            82.58      0.013      83.814     83.497     0
0
;Material assumed. Relined in 1994.
1929            1915            1916            89.86      0.013      83.479     82.93      0
0
;Material assumed. Relined in 1994.
1931            1916            1917            115.74     0.013      82.903     82.016     0
0
;Material assumed.
;Bobby Pettigrew - 2017.09.27 Outlet elevation assumed to match inlet of downstream conduit
1933            1918            1919            16.98      0.013      81.738     81.186     0
0
;Material assumed. Relined in 1994.
1934            1917            1918            20.26      0.013      81.979     81.711     0
0
;Material assumed. Relined in 1994.
1935            1943            1920            62.32      0.013      81.744     81.482     0
0
;Material assumed. Relined in 1994.
1946            1920            1923            74.54      0.013      81.433     81.497     0
0
;Material assumed. Relined in 1994.
1947            1923            1927            101.63     0.013      81.51      81.232     0
0
;Material assumed. Relined in 1994.
1948            1927            1044            101.08     0.013      81.232     80.967     0
0
;Material assumed.
1949            1919            1931            92.84      0.013      81.186     79.245     0
0
;Material assumed.
1950            1931            1932            73.29      0.013      79.199     77.252     0
0
;Material assumed.
1951            1932            1933            111.33     0.013      77.252     75.197     0
0
1956            1876            1939            103.19     0.013      73.012     72.878     0
0
1957            1939            1940            84.49      0.013      72.878     72.731     0
0
1958            1940            1938            81.88      0.013      72.731     72.649     0
0
1959            1938            1941            49.88      0.013      72.649     72.591     0
0
1960            1941            1942            156.871    0.013      72.591     72.396     0
0
1977            1514            1969            26.24      0.013      87.895     87.883     0
0
1978            1969            1968            93.54      0.013      87.883     87.508     0
0
1979            1968            1593            97.25      0.013      87.508     87.435     0
0
1980            1970            1514            23.55      0.013      87.999     87.895     0
0
2015            2031            2030            89.39      0.013      84.24      84.165     0
0
2016            2029            2032            62.08      0.013      84.066     84.003     0
0
2017            2030            2029            79.31      0.013      84.138     84.084     0
0
2018            2033            2031            80.709     0.013      84.311     84.225     0
0
2019            2034            2033            126.49     0.013      84.393     84.311     0
0
2020            2035            2034            50.1       0.013      84.502     84.391     0
0
2021            2036            2035            101.78     0.013      84.668     84.53      0
0
;Material assumed.
2029            1511            1970            95.1       0.013      88.06      87.998     0
0
2048            161             2061            15.174     0.013      87.161     86.947     0
0
2049            435             2063            48.64      0.013      87.395     82.869     0
0
2056            418             421             39.62      0.013      75.715     74.786     0
0
208             171             212             93.757     0.013      93.497     92.165     0
0
2082            1352            2097            91.5       0.013      79.898     79.706     0
0
2083            2097            2096            86.98      0.013      79.706     79.548     0
0
;Bobby Pettigrew - 2017.09.27 JLR updated FromSanMH from 2069 to 2096
2084            2096            978             114.22     0.013      79.548     79.315     0
0
2085            1348            1352            86.39      0.013      80.39      79.928     0
0
;Missing data. Digitized based on Jason Pettit info. Material & Year assumed.
;Bobby Pettigrew - 2017.09.27 Inlet based on upstream outlet
;Outlet based on constant slope downstream
2086            978             984             149.26     0.013      79.315     78.73      0
0
;Missing data. Digitized based on Jason Pettit info. Material & Year assumed.
;Bobby Pettigrew - 2017.09.27 Inlet based on constant upstream slope
;Outlet based on inlet of downstream pipe
2087            984             985             58.4       0.013      78.73      78.504     0
0
209             212             211             96.364     0.013      92.156     91.693     0
0
2099            654             2105            31.43      0.013      87.374     87.328     0
0
210             211             213             92.94      0.013      91.693     91.474     0
0
;Material and Year assumed.
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2135            2140            44              104.493    0.013      78.65      78.55      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
```

```
2135_1           2140_1           2140             115.537    0.013      78.77      78.65      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2135_2           2140_2           2140_1           95.085     0.013      78.86      78.77      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2135_3           2140_3           2140_2           102.619    0.013      78.96      78.86      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
2135_4           2140_4           2140_3           59.787     0.013      79.02      78.96      0
0
;Bobby Pettigrew - 2018.01.11 Downstream elevation updated as per Project No. 61-5-84 Contract 1 Trunk
Sewer from Moira River at Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction
Chamber
;Bobby Pettigrew - 2017.09.27 Elevations assumed to match upstream and downstream conduits
2136             2141             2282             7.07       0.013      73.426     73.304     0
0
2137             414              427              52.61      0.013      73.981     73.469     0
0
2138             427              2141             7.86       0.013      73.469     73.426     0
0
;Bobby Pettigrew - 2017.09.27 Updated as per Project 1-0004-01
;Connected to pressure main manholes
2140             2276             2277             88.003     0.013      77.46      76.78      0
0
2144             2146             1208             35.85      0.013      89.892     89.777     0
0
;Bobby Pettigrew - 2018.02.13 Outlet lowered to connect to downstream manhole with no negative slope
2145             2148             2147             114.25     0.013      90.853     90.415     0
0
2146             2147             2146             120.55     0.013      90.415     89.937     0
0
;Bobby Pettigrew - 2017.10.23 Elevations based on Project No. Project No. 1-0004-01 Main Trunk Sewer
Connection Drawings
2147             1051             2151             367.249    0.013      73.425     71.557     0
0
;Bobby Pettigrew - 2017.10.23 Elevations based on Project No. Project No. 1-0004-01 Main Trunk Sewer
Connection Drawings
2149             2151             2152             170.11     0.013      71.557     71.392     0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
2152             2154             2155             116.53     0.013      77.898     76.81      0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
2153             2155             289              8.27       0.013      76.81      76.767     0
0
216              213              216              64.62      0.013      91.474     91.303     0
0
2175             2178             2177             73.79      0.013      83.68      83.61      0
0
;Bobby Pettigrew - 2017.09.27 Outlet elevation dropped to connecting conduit
2176             2176             1117             41.8       0.013      83.55      83.442     0
0
2177             2177             2176             85.04      0.013      83.61      83.55      0
0
2178             2032             2180             116.01     0.013      83.9       83.79      0
0
2179             2180             2179             20.74      0.013      83.79      83.76      0
0
2180             2180             2179             20.29      0.013      83.79      83.76      0
0
2181             2179             2178             103.05     0.013      83.76      83.68      0
0
219              216              222              97.02      0.013      91.303     90.98      0
0
2219             685              2217             9.47       0.013      86.79      86.78      0
0
2220             2218             686              8.48       0.013      86.62      86.61      0
0
2221             689              2219             25.97      0.013      86.5       86.46      0
0
2222             2220             781              31.15      0.013      85.95      85.88      0
0
2223             780              2221             32.36      0.013      86.7       86.08      0
0
2224             783              2222             30.39      0.013      85.62      85.57      0
0
2225             2223             883              36.55      0.013      85.41      85.3       0
0
2226             884              2224             28.72      0.013      85.18      85.16      0
0
;Bobby Pettigrew - 2017.09.27 Outlet elevation estimated
2264             676              2259             30.39      0.013      87.106     87.054     0
0
;Bobby Pettigrew - 2019.03.26 Upstream invert based on slope from GIS
2269             2264             948              25.016     0.013      84.885     84.14      0
0
;Bobby Pettigrew - 2017.09.27 Elevations on Project 1-0004-01, Drawing 1/3
2270             2265             2266             171.21     0.013      81.871     81.183     0
0
;Pressure sewer
;Bobby Pettigrew - 2017.09.27 Elevations on Project 1-0004-01, Drawing 1
2271             2267             1182             11.95      0.013      78.897     78.8       0
0
;Bobby Pettigrew - 2017.09.27 Elevations on Project 1-0004-01, Drawing 1
2272             2266             2267             19.57      0.013      81.183     80.88      0
0
2273             2264             2265             7.755      0.013      84.885     81.871     0
0
;Bobby Pettigrew - 2017.09.27 Elevation on Project 1-0004-01, Drawing 3 and 4
2274             2268             2265             64.96      0.013      85.457     85.203     0
0
2277             2062             2273             46.25      0.013      81.5       80.039     0
0
;Pressure sewer.
2278             2063             2062             3.88       0.013      81.651     81.575     0
0
;Pressure sewer. Horizontal bends at 17m and 30.7m..
2279             2273             2275             136.699    0.013      78.794     77.6       0
0
;Pressure pipe.
2280             2275             2276             102.75     0.013      77.585     77.364     0
0
;Pressure pipe. Material and Year assumed.
2281             2277             430              51.91      0.013      76.163     75.996     0
0
;Pressure pipe. Material and Year assumed.
2282             430              2278             25.14      0.013      75.996     75.91      0
0
;Pressure pipe. End connection to validate.
2283             2278             962              68.82      0.013      72.7       72.375     0
0
2284             360              2269             11.2       0.013      81.705     81.686     0
0
;Pressure pipe. Two bends with slope change.
;Bobby Pettigrew - 2017.09.27 Elevation from Project 1-0004-01, Drawing 9
2285             2269             2270             121.278    0.013      81.25      80.007     0
0
;Pressure pipe. Two bends with slope change.
;Bobby Pettigrew - 2017.09.27 Inlet Elevation on Project 1-0004-01, Drawing 8
;Outlet Elevation Estimated based on Project 1-0004-01, Drawing 7
2286             2270             2271             131.83     0.013      80.007     79.285     0
0
;Bobby Pettigrew - 2017.09.27 Outlet Elevation on Project 1-0004-01, Drawing 6
;Inlet Elevation Estimated based on Project 1-0004-01, Drawing 7
2287             2271             2272             116.88     0.013      79.285     78.643     0
0
;Pressure pipe.
;Bobby Pettigrew - 2017.09.27 Inlet Elevation on Project 1-0004-01, Drawing 6
2288             2272             2279             47.92      0.013      77.419     77.126     0
0
;Pressure pipe
2289             2279             2280             56.97      0.013      77.118     74.1       0
0
229              222              231              99.33      0.013      90.98      90.638     0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
2291             406              2282             142.5      0.013      73.304     72.847     0
0
2292             2282_1           1049             165.001    0.013      71.009     70.714     0
0
;Length Assumed
;Bobby Pettigrew - 2017.09.27 Elevations assumed based on upstream and downstream sewers
2339             9006             2032             64.5       0.013      84.049     83.9       0
0
2340             9005             9006             25.12      0.013      84.176     84.049     0
0
235              231              236              94.45      0.013      90.638     89.7       0
0
;Sanitary Forcemain
2390_1           159              DundasFM_3       15.004     0.013      80.8       79.96      0
0
;Sanitary Forcemain
2390_2           DundasFM_1       DundasFM_2       10.407     0.013      82.1       79.95      0
0
;Sanitary Forcemain
2390_3           DundasFM_3       DundasFM_2       10.423     0.013      79.96      79.95      0
0
;Sanitary Forcemain
2390_5           DundasFM_1       67               641.252    0.013      82.1       79.7       0
0
;Ivan DZeparoski - 2018.08.16 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
273              159              284              84.3       0.013      80.693     78.641     0
0
274              284              285              15.36      0.013      78.388     78.346     0
0
275              285              286              115.03     0.013      78.34      77.876     0
0
276              286              287              108.16     0.013      77.876     77.114     0
0
277              287              288              159.2      0.013      75.987     75.743     0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
278              289              290              141.8      0.013      75.377     75.255     0
0
283              288              289              123.47     0.013      75.743     75.377     0
0
289              300              301              90.24      0.013      92.784     92.263     0
0
290              301              211              85.74      0.013      92.263     91.73      0
0
291              302              303              53.08      0.013      93.43      93.141     0
0
292              303              300              65.59      0.013      93.141     92.784     0
0
3300             2300             1291             20.7       0.013      88.2       88.1       0
0
3301             2301             2300             164.79     0.013      88.8       88.2       0
0
3302             2302             2301             20.13      0.013      88.9       88.8       0
0
3303             2303             2302             86.1       0.013      89.2       88.9       0
0
3304             2304             2303             10.6       0.013      89.2       89.17      0
0
3305             2305             2304             110.1      0.013      89.6       89.2       0
0
3306             2306             2305             128.99     0.013      90.1       89.6       0
0
3307             2307             2306             114.39     0.013      90.45      90.08      0
0
3309             2309             2307             162.29     0.013      91         90.46      0
0
3310             2310             2309             102.5      0.013      91.36      91         0
0
3311             2311             2310             60.2       0.013      91.6       91.36      0
0
```

```
;Bobby Pettigrew - 2018.03.12 Forcemain updated as per Drawings in Appendix D of the Cannifton Secondary
Plan Servicing Review and Update, Greer Galloway Group, Nov 2013
3312            2312            2311            78.8        0.013       91.99       91.31       0
0
;Drop Connection at MH 2312
3313            2313            2312            106.69      0.013       93.94       93.39       0
0
3314            2314            2313            104.99      0.013       94.55       93.94       0
0
3315            2315            2314            105.49      0.013       94.98       94.55       0
0
3317            2317            2315            108.89      0.013       95.2        94.98       0
0
;Drop Connection at MH 2318
3318            2318            2317            102.1       0.013       97.15       95.2        0
0
;Drop Connection at MH 2318
3319            2319            2318            103.8       0.013       97.64       97.15       0
0
3320            2320            2319            103.8       0.013       97.85       97.64       0
0
3321            2321            2320            104.99      0.013       98.07       97.85       0
0
;Forcemain under River. There is one 450mm and two 250mm pipes
3339_10         2339            2339_2          13.043      0.013       92.646      90.6        0
0
3339_11         2339            2339_1          16.978      0.013       92.75       90.6        0
0
3339_12         2339            2339_3          18.28       0.013       92.577      90.6        0
0
;Forcemain under River. There is one 450mm and two 250mm pipes
3339_2          2340_4          2339_2          113.875     0.013       90.7        90.6        0
0
3339_3          2340_2          2340_5          17.799      0.013       93.515      90.7        0
0
;Forcemain under River. There is one 450mm and two 250mm pipes
3339_5          2340            2340_4          29.845      0.013       93.52       90.7        0
0
3339_6          2340_1          2340_3          17.932      0.013       93.514      90.7        0
0
3339_8          2340_5          2339_3          121.564     0.013       90.7        90.6        0
0
3339_9          2340_3          2339_1          116.401     0.013       90.7        90.6        0
0
;Bobby Pettigrew - 2017.09.27 Elevations based on upstream outlet
3340            2341            2340            130.19      0.013       93.87       93.58       0
0
3341            2342            2341            124.99      0.013       94.15       93.87       0
0
3342            2343            2342            100.1       0.013       94.36       94.16       0
0
3343            2344            2343            71.8        0.013       94.51       94.37       0
0
3344            2345            2344            57          0.013       94.6        94.5        0
0
3345            2346            2345            80          0.013       94.79       94.6        0
0
3346            2347            2346            129.69      0.013       95.25       94.79       0
0
3347            2348            2347            109.99      0.013       95.56       95.3        0
0
;Connects to 200mm forcemain at MH 2349
3348            2349            2348            18.8        0.013       95.74       95.61       0
0
3364            2363            553             124.7       0.013       89.17       88.86       0
0
3365            2364            2363            21.8        0.013       89.3        89.2        0
0
3366            2365            2364            119.99      0.013       89.63       89.33       0
0
3367            2366            2365            119.99      0.013       89.93       89.63       0
0
3368            2367            2366            139.99      0.013       90.29       89.93       0
0
3369            2368            2367            20          0.013       90.37       90.32       0
0
3370            2369            2368            54.6        0.013       90.53       90.4        0
0
3371            2370            2369            117.19      0.013       90.83       90.54       0
0
3372            2371            2370            13.1        0.013       90.89       90.83       0
0
3373            2372            2371            119.99      0.013       91.22       90.92       0
0
3374            2373            2372            119.99      0.013       91.53       91.23       0
0
3375            2374            2373            119.99      0.013       91.83       91.53       0
0
3376            2375            2374            119.99      0.013       92.14       91.84       0
0
3377            2376            2375            119.99      0.013       92.44       92.14       0
0
3378            2377            2376            119.99      0.013       92.74       92.44       0
0
3379            2378            2377            119.99      0.013       93.05       92.75       0
0
3380            2379            2378            125.59      0.013       93.37       93.05       0
0
3381            2380            2379            9.42        0.013       93.42       93.4        0
0
3382            2381            2380            132.69      0.013       93.78       93.45       0
0
3383            2382            2381            96.09       0.013       94.08       93.84       0
0
3384            2383            2382            96.09       0.013       94.32       94.08       0
0
3385            2384            2383            104.09      0.013       94.64       94.38       0
0
3386            2385            2384            104.09      0.013       94.91       94.65       0
0
3387            2386            2385            115.76      0.013       95.27       94.98       0
0
3388            2387            2386            119.99      0.013       95.58       95.28       0
0
3389            2388            2387            119.99      0.013       95.88       95.58       0
0
3390            2389            2388            119.99      0.013       96.19       95.89       0
0
3391            2390            2389            119.99      0.013       96.49       96.19       0
0
3392            2391            2390            144.49      0.013       96.86       96.5        0
0
3393            2392            2391            28.8        0.013       97.01       96.93       0
0
3394            2393            2392            96.39       0.013       98.13       97.89       0
0
3395            2394            2393            79.99       0.013       98.33       98.13       0
0
3396            2395            2394            76.99       0.013       98.53       98.34       0
0
3398            2397            2385            121.99      0.013       95.36       95.06       0
0
3399            2398            2397            119.99      0.013       95.67       95.37       0
0
3400            2399            2398            119.99      0.013       95.97       95.67       0
0
3401            2400            2399            119.99      0.013       96.27       95.97       0
0
3402            2401            2400            119.99      0.013       96.65       96.35       0
0
3403            2402            2401            119.99      0.013       96.95       96.65       0
0
;Bobby Pettigrew - 2018.03.12 Forcemain updated as per Drawings in Appendix D of the Cannifton Secondary
Plan Servicing Review and Update, Greer Galloway Group, Nov 2013
3500            2339            2312            37.7        0.013       92.449      92.387      0
0
3502            2474            2475            104.54      0.013       75.543      75.2        0
0
3503            2475            2476            107.04      0.013       75.17       74.827      0
0
3504            2476            2477            74.96       0.013       74.767      74.555      0
0
3505            2477            413             8.94        0.013       74.495      74.485      0
0
;No profile available for MH 2453
;Bobby Pettigrew - 2017.09.27 Outlet elevation estimated
3690            2219            2453            52.5        0.013       86.46       86.38       0
0
;Material and Year assumed.
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
39              44              45              66.93       0.013       78.55       78.48       0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
391             290             401             105.8       0.013       75.255      75.072      0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
392             401             402             47.22       0.013       75.072      74.935      0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
393             402             403             118.37      0.013       74.7        74.371      0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
394             403             404             99.75       0.013       74.371      74.066      0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
395             404             405             49.47       0.013       73.64       73.457      0
0
;Info missing. Install Year assumed from 'N-11-2-2-Dundas_Street_West_Trunk_Sewer.pdf'.
396             405             406             42.11       0.013       73.457      73.304      0
0
;Repaired in 2012
400             411             406             80.42       0.013       73.679      73.155      0
0
;Repaired in 2012
401             409             411             96.6        0.013       74.109      73.679      0
0
403             413             414             65.84       0.013       74.423      73.981      0
0
4035            9004            9005            29.29       0.013       84.203      84.174      0
0
4036            9003            9004            44.75       0.013       84.243      84.202      0
0
4037            9002            9003            32.73       0.013       84.424      84.242      0
0
4038            9001            9002            40.2        0.013       84.485      84.272      0
0
;Repaired in 2012
408             421             409             115.7       0.013       74.786      74.109      0
0
412             424             425             136.37      0.013       75.325      74.164      0
0
413             425             426             121.32      0.013       74.164      73.451      0
0
414             426             427             44.23       0.013       73.469      73.451      0
0
415             428             429             103.51      0.013       76.986      75.788      0
0
;Bobby Pettigrew - 2017.09.27 Updated as per Project 1-0004-01 Drawing 10
417             429             424             144.186     0.013       75.788      75.326      0
0
418             431             419             17.55       0.013       75.968      75.856      0
0
419             432             431             127.64      0.013       76.602      75.956      0
0
420             433             432             103.65      0.013       77.584      76.584      0
0
421             434             433             4.56        0.013       77.209      77.157      0
0
;Bobby Pettigrew - 2018.07.05 Added to incorporate overflow path into model
```

```
422             433             428             84.141     0.013      77.898     77.239     0
0
423             236             435             67.54      0.013      89.7       87.401     0
0
;Ivan DZeparoski - 2018.09.05 Pipe size according to as-build dwg 14 (Catherine Street from sta 0+424.4 to
sta. 0+484.70, dated June 1983) by Gore & Storrie Limited
424             2063            436             52.61      0.013      81.574     80.04      0
0
425             436             437             52.72      0.013      79.224     78.075     0
0
;Ivan DZeparoski - 2018.09.05 Pipe size according to as-build dwg 13 (Catherine Street from sta 0+306.4 to
sta. 0+424.40, dated June 1983) by Gore & Storrie Limited
426             437             438             5.25       0.013      78.075     77.919     0
0
;Ivan DZeparoski - 2018.09.05 Pipe inlet elevation estimated from as-build dwg 13 (Catherine Street from
sta 0+306.4 to sta. 0+424.40, dated June 1983) by Gore & Storrie Limited
427             437             439             110.41     0.013      76.85      76.724     0
0
428             439             418             126.91     0.013      76.724     76.109     0
0
;Ivan DZeparoski - 2018.09.05 Pipe size according to as-build dwg 13 (Catherine Street from sta 0+306.4 to
sta. 0+424.40, dated June 1983) by Gore & Storrie Limited
429             438             434             76.25      0.013      77.837     77.172     0
0
;Not sure if it's been relined.
436             446             447             45.34      0.013      80.388     80.175     0
0
;Not sure if it's been relined.
437             447             448             98.98      0.013      80.175     79.629     0
0
438             460             449             131.3      0.013      77.486     77.084     0
0
;Ivan DZeparoski - 2018.09.05 Pipe outlet elevation estimated from as-build dwg 13 (Catherine Street from
sta 0+306.4 to sta. 0+424.40, dated June 1983) by Gore & Storrie Limited
439             449             437             94.34      0.013      77.084     76.85      0
0
442             448             451             80.37      0.013      79.629     78.044     0
0
443             451             452             165.22     0.013      78.056     77.273     0
0
444             452             434             31.25      0.013      77.255     77.221     0
0
445             451             453             79.06      0.013      78.044     77.992     0
0
446             453             454             106.31     0.013      77.992     77.517     0
0
447             454             428             91.75      0.013      77.517     76.986     0
0
;Bobby Pettigrew - 2018.07.24 Added to incorporate overflow path into model
448             360             455             93.986     0.01       81.287     80.373     0
0
;Bobby Pettigrew - 2018.07.24 Added to incorporate overflow path into model
449             456             455             400        0.01       80.921     80.373     0
0
;Material and Year assumed.
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
45              45              51              119.227    0.013      78.33      78.21      0
0
;Bobby Pettigrew - 2018.07.24 Added to incorporate overflow path into model
450             456             447             86.399     0.01       80.921     80.458     0
0
;Bobby Pettigrew - 2018.07.24 Added to incorporate overflow path into model
451             455             457             31.923     0.01       80.104     79.376     0
0
452             457             458             53.99      0.013      78.032     77.727     0
0
453             458             459             13.79      0.013      80.168     80.144     0
0
454             458             460             136.33     0.013      78.974     77.486     0
0
;Bobby Pettigrew - 2018.07.05 Added to incorporate overflow path into model
455             459             461             52.008     0.013      78.849     78.681     0
0
;Bobby Pettigrew - 2018.07.05 Added to incorporate overflow path into model
456             461             462             22.503     0.013      78.681     78.58      0
0
457             463             462             15.27      0.013      78.571     78.51      0
0
458             464             451             69.17      0.013      78.346     78.044     0
0
459             463             464             60.8       0.013      78.51      78.328     0
0
460             462             465             79.3       0.013      78.58      78.349     0
0
461             465             453             127.23     0.013      78.425     77.992     0
0
465             469             468             14.72      0.013      78.593     78.446     0
0
468             468             473             90.95      0.013      78.446     78.166     0
0
469             473             457             93.53      0.013      78.166     78.032     0
0
474             477             478             100.45     0.013      79.733     79.339     0
0
;Bobby Pettigrew - 2017.09.27 Elevations dropped to match upstream and downstream conduits
475             478             469             64.16      0.013      79.339     78.593     0
0
476             479             480             74.54      0.013      82.089     81.513     0
0
477             480             481             41.57      0.013      81.513     81.382     0
0
478             481             477             140.31     0.013      80.303     79.733     0
0
499             501             502             39.27      0.013      78.903     78.83      0
0
500             502             503             109.56     0.013      78.83      78.547     0
0
502             503             465             13.81      0.013      79.661     79.474     0
0
;Missing Diameter
505             507             508             113.08     0.013      79.92      79.575     0
0
5050            419             2474            37.63      0.013      75.963     75.603     0
0
506             508             506             83.79      0.013      79.575     79.322     0
0
507             506             501             73.19      0.013      79.322     78.903     0
0
;Material and Year assumed.
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
51              51              54              127.81     0.013      78.21      78.08      0
0
510             511             512             143.56     0.013      80.942     80.334     0
0
511             512             507             131.07     0.013      80.344     79.975     0
0
512             513             512             70.35      0.013      80.806     80.437     0
0
513             514             513             46.63      0.013      81.034     80.806     0
0
515             516             511             36.787     0.013      81.162     80.894     0
0
520             521             514             7.7        0.013      81.107     81.077     0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
53_1            54              55_1            78.892     0.013      78.08      78.01      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
53_2            55_1            56              83.9       0.013      78.01      77.92      0
0
551             554             555             83.51      0.013      88.191     88.087     0
0
552             555             556             88.07      0.013      88.087     87.889     0
0
558             553             563             79.49      0.013      88.78      88.58      0
0
560             563             554             19.2       0.013      88.55      88.51      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
60              56              63              82.99      0.013      77.92      77.84      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
61              63              64              118.158    0.013      77.84      77.72      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
62              64              65              95.04      0.013      77.72      77.63      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20 - NOT GEOREFERENCED
63              65_1            66              3.755      0.013      77.51      77.38      0
0
;Bobby Pettigrew - 2018.03.23 Updated from drawings for Dundas Street West Sanitary Trunk Sewer, June
2013, ENG2014-20
63_1            65              65_1            6.219      0.013      77.57      77.56      0
0
;Bobby Pettigrew - 2017.10.13 Connectivity updated to reflect drawings
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
64              68              66              39.682     0.013      77.786     77.561     0
0
646             556             649             102.38     0.013      87.889     87.764     0
0
647             649             650             100.67     0.013      87.764     87.664     0
0
649             650             652             96.46      0.013      87.813     87.575     0
0
650             652             653             22.38      0.013      87.575     87.542     0
0
651             653             654             78.78      0.013      87.542     87.374     0
0
663             666             667             85.45      0.013      89.45      89.184     0
0
664             667             668             99.97      0.013      89.102     88.828     0
0
665             668             669             92.28      0.013      88.828     88.538     0
0
666             669             670             99.14      0.013      88.474     88.319     0
0
667             670             671             105.98     0.013      88.316     88.154     0
0
668             671             672             98.27      0.013      88.154     88.014     0
0
669             672             650             99.11      0.013      88.014     87.813     0
0
;Bobby Pettigrew - 2017.09.27 JLR Updated Inlet node from 654
670             2105            673             103.15     0.013      87.328     87.215     0
0
672             673             675             30.54      0.013      87.215     87.173     0
0
673             675             676             73.04      0.013      87.173     87.106     0
0
;Bobby Pettigrew - 2017.09.27 Inlet elevation estimated
675             2259            678             79.43      0.013      87.054     86.917     0
0
680             708             682             125.32     0.013      89.236     88.91      0
0
681             682             684             64.69      0.013      88.91      88.587     0
0
682             684             678             64.35      0.013      88.587     88.429     0
0
683             678             685             74.03      0.013      86.92      86.79      0
0
684             2217            2218            59.71      0.013      86.78      86.62      0
0
```

```
688              686              689              51.3       0.013      86.61      86.5       0
0
;No profile found at MH 2453
;Bobby Pettigrew - 2017.09.27 Inlet elevation estimated
689              2453             690              44.63      0.013      86.38      86.31      0
0
779              690              780              62.65      0.013      86.3       86.18      0
0
780              2221             2220             74.94      0.013      86.08      85.95      0
0
781              781              782              94.97      0.013      85.88      85.72      0
0
782              782              783              66.75      0.013      85.72      85.56      0
0
854              796              852              61.99      0.013      91.986     91.316     0
0
855              852              853              67.45      0.013      91.316     90.648     0
0
860              853              860              61.9       0.013      90.648     89.964     0
0
861              860              861              18.19      0.013      89.964     89.771     0
0
862              861              859              44.34      0.013      89.771     89.278     0
0
866              859              865              72.57      0.013      89.276     88.457     0
0
867              865              864              52.52      0.013      88.457     87.814     0
0
;Bobby Pettigrew - 2018.02.13 Outlet elevation changed to reflect downstream connection manhole
868              864              866              8.24       0.013      87.814     87.659     0
0
880              866              878              32.03      0.013      87.659     87.346     0
0
881              878              877              61.99      0.013      87.346     86.55      0
0
882              877              879              62.56      0.013      86.55      86.06      0
0
883              879              880              87.33      0.013      86.06      85.646     0
0
884              880              881              71.53      0.013      85.646     85.266     0
0
885              881              882              79.05      0.013      85.266     84.918     0
0
886              2222             2223             52.87      0.013      85.57      85.41      0
0
887              883              884              67.25      0.013      85.3       85.18      0
0
888              2224             885              56.96      0.013      85.16      84.96      0
0
889              885              882              31.07      0.013      84.96      84.88      0
0
890              882              886              102.88     0.013      84.917     84.119     0
0
891              886              887              102.06     0.013      84.119     83.515     0
0
892              887              479              115.35     0.013      83.515     82.601     0
0
9011             1051             9915             142.254    0.013      76.26      74.5       0
0
9012             1051             9916             136.159    0.013      76.26      74.5       0
0
9013             1051             WWTP             14.95      0.013      73.425     73.42      0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9014             2286             9050             33.644     0.013      86.624     86.504     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9015             9050             9051             9.988      0.013      86.448     86.388     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9016             9051             9052             60.751     0.013      86.338     85.978     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9017             9052             9053             59.839     0.013      85.928     85.568     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9018             9053             9054             13.88      0.013      85.518     85.427     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9019             9054             9055             37.931     0.013      85.377     84.689     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9020             9055             9056             57.534     0.013      82.513     81.473     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9021             9056             9057             20.519     0.013      79.667     79.302     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9022             9057             9058             34.669     0.013      77.26      76.641     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9023             9058             9059             38.062     0.013      76.564     76.298     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9024             9059             9060             71.342     0.013      76.248     75.797     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9025             9060             9061             9.587      0.013      75.747     75.682     0
0
;Bobby Pettigrew - 2017.11.21 Entered based on data from PDF drawings of Quinte Healthcare Corporation
Belleville General Hospital Infrastructure Improvements April 2004, GD Jewel Engineering
9026             9061             1873             15.802     0.013      75.632     75.51      0
0
;Bobby Pettigrew - 2017.12.12 Revised to match Project No. 1-0004-01 Main Trunk Sewer Connection and
elevations added - control rule added to close sewer
9027             1048             1049             12.688     0.013      70.7       70.69      0
0
;Bobby Pettigrew - 2017.12.12 Revised to match Project No. 1-0004-01 Main Trunk Sewer Connection and
elevations added - drawings show to be blocked but not completed
9028             1026             Front_St_PS_Overflow_1 19.114 0.013   75.419     74         0
0
;Bobby Pettigrew - 2017.12.12 Revised to match Project No. 1-0004-01 Main Trunk Sewer Connection and
elevations added
9029             9902             1049             8.516      0.013      70.782     70.69      0
0
;Assumed old 250mm pipe was removed.
;Elevation on Project 1-0004-01, Drawing 4
932              924              2268             116.869    0.013      87.5       86.2       0
0
946              924              941              91.63      0.013      87.981     86.783     0
0
947              941              940              85.53      0.013      86.783     83.561     0
0
948              940              942              69.95      0.013      83.561     81.5       0
0
949              942              521              90.29      0.013      81.5       81.15      0
0
952              945              946              66.845     0.013      81.583     81.379     0
0
953              946              516              82.635     0.013      81.379     81.165     0
0
955              948              945              86.829     0.013      83.037     81.753     0
0
;Unable to read Invert
957              950              951              144.28     0.013      77.69      76.83      0
0
;Unable to read Invert
958              951              952              82.47      0.013      76.83      76.5       0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
959              952              953              155.61     0.013      76.34      75.95      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
960              953              954              83.4       0.013      75.8       75.63      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
961              954              955              89.33      0.013      75.5       75.18      0
0
;Unable to read Invert.
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
962              955              956              152.13     0.013      75.04      74.49      0
0
;Unable to read Invert.
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
963              956              957              115.73     0.013      74.54      74.23      0
0
;Unable to read Invert. Valve chamber on this pipe?
964_1            957              2280             34.313     0.013      74.14      74.072     0
0
;Unable to read Invert. Valve chamber on this pipe?
964_2            2280             958              39.979     0.013      74.072     73.92      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
965              958              959              111.75     0.013      73.79      73.51      0
0
;Unable to read Invert.
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
966              959              960              161.46     0.013      73.41      73         0
0
;Unable to read Invert.
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
967              960              961              109.72     0.013      72.84      72.58      0
0
;Unable to read Invert.
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
;Bobby Pettigrew - 2017.09.27 Outlet Elevation as per Project 1-0004-01 Drawing 10
968              961              962              41.82      0.013      72.45      72.33      0
0
;Unable to read Invert.
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
;Bobby Pettigrew - 2017.09.27 Inlet Elevation as per Project 1-0004-01 Drawing 10
969              962              963              151.36     0.013      71.75      71.31      0
0
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
970              963              964              93.15      0.013      71.31      71.15      0
0
;Unable to read Invert
;Bobby Pettigrew - 2017.09.27 Elevation data taken from as-built data Project No. 1-0220-70
971              964              965              154.29     0.013      71.15      70.75      0
0
988              985              986              56.31      0.013      78.54      78.31      0
0
989              986              987              100.03     0.013      78.25      78.05      0
0
990              987              3000             49.5       0.013      77.94      77.88      0
0
990_1            3000             3000A            8.476      0.013      77.83      77.81      0
0
;Bobby Pettigrew - 2017.09.28 Added based on information in the Belleville WPCP East End Pumping Station
Upgrade Projet Study Report (CH2M Hill Engineering, March 1994)
9902             1933             1942             126.35     0.013      72.74      72.44      0
0
;Bobby Pettigrew - 2018.01.10 Upstream Nodes Information from AECOM Front Street Sewage Pumping Station
Upgrades Contract No. 07-19, January 2010
;Bobby Pettigrew - 2018.01.10 Elevations and approximate route from drawing set for Ontario Water
Commission Project 61-5-84, February 1962
```

```
9904            1050_1          905             518.159   0.013     75.55     75.46     0
0
;Bobby Pettigrew - 2017.11.17 Elevations and approximate route from drawing set for Ontario Water
Commission Project 1-0004-66, August 1969
9905            905             1051            560.512   0.013     75.45     73.765    0
0
;Bobby Pettigrew - 2018.01.10 Elevations and approximate route from drawing set for Ontario Water
Commission Project 61-5-84, February 1962
9906_1          902a            902             51.968    0.013     75.286    75.276    0
0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
9906_2          1050_2          902a            4.87      0.013     74.675    75.286    0
0
;Bobby Pettigrew - 2017.11.17 Elevations and approximate route from drawing set for Ontario Water
Commission Project 61-5-84, February 1962
9907            902             1051            1027.205  0.013     75.276    74.182    0
0
;Bobby Pettigrew - 2017.10.13 Updated as per Project No 08-3-7388 Drawings in Palmer Road PS Operations
and Maintenance Manual August 2013
9908            66              Dundas_Street_PS_Overflow_1 35.834 0.013 78.804   77        0
0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
9909            1050            1050_2          0.958     0.013     74.447    74.446    0
0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
9910            1050            1050_1          0.986     0.013     74.447    74.446    0
0
;Bobby Pettigrew - 2018.01.10 Information from AECOM Front Street Sewage Pumping Station Upgrades Contract
No. 07-19, January 2010
9911            1050            9914            12.307    0.013     75.2      71.858    0
0
;Bobby Pettigrew - 2018.01.11 As per Project No. 61-5-84 Contract 1 Trunk Sewer from Moira River at Dundas
Street East to College STreet at Fahey Street, Drawing 12 Junction Chamber
9912            2282_2          Dundas_Street_Outfall 23.053 0.013    73.304    72.5      0
0
;Sanitary Forcemain
9914            138             67              562.911   0.013     82.381    79.7      0
0
9915            EastFM_1        9915            2.74      0.013     76.63     74.678    0
0
9916            EastFM_2        9916            3.048     0.013     76.63     74.678    0
0
992_1           3000A           988             69.4      0.013     77.76     77.61     0
0
992_2           988             991             47.074    0.013     77.534    77.5      0
0
998             991             996             91.31     0.013     77.5      77.13     0
0
999             996             997             87.42     0.013     77.09     76.77     0
0

[PUMPS]
;;Name          From Node       To Node         Pump Curve      Status   Startup  Shutoff
;;-------------- ---------------- ---------------- ---------------- -------- -------- --------
;Bobby Pettigrew - 2018.07.06 Start/Stop levels and pump details as supplied from OCWA via USB on October
13, 2017
Dundas_1        66              67              100_NT3202.090MT ON      2        1.1
;Bobby Pettigrew - 2018.07.06 Start/Stop levels and pump details as supplied from OCWA via USB on October
13, 2017
Dundas_2        66              67              100_NT3202.090MT ON      2.5      1.5
;Assumed as standby
;Bobby Pettigrew - 2018.07.06 Start/Stop levels and pump details as supplied from OCWA via USB on October
13, 2017
Dundas_3        66              67              100_NT3202.090MT ON      10       9
East_PS_1       1942            EastFM_1        K4D1-604400_#1   ON      1.25     1.08
East_PS_2       1942            EastFM_1        K4D1-604400_#2   ON      1.4      1.17
East_PS_3       1942            EastFM_2        K4D1-604400_#3   ON      1.7      1.38
East_PS_4       1942            EastFM_2        K4D1-604400_#4   ON      1.7      1.25
;Bobby Pettigrew - 2018.01.11 Pump start stop elevations from SCADA data photo IMG_1358 supplied by OCWA
via USB on October 13, 2017
;Bobby Pettigrew - 2018.01.10 Pump information from AECOM Front Street Sewage Pumping Station Operations
and Maintenance Manual June 2010
FrontSt#1       1049            1050_1          100_D5731CW      ON      1.7      1.3
;Bobby Pettigrew - 2018.01.11 Pump start stop elevations from SCADA data photo IMG_1358 supplied by OCWA
via USB on October 13, 2017
;Bobby Pettigrew - 2018.01.10 Pump information from AECOM Front Street Sewage Pumping Station Operations
and Maintenance Manual June 2010
FrontSt#2       1049            1050_2          100_NT3301LT3    ON      1.95     1.4
;Bobby Pettigrew - 2018.01.11 Pump start stop elevations from SCADA data photo IMG_1358 supplied by OCWA
via USB on October 13, 2017
;Bobby Pettigrew - 2018.01.10 Pump information from AECOM Front Street Sewage Pumping Station Operations
and Maintenance Manual June 2010
FrontSt#3       1049            1050_1          100_D5731CW      ON      2.1      1.5
;Bobby Pettigrew - 2018.01.11 Pump start stop elevations from SCADA data photo IMG_1358 supplied by OCWA
via USB on October 13, 2017
;Bobby Pettigrew - 2018.01.10 Pump information from AECOM Front Street Sewage Pumping Station Operations
and Maintenance Manual June 2010
FrontSt#4       1049            1050            100_NT3315LT3_626 ON     2.2      1.6

[ORIFICES]
;;Name          From Node       To Node         Type         Offset     Qcoeff     Gated    CloseTime
;;-------------- ---------------- ---------------- ------------ ---------- ---------- -------- ----------
;Bobby Pettigrew - 2018.01.11 Flapgate as per Project No. 61-5-84 Contract 1 Trunk Sewer from Moira River
at Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction Chamber
2282_c          2282            2282_2          SIDE         73.533     0.65       YES      0
;Bobby Pettigrew - 2018.01.11 Sluice gate orifice as per Project No. 61-5-84 Contract 1 Trunk Sewer from
Moira River at Dundas Street East to College STreet at Fahey Street, Drawing 12 Junction Chamber
9913            2282            2282_1          SIDE         71.323     0.65       NO       0

[WEIRS]
;;Name          From Node       To Node         Type         CrestHt    Qcoeff     Gated    EndCon
EndCoeff   Surcharge  RoadWidth  RoadSurf   Coeff. Curve
;;-------------- ---------------- ---------------- ------------ ---------- ---------- -------- -------- --
-------- ---------- ---------- ---------- ----------------
3339_1          2340            2340_2          TRANSVERSE   93.773     1.67       NO       0        0
NO
3339_4          2340            2340_1          TRANSVERSE   93.841     1.67       NO       0        0
NO
```

```
[XSECTIONS]
;;Link          Shape        Geom1            Geom2      Geom3      Geom4      Barrels    Culvert
;;-------------- ------------ ---------------- ---------- ---------- ---------- ---------- ----------
1001            CIRCULAR     0.525            0          0          0          1
1009            CIRCULAR     0.5              0          0          0          1
1010            CIRCULAR     0.5              0          0          0          1
1011            CIRCULAR     0.525            0          0          0          1
1023            CIRCULAR     0.5              0          0          0          1
1025            CIRCULAR     0.5              0          0          0          1
1026            CIRCULAR     0.5              0          0          0          1
1027            CIRCULAR     0.5              0          0          0          1
1028            CIRCULAR     0.5              0          0          0          1
1029            CIRCULAR     0.6              0          0          0          1
103             CIRCULAR     0.375            0          0          0          1
1030            CIRCULAR     0.6              0          0          0          1
1032            CIRCULAR     0.525            0          0          0          1
1033            CIRCULAR     0.525            0          0          0          1
104             CIRCULAR     0.375            0          0          0          1
1045            CIRCULAR     0.525            0          0          0          1
1046            CIRCULAR     0.45             0          0          0          1
1048            CIRCULAR     0.45             0          0          0          1
1050            CIRCULAR     1.05             0          0          0          1
1052            CIRCULAR     0.6              0          0          0          1
1054_1          CIRCULAR     1.5              0          0          0          1
1054_2          CIRCULAR     1.5              0          0          0          1
109             CIRCULAR     0.375            0          0          0          1
1090            CIRCULAR     0.6              0          0          0          1
1091            CIRCULAR     0.6              0          0          0          1
1092            CIRCULAR     0.6              0          0          0          1
1093            CIRCULAR     0.6              0          0          0          1
1096            CIRCULAR     0.6              0          0          0          1
1103            CIRCULAR     0.6              0          0          0          1
1116            CIRCULAR     0.6              0          0          0          1
1117            CIRCULAR     0.6              0          0          0          1
1118            CIRCULAR     0.6              0          0          0          1
1119            CIRCULAR     0.6              0          0          0          1
1120            CIRCULAR     0.6              0          0          0          1
1179            CIRCULAR     1.05             0          0          0          1
1180            CIRCULAR     1.05             0          0          0          1
1181            CIRCULAR     1.05             0          0          0          1
1182            CIRCULAR     1.05             0          0          0          1
1183            CIRCULAR     1.05             0          0          0          1
1184            CIRCULAR     1.05             0          0          0          1
1185            CIRCULAR     1.05             0          0          0          1
1186            CIRCULAR     1.05             0          0          0          1
1189            CIRCULAR     0.75             0          0          0          1
1190            CIRCULAR     0.75             0          0          0          1
1193            CIRCULAR     0.75             0          0          0          1
1194            CIRCULAR     0.75             0          0          0          1
1195            CIRCULAR     0.75             0          0          0          1
1196            CIRCULAR     0.675            0          0          0          1
1198            CIRCULAR     0.675            0          0          0          1
1199            CIRCULAR     0.675            0          0          0          1
1202            CIRCULAR     0.675            0          0          0          1
1203            CIRCULAR     0.675            0          0          0          1
1206            CIRCULAR     0.675            0          0          0          1
1207            CIRCULAR     0.675            0          0          0          1
1208            CIRCULAR     0.675            0          0          0          1
1209            CIRCULAR     0.675            0          0          0          1
1210            CIRCULAR     0.675            0          0          0          1
1212            CIRCULAR     0.675            0          0          0          1
1213            CIRCULAR     0.675            0          0          0          1
1214            CIRCULAR     0.675            0          0          0          1
1215            CIRCULAR     0.675            0          0          0          1
1216            CIRCULAR     0.675            0          0          0          1
1220            CIRCULAR     0.3              0          0          0          1
1221            CIRCULAR     0.375            0          0          0          1
1222            CIRCULAR     0.375            0          0          0          1
1223            CIRCULAR     0.375            0          0          0          1
1224            CIRCULAR     0.375            0          0          0          1
1225            CIRCULAR     0.375            0          0          0          1
1226            CIRCULAR     0.3              0          0          0          1
1245            CIRCULAR     0.35             0          0          0          1
1246            CIRCULAR     0.35             0          0          0          1
1247            CIRCULAR     0.35             0          0          0          1
1248            CIRCULAR     0.35             0          0          0          1
1249            CIRCULAR     0.35             0          0          0          1
1250            CIRCULAR     0.35             0          0          0          1
1251            CIRCULAR     0.35             0          0          0          1
1252            CIRCULAR     0.35             0          0          0          1
1255            CIRCULAR     0.35             0          0          0          1
1256            CIRCULAR     0.35             0          0          0          1
1290            CIRCULAR     0.4              0          0          0          1
1291            CIRCULAR     0.4              0          0          0          1
1292            CIRCULAR     0.4              0          0          0          1
1293            CIRCULAR     0.4              0          0          0          1
1294            CIRCULAR     0.4              0          0          0          1
1295            CIRCULAR     0.4              0          0          0          1
1296            CIRCULAR     0.825            0          0          0          1
1297            CIRCULAR     0.825            0          0          0          1
1298            CIRCULAR     0.825            0          0          0          1
1299            CIRCULAR     0.825            0          0          0          1
1300            CIRCULAR     0.825            0          0          0          1
1301            CIRCULAR     0.825            0          0          0          1
1302            CIRCULAR     0.825            0          0          0          1
1303            CIRCULAR     0.825            0          0          0          1
1308            CIRCULAR     0.825            0          0          0          1
1311            CIRCULAR     0.825            0          0          0          1
1312            CIRCULAR     0.825            0          0          0          1
1313            CIRCULAR     0.825            0          0          0          1
1314            CIRCULAR     0.825            0          0          0          1
1315            CIRCULAR     0.825            0          0          0          1
1316            CIRCULAR     0.825            0          0          0          1
132             CIRCULAR     0.375            0          0          0          1
133             CIRCULAR     0.375            0          0          0          1
134             CIRCULAR     0.375            0          0          0          1
1348            CIRCULAR     0.4              0          0          0          1
1349            CIRCULAR     0.4              0          0          0          1
1350            CIRCULAR     0.4              0          0          0          1
1351            CIRCULAR     0.45             0          0          0          1
```

154	CIRCULAR	0.45	0	0	0	1
155	CIRCULAR	0.3	0	0	0	1
156	CIRCULAR	0.45	0	0	0	1
158	CIRCULAR	0.25	0	0	0	1
159	CIRCULAR	0.3	0	0	0	1
160	CIRCULAR	0.3	0	0	0	1
161	CIRCULAR	0.3	0	0	0	1
162	CIRCULAR	0.25	0	0	0	1
163	CIRCULAR	0.25	0	0	0	1
164	CIRCULAR	0.25	0	0	0	1
165	CIRCULAR	0.3	0	0	0	1
166	CIRCULAR	0.3	0	0	0	1
167	CIRCULAR	0.3	0	0	0	1
168	CIRCULAR	0.3	0	0	0	1
169	CIRCULAR	0.3	0	0	0	1
170	CIRCULAR	0.3	0	0	0	1
1703	CIRCULAR	0.3	0	0	0	1
171	CIRCULAR	0.3	0	0	0	1
1716	CIRCULAR	0.25	0	0	0	1
1717	CIRCULAR	0.25	0	0	0	1
1718	CIRCULAR	0.25	0	0	0	1
1719	CIRCULAR	0.25	0	0	0	1
172	CIRCULAR	0.3	0	0	0	1
1742	CIRCULAR	0.25	0	0	0	1
1743	CIRCULAR	0.25	0	0	0	1
1745	CIRCULAR	0.25	0	0	0	1
1746	CIRCULAR	0.25	0	0	0	1
1747	CIRCULAR	0.6	0	0	0	1
1748	CIRCULAR	0.6	0	0	0	1
1749	CIRCULAR	0.6	0	0	0	1
1750	CIRCULAR	0.6	0	0	0	1
1751	CIRCULAR	0.6	0	0	0	1
1752	CIRCULAR	0.6	0	0	0	1
1755	CIRCULAR	0.3	0	0	0	1
1756	CIRCULAR	0.3	0	0	0	1
1757	CIRCULAR	0.3	0	0	0	1
1759	CIRCULAR	0.3	0	0	0	1
1760	CIRCULAR	0.3	0	0	0	1
1761	CIRCULAR	0.3	0	0	0	1
1766	CIRCULAR	0.25	0	0	0	1
1772	CIRCULAR	0.25	0	0	0	1
1773	CIRCULAR	0.3	0	0	0	1
1774	CIRCULAR	0.2	0	0	0	1
1775	CIRCULAR	0.2	0	0	0	1
1776	CIRCULAR	0.6	0	0	0	1
1777	CIRCULAR	0.6	0	0	0	1
1778	CIRCULAR	0.6	0	0	0	1
1779	CIRCULAR	0.6	0	0	0	1
1802	CIRCULAR	0.6	0	0	0	1
1803	CIRCULAR	0.6	0	0	0	1
1804	CIRCULAR	0.6	0	0	0	1
1805	CIRCULAR	0.6	0	0	0	1
1806	CIRCULAR	0.9	0	0	0	1
1807	CIRCULAR	0.9	0	0	0	1
1808	CIRCULAR	0.9	0	0	0	1
1809	CIRCULAR	0.9	0	0	0	1
1821	CIRCULAR	0.9	0	0	0	1
1877	CIRCULAR	0.9	0	0	0	1
1878	CIRCULAR	0.9	0	0	0	1
1879	CIRCULAR	0.9	0	0	0	1
1880	CIRCULAR	0.9	0	0	0	1
1881	CIRCULAR	0.9	0	0	0	1
1882	CIRCULAR	0.9	0	0	0	1
1883	CIRCULAR	0.9	0	0	0	1
1884	CIRCULAR	0.9	0	0	0	1
1885	CIRCULAR	0.9	0	0	0	1
1886	CIRCULAR	0.9	0	0	0	1
1887	CIRCULAR	0.9	0	0	0	1
1888	CIRCULAR	0.525	0	0	0	1
1891	CIRCULAR	0.525	0	0	0	1
1893	CIRCULAR	0.525	0	0	0	1
1905	CIRCULAR	0.525	0	0	0	1
1912	CIRCULAR	0.3	0	0	0	1
1925	CIRCULAR	0.3	0	0	0	1
1926	CIRCULAR	0.375	0	0	0	1
1927	CIRCULAR	0.375	0	0	0	1
1929	CIRCULAR	0.375	0	0	0	1
1931	CIRCULAR	0.375	0	0	0	1
1933	CIRCULAR	0.45	0	0	0	1
1934	CIRCULAR	0.375	0	0	0	1
1935	CIRCULAR	0.45	0	0	0	1
1946	CIRCULAR	0.375	0	0	0	1
1947	CIRCULAR	0.375	0	0	0	1
1948	CIRCULAR	0.45	0	0	0	1
1949	CIRCULAR	0.45	0	0	0	1
1950	CIRCULAR	0.45	0	0	0	1
1951	CIRCULAR	0.45	0	0	0	1
1956	CIRCULAR	0.9	0	0	0	1
1957	CIRCULAR	0.875	0	0	0	1
1958	CIRCULAR	0.9	0	0	0	1
1959	CIRCULAR	0.9	0	0	0	1
1960	CIRCULAR	0.9	0	0	0	1
1977	CIRCULAR	0.45	0	0	0	1
1978	CIRCULAR	0.45	0	0	0	1
1979	CIRCULAR	0.45	0	0	0	1
1980	CIRCULAR	0.45	0	0	0	1
2015	CIRCULAR	0.525	0	0	0	1
2016	CIRCULAR	0.525	0	0	0	1
2017	CIRCULAR	0.525	0	0	0	1
2018	CIRCULAR	0.525	0	0	0	1
2019	CIRCULAR	0.525	0	0	0	1
2020	CIRCULAR	0.525	0	0	0	1
2021	CIRCULAR	0.45	0	0	0	1
2029	CIRCULAR	0.45	0	0	0	1
2048	CIRCULAR	0.25	0	0	0	1
2049	CIRCULAR	0.375	0	0	0	1
2056	CIRCULAR	0.9	0	0	0	1
208	CIRCULAR	0.225	0	0	0	1
2082	CIRCULAR	0.45	0	0	0	1
2083	CIRCULAR	0.45	0	0	0	1
2084	CIRCULAR	0.45	0	0	0	1
2085	CIRCULAR	0.45	0	0	0	1
2086	CIRCULAR	0.45	0	0	0	1
2087	CIRCULAR	0.45	0	0	0	1
209	CIRCULAR	0.225	0	0	0	1
2099	CIRCULAR	0.6	0	0	0	1
210	CIRCULAR	0.375	0	0	0	1
2135	CIRCULAR	0.6	0	0	0	1
2135_1	CIRCULAR	0.6	0	0	0	1
2135_2	CIRCULAR	0.6	0	0	0	1
2135_3	CIRCULAR	0.6	0	0	0	1
2135_4	CIRCULAR	0.6	0	0	0	1
2136	CIRCULAR	0.525	0	0	0	1
2137	CIRCULAR	0.525	0	0	0	1
2138	CIRCULAR	0.525	0	0	0	1
2140	CIRCULAR	0.45	0	0	0	1
2144	CIRCULAR	0.675	0	0	0	1
2145	CIRCULAR	0.675	0	0	0	1
2146	CIRCULAR	0.675	0	0	0	1
2147	CIRCULAR	1.5	0	0	0	1
2149	CIRCULAR	1.5	0	0	0	1
2152	CIRCULAR	0.3	0	0	0	1
2153	CIRCULAR	0.375	0	0	0	1
216	CIRCULAR	0.4	0	0	0	1
2175	CIRCULAR	0.6	0	0	0	1
2176	CIRCULAR	0.6	0	0	0	1
2177	CIRCULAR	0.6	0	0	0	1
2178	CIRCULAR	0.525	0	0	0	1
2179	CIRCULAR	0.375	0	0	0	1
2180	CIRCULAR	0.375	0	0	0	1
2181	CIRCULAR	0.6	0	0	0	1
219	CIRCULAR	0.4	0	0	0	1
2219	CIRCULAR	0.6	0	0	0	1
2220	CIRCULAR	0.6	0	0	0	1
2221	CIRCULAR	0.6	0	0	0	1
2222	CIRCULAR	0.6	0	0	0	1
2223	CIRCULAR	0.6	0	0	0	1
2224	CIRCULAR	0.6	0	0	0	1
2225	CIRCULAR	0.6	0	0	0	1
2226	CIRCULAR	0.6	0	0	0	1
2264	CIRCULAR	0.6	0	0	0	1
2269	CIRCULAR	0.25	0	0	0	1
2270	CIRCULAR	0.45	0	0	0	1
2271	CIRCULAR	0.45	0	0	0	1
2272	CIRCULAR	0.45	0	0	0	1
2273	CIRCULAR	0.25	0	0	0	1
2274	CIRCULAR	0.45	0	0	0	1
2277	CIRCULAR	0.45	0	0	0	1
2278	CIRCULAR	0.45	0	0	0	1
2279	CIRCULAR	0.45	0	0	0	1
2280	CIRCULAR	0.45	0	0	0	1
2281	CIRCULAR	0.4	0	0	0	1
2282	CIRCULAR	0.4	0	0	0	1
2283	CIRCULAR	0.4	0	0	0	1
2284	CIRCULAR	0.4	0	0	0	1
2285	CIRCULAR	0.4	0	0	0	1
2286	CIRCULAR	0.4	0	0	0	1
2287	CIRCULAR	0.4	0	0	0	1
2288	CIRCULAR	0.4	0	0	0	1
2289	CIRCULAR	0.4	0	0	0	1
229	CIRCULAR	0.45	0	0	0	1
2291	CIRCULAR	0.9	0	0	0	1
2292	CIRCULAR	0.75	0	0	0	1
2339	CIRCULAR	0.525	0	0	0	1
2340	CIRCULAR	0.525	0	0	0	1
235	CIRCULAR	0.375	0	0	0	1
2390_1	FORCE_MAIN	0.45	120	0	0	1
2390_2	FORCE_MAIN	0.45	120	0	0	1
2390_3	FORCE_MAIN	0.45	120	0	0	1
2390_5	FORCE_MAIN	0.45	120	0	0	1
273	CIRCULAR	0.45	0	0	0	1
274	CIRCULAR	0.525	0	0	0	1
275	CIRCULAR	0.525	0	0	0	1
276	CIRCULAR	0.525	0	0	0	1
277	CIRCULAR	0.6	0	0	0	1
278	CIRCULAR	0.6	0	0	0	1
283	CIRCULAR	0.6	0	0	0	1
289	CIRCULAR	0.375	0	0	0	1
290	CIRCULAR	0.375	0	0	0	1
291	CIRCULAR	0.375	0	0	0	1
292	CIRCULAR	0.375	0	0	0	1
3300	CIRCULAR	0.675	0	0	0	1
3301	CIRCULAR	0.675	0	0	0	1
3302	CIRCULAR	0.675	0	0	0	1
3303	CIRCULAR	0.675	0	0	0	1
3304	CIRCULAR	0.675	0	0	0	1
3305	CIRCULAR	0.675	0	0	0	1
3306	CIRCULAR	0.675	0	0	0	1
3307	CIRCULAR	0.675	0	0	0	1
3309	CIRCULAR	0.675	0	0	0	1
3310	CIRCULAR	0.675	0	0	0	1
3311	CIRCULAR	0.675	0	0	0	1
3312	CIRCULAR	0.675	0	0	0	1
3313	CIRCULAR	0.45	0	0	0	1
3314	CIRCULAR	0.45	0	0	0	1
3315	CIRCULAR	0.45	0	0	0	1
3317	CIRCULAR	0.45	0	0	0	1
3318	CIRCULAR	0.45	0	0	0	1
3319	CIRCULAR	0.45	0	0	0	1
3320	CIRCULAR	0.45	0	0	0	1
3321	CIRCULAR	0.45	0	0	0	1
3339_10	CIRCULAR	0.25	0	0	0	1
3339_11	CIRCULAR	0.45	0	0	0	1
3339_12	CIRCULAR	0.25	0	0	0	1
3339_2	CIRCULAR	0.25	0	0	0	1
3339_3	CIRCULAR	0.25	0	0	0	1
3339_5	CIRCULAR	0.25	0	0	0	1
3339_6	CIRCULAR	0.45	0	0	0	1
3339_8	CIRCULAR	0.25	0	0	0	1
3339_9	CIRCULAR	0.45	0	0	0	1
3340	CIRCULAR	0.6	0	0	0	1
3341	CIRCULAR	0.6	0	0	0	1

3342	CIRCULAR	0.6	0	0	0	1
3343	CIRCULAR	0.6	0	0	0	1
3344	CIRCULAR	0.6	0	0	0	1
3345	CIRCULAR	0.6	0	0	0	1
3346	CIRCULAR	0.6	0	0	0	1
3347	CIRCULAR	0.6	0	0	0	1
3348	CIRCULAR	0.6	0	0	0	1
3364	CIRCULAR	0.525	0	0	0	1
3365	CIRCULAR	0.525	0	0	0	1
3366	CIRCULAR	0.525	0	0	0	1
3367	CIRCULAR	0.525	0	0	0	1
3368	CIRCULAR	0.525	0	0	0	1
3369	CIRCULAR	0.525	0	0	0	1
3370	CIRCULAR	0.525	0	0	0	1
3371	CIRCULAR	0.525	0	0	0	1
3372	CIRCULAR	0.525	0	0	0	1
3373	CIRCULAR	0.525	0	0	0	1
3374	CIRCULAR	0.525	0	0	0	1
3375	CIRCULAR	0.525	0	0	0	1
3376	CIRCULAR	0.525	0	0	0	1
3377	CIRCULAR	0.525	0	0	0	1
3378	CIRCULAR	0.525	0	0	0	1
3379	CIRCULAR	0.525	0	0	0	1
3380	CIRCULAR	0.525	0	0	0	1
3381	CIRCULAR	0.525	0	0	0	1
3382	CIRCULAR	0.525	0	0	0	1
3383	CIRCULAR	0.525	0	0	0	1
3384	CIRCULAR	0.525	0	0	0	1
3385	CIRCULAR	0.525	0	0	0	1
3386	CIRCULAR	0.525	0	0	0	1
3387	CIRCULAR	0.45	0	0	0	1
3388	CIRCULAR	0.45	0	0	0	1
3389	CIRCULAR	0.45	0	0	0	1
3390	CIRCULAR	0.45	0	0	0	1
3391	CIRCULAR	0.45	0	0	0	1
3392	CIRCULAR	0.45	0	0	0	1
3393	CIRCULAR	0.375	0	0	0	1
3394	CIRCULAR	0.3	0	0	0	1
3395	CIRCULAR	0.3	0	0	0	1
3396	CIRCULAR	0.3	0	0	0	1
3398	CIRCULAR	0.375	0	0	0	1
3399	CIRCULAR	0.375	0	0	0	1
3400	CIRCULAR	0.375	0	0	0	1
3401	CIRCULAR	0.375	0	0	0	1
3402	CIRCULAR	0.3	0	0	0	1
3403	CIRCULAR	0.3	0	0	0	1
3500	CIRCULAR	0.6	0	0	0	1
3502	CIRCULAR	0.525	0	0	0	1
3503	CIRCULAR	0.525	0	0	0	1
3504	CIRCULAR	0.525	0	0	0	1
3505	CIRCULAR	0.525	0	0	0	1
3690	CIRCULAR	0.6	0	0	0	1
39	CIRCULAR	0.6	0	0	0	1
391	CIRCULAR	0.6	0	0	0	1
392	CIRCULAR	0.6	0	0	0	1
393	CIRCULAR	0.6	0	0	0	1
394	CIRCULAR	0.6	0	0	0	1
395	CIRCULAR	0.6	0	0	0	1
396	CIRCULAR	0.6	0	0	0	1
400	CIRCULAR	0.9	0	0	0	1
401	CIRCULAR	0.9	0	0	0	1
403	CIRCULAR	0.45	0	0	0	1
4035	CIRCULAR	0.525	0	0	0	1
4036	CIRCULAR	0.525	0	0	0	1
4037	CIRCULAR	0.525	0	0	0	1
4038	CIRCULAR	0.375	0	0	0	1
408	CIRCULAR	0.9	0	0	0	1
412	CIRCULAR	0.5	0	0	0	1
413	CIRCULAR	0.5	0	0	0	1
414	CIRCULAR	0.5	0	0	0	1
415	CIRCULAR	0.5	0	0	0	1
417	CIRCULAR	0.5	0	0	0	1
418	CIRCULAR	0.525	0	0	0	1
419	CIRCULAR	0.525	0	0	0	1
420	CIRCULAR	0.525	0	0	0	1
421	CIRCULAR	0.525	0	0	0	1
422	CIRCULAR	0.25	0	0	0	1
423	CIRCULAR	0.375	0	0	0	1
424	CIRCULAR	0.375	0	0	0	1
425	CIRCULAR	0.375	0	0	0	1
426	CIRCULAR	0.45	0	0	0	1
427	CIRCULAR	0.9	0	0	0	1
428	CIRCULAR	0.9	0	0	0	1
429	CIRCULAR	0.45	0	0	0	1
436	CIRCULAR	0.3	0	0	0	1
437	CIRCULAR	0.3	0	0	0	1
438	CIRCULAR	0.9	0	0	0	1
439	CIRCULAR	0.9	0	0	0	1
442	CIRCULAR	0.225	0	0	0	1
443	CIRCULAR	0.525	0	0	0	1
444	CIRCULAR	0.525	0	0	0	1
445	CIRCULAR	0.225	0	0	0	1
446	CIRCULAR	0.5	0	0	0	1
447	CIRCULAR	0.5	0	0	0	1
448	CIRCULAR	0.25	0	0	0	1
449	CIRCULAR	0.225	0	0	0	1
45	CIRCULAR	0.75	0	0	0	1
450	CIRCULAR	0.225	0	0	0	1
451	CIRCULAR	0.25	0	0	0	1
452	CIRCULAR	0.75	0	0	0	1
453	CIRCULAR	0.4	0	0	0	1
454	CIRCULAR	0.9	0	0	0	1
455	CIRCULAR	0.25	0	0	0	1
456	CIRCULAR	0.25	0	0	0	1
457	CIRCULAR	0.35	0	0	0	1
458	CIRCULAR	0.45	0	0	0	1
459	CIRCULAR	0.525	0	0	0	1
460	CIRCULAR	0.3	0	0	0	1
461	CIRCULAR	0.45	0	0	0	1
465	CIRCULAR	0.75	0	0	0	1
468	CIRCULAR	0.75	0	0	0	1
469	CIRCULAR	0.75	0	0	0	1
474	CIRCULAR	0.75	0	0	0	1
475	CIRCULAR	0.75	0	0	0	1
476	CIRCULAR	0.6	0	0	0	1
477	CIRCULAR	0.6	0	0	0	1
478	CIRCULAR	0.75	0	0	0	1
499	CIRCULAR	0.45	0	0	0	1
500	CIRCULAR	0.45	0	0	0	1
502	CIRCULAR	0.45	0	0	0	1
505	CIRCULAR	0.375	0	0	0	1
5050	CIRCULAR	0.525	0	0	0	1
506	CIRCULAR	0.375	0	0	0	1
507	CIRCULAR	0.45	0	0	0	1
51	CIRCULAR	0.75	0	0	0	1
510	CIRCULAR	0.3	0	0	0	1
511	CIRCULAR	0.375	0	0	0	1
512	CIRCULAR	0.3	0	0	0	1
513	CIRCULAR	0.3	0	0	0	1
515	CIRCULAR	0.25	0	0	0	1
520	CIRCULAR	0.3	0	0	0	1
53_1	CIRCULAR	0.75	0	0	0	1
53_2	CIRCULAR	0.75	0	0	0	1
551	CIRCULAR	0.6	0	0	0	1
552	CIRCULAR	0.6	0	0	0	1
558	CIRCULAR	0.6	0	0	0	1
560	CIRCULAR	0.6	0	0	0	1
60	CIRCULAR	0.75	0	0	0	1
61	CIRCULAR	0.75	0	0	0	1
62	CIRCULAR	0.75	0	0	0	1
63	CIRCULAR	0.75	0	0	0	1
63_1	CIRCULAR	0.75	0	0	0	1
64	CIRCULAR	0.375	0	0	0	1
646	CIRCULAR	0.6	0	0	0	1
647	CIRCULAR	0.6	0	0	0	1
649	CIRCULAR	0.6	0	0	0	1
650	CIRCULAR	0.6	0	0	0	1
651	CIRCULAR	0.6	0	0	0	1
663	CIRCULAR	0.3	0	0	0	1
664	CIRCULAR	0.375	0	0	0	1
665	CIRCULAR	0.375	0	0	0	1
666	CIRCULAR	0.45	0	0	0	1
667	CIRCULAR	0.45	0	0	0	1
668	CIRCULAR	0.45	0	0	0	1
669	CIRCULAR	0.45	0	0	0	1
670	CIRCULAR	0.6	0	0	0	1
672	CIRCULAR	0.6	0	0	0	1
673	CIRCULAR	0.6	0	0	0	1
675	CIRCULAR	0.6	0	0	0	1
680	CIRCULAR	0.4	0	0	0	1
681	CIRCULAR	0.4	0	0	0	1
682	CIRCULAR	0.4	0	0	0	1
683	CIRCULAR	0.6	0	0	0	1
684	CIRCULAR	0.6	0	0	0	1
688	CIRCULAR	0.6	0	0	0	1
689	CIRCULAR	0.6	0	0	0	1
779	CIRCULAR	0.6	0	0	0	1
780	CIRCULAR	0.6	0	0	0	1
781	CIRCULAR	0.6	0	0	0	1
782	CIRCULAR	0.6	0	0	0	1
854	CIRCULAR	0.35	0	0	0	1
855	CIRCULAR	0.35	0	0	0	1
860	CIRCULAR	0.35	0	0	0	1
861	CIRCULAR	0.35	0	0	0	1
862	CIRCULAR	0.35	0	0	0	1
866	CIRCULAR	0.35	0	0	0	1
867	CIRCULAR	0.35	0	0	0	1
868	CIRCULAR	0.4	0	0	0	1
880	CIRCULAR	0.4	0	0	0	1
881	CIRCULAR	0.45	0	0	0	1
882	CIRCULAR	0.45	0	0	0	1
883	CIRCULAR	0.45	0	0	0	1
884	CIRCULAR	0.45	0	0	0	1
885	CIRCULAR	0.45	0	0	0	1
886	CIRCULAR	0.6	0	0	0	1
887	CIRCULAR	0.6	0	0	0	1
888	CIRCULAR	0.6	0	0	0	1
889	CIRCULAR	0.6	0	0	0	1
890	CIRCULAR	0.6	0	0	0	1
891	CIRCULAR	0.6	0	0	0	1
892	CIRCULAR	0.6	0	0	0	1
9011	FORCE_MAIN	0.45	120	0	0	1
9012	FORCE_MAIN	0.45	120	0	0	1
9013	CIRCULAR	1	0	0	0	1
9014	CIRCULAR	0.525	0	0	0	1
9015	CIRCULAR	0.525	0	0	0	1
9016	CIRCULAR	0.525	0	0	0	1
9017	CIRCULAR	0.525	0	0	0	1
9018	CIRCULAR	0.525	0	0	0	1
9019	CIRCULAR	0.525	0	0	0	1
9020	CIRCULAR	0.525	0	0	0	1
9021	CIRCULAR	0.525	0	0	0	1
9022	CIRCULAR	0.525	0	0	0	1
9023	CIRCULAR	0.6	0	0	0	1
9024	CIRCULAR	0.6	0	0	0	1
9025	CIRCULAR	0.6	0	0	0	1
9026	CIRCULAR	0.6	0	0	0	1
9027	CIRCULAR	1.05	0	0	0	1
9028	CIRCULAR	0.6	0	0	0	1
9029	CIRCULAR	0.6	0	0	0	1
932	CIRCULAR	0.45	0	0	0	1
946	CIRCULAR	0.3	0	0	0	1
947	CIRCULAR	0.3	0	0	0	1
948	CIRCULAR	0.3	0	0	0	1
949	CIRCULAR	0.3	0	0	0	1
952	CIRCULAR	0.25	0	0	0	1
953	CIRCULAR	0.25	0	0	0	1
955	CIRCULAR	0.25	0	0	0	1
957	CIRCULAR	1.05	0	0	0	1
958	CIRCULAR	1.05	0	0	0	1
959	CIRCULAR	1.05	0	0	0	1
960	CIRCULAR	1.05	0	0	0	1

961	CIRCULAR	1.05	0	0	0	1
962	CIRCULAR	1.05	0	0	0	1
963	CIRCULAR	1.05	0	0	0	1
964_1	CIRCULAR	1.05	0	0	0	1
964_2	CIRCULAR	1.05	0	0	0	1
965	CIRCULAR	1.05	0	0	0	1
966	CIRCULAR	1.05	0	0	0	1
967	CIRCULAR	1.05	0	0	0	1
968	CIRCULAR	1.05	0	0	0	1
969	CIRCULAR	1.05	0	0	0	1
970	CIRCULAR	1.05	0	0	0	1
971	CIRCULAR	1.05	0	0	0	1
988	CIRCULAR	0.45	0	0	0	1
989	CIRCULAR	0.45	0	0	0	1
990	CIRCULAR	0.45	0	0	0	1
990_1	CIRCULAR	0.525	0	0	0	1
9902	CIRCULAR	0.75	0	0	0	1
9904	FORCE_MAIN	0.6	120	0	0	1
9905	CIRCULAR	0.6	0	0	0	1
9906_1	FORCE_MAIN	0.45	120	0	0	1
9906_2	FORCE_MAIN	0.45	120	0	0	1
9907	CIRCULAR	0.45	0	0	0	1
9908	CIRCULAR	0.45	0	0	0	1
9909	FORCE_MAIN	0.6	120	0	0	1
9910	FORCE_MAIN	0.6	120	0	0	1
9911	CIRCULAR	0.35	0	0	0	1
9912	CIRCULAR	0.91	0	0	0	1
9914	FORCE_MAIN	0.3	120	0	0	1
9915	FORCE_MAIN	0.35	120	0	0	1
9916	FORCE_MAIN	0.35	120	0	0	1
992_1	CIRCULAR	0.525	0	0	0	1
992_2	CIRCULAR	0.525	0	0	0	1
998	CIRCULAR	0.5	0	0	0	1
999	CIRCULAR	0.5	0	0	0	1
2282_c	CIRCULAR	1.05	0	0	0	
9913	CIRCULAR	0.91	0	0	0	
3339_1	RECT_OPEN	0.852	1.2	0	0	
3339_4	RECT_OPEN	0.784	1.2	0	0	

[LOSSES]

;;Link	Kentry	Kexit	Kavg	Flap Gate	Seepage
;;--------------	----------	----------	----------	----------	----------
1001	0	0.02	0	NO	0
1009	0	0.045	0	NO	0
1010	0	1.32	0	NO	0
1011	0	0.045	0	NO	0
1023	0	0.045	0	NO	0
1025	0	0.045	0	NO	0
1026	0	0.045	0	NO	0
1027	0	0.21	0	NO	0
1028	0	0.325	0	NO	0
1029	0	1.32	0	NO	0
103	0	0.045	0	NO	0
1030	0	1.065	0	NO	0
1032	0	0.045	0	NO	0
1033	0	0.118	0	NO	0
104	0	0.045	0	NO	0
1045	0	0.045	0	NO	0
1046	0	0.045	0	NO	0
1048	0	0.045	0	NO	0
1050	0	0.21	0	NO	0
1052	0	1.32	0	NO	0
1054_1	0	0.02	0	NO	0
1054_2	0	1.32	0	NO	0
109	0	0.02	0	NO	0
1090	0	0.045	0	NO	0
1091	0	0.045	0	NO	0
1092	0	0.045	0	NO	0
1093	0	0.045	0	NO	0
1096	0	0.045	0	NO	0
1103	0	0.045	0	NO	0
1116	0	0.045	0	NO	0
1117	0	0.045	0	NO	0
1118	0	0.045	0	NO	0
1119	0	0.045	0	NO	0
1120	0	0.045	0	NO	0
1179	0	0.21	0	NO	0
1180	0	0.045	0	NO	0
1181	0	0.045	0	NO	0
1182	0	0.02	0	NO	0
1183	0	0.325	0	NO	0
1184	0	0.325	0	NO	0
1185	0	0.045	0	NO	0
1186	0	0.045	0	NO	0
1189	0	0.325	0	NO	0
1190	0	0.045	0	NO	0
1193	0	0.118	0	NO	0
1194	0	1.065	0	NO	0
1195	0	1.32	0	NO	0
1196	0	0.045	0	NO	0
1198	0	0.045	0	NO	0
1199	0	0.21	0	NO	0
1202	0	0.045	0	NO	0
1203	0	0.325	0	NO	0
1206	0	0.045	0	NO	0
1207	0	0.045	0	NO	0
1208	0	0.045	0	NO	0
1209	0	0.045	0	NO	0
1210	0	0.118	0	NO	0
1212	0	0.045	0	NO	0
1213	0	0.045	0	NO	0
1214	0	0.045	0	NO	0
1215	0	0.045	0	NO	0
1216	0	0.045	0	NO	0
1220	0	0.045	0	NO	0
1221	0	0.045	0	NO	0
1222	0	0.045	0	NO	0
1223	0	0.045	0	NO	0
1224	0	0.045	0	NO	0
1225	0	1.32	0	NO	0
1226	0	0.045	0	NO	0
1245	0	0.045	0	NO	0
1246	0	0.045	0	NO	0
1247	0	0.118	0	NO	0
1248	0	0.045	0	NO	0
1249	0	0.045	0	NO	0
1250	0	0.045	0	NO	0
1251	0	0.325	0	NO	0
1252	0	1.32	0	NO	0
1255	0	0.84	0	NO	0
1256	0	0.21	0	NO	0
1290	0	0.045	0	NO	0
1291	0	0.045	0	NO	0
1292	0	0.045	0	NO	0
1293	0	0.045	0	NO	0
1294	0	0.045	0	NO	0
1295	0	1.32	0	NO	0
1296	0	0.045	0	NO	0
1297	0	0.045	0	NO	0
1298	0	0.045	0	NO	0
1299	0	0.118	0	NO	0
1300	0	0.045	0	NO	0
1301	0	0.02	0	NO	0
1302	0	0.045	0	NO	0
1303	0	0.045	0	NO	0
1308	0	0.045	0	NO	0
1311	0	0.045	0	NO	0
1312	0	0.325	0	NO	0
1313	0	0.045	0	NO	0
1314	0	0.325	0	NO	0
1315	0	0.045	0	NO	0
1316	0	0.46	0	NO	0
132	0	0.045	0	NO	0
133	0	0.045	0	NO	0
134	0	0.045	0	NO	0
1348	0	0.045	0	NO	0
1349	0	0.045	0	NO	0
1350	0	0.045	0	NO	0
1351	0	0.045	0	NO	0
154	0	0.635	0	NO	0
155	0	1.32	0	NO	0
156	0	1.32	0	NO	0
158	0	0.045	0	NO	0
159	0	0.045	0	NO	0
160	0	0.045	0	NO	0
161	0	0.21	0	NO	0
162	0	0.045	0	NO	0
163	0	0.045	0	NO	0
164	0	0.045	0	NO	0
165	0	0.045	0	NO	0
166	0	0.045	0	NO	0
167	0	0.045	0	NO	0
168	0	0.635	0	NO	0
169	0	0.045	0	NO	0
170	0	0.045	0	NO	0
1703	0	0.045	0	NO	0
171	0	0.21	0	NO	0
1716	0	0.045	0	NO	0
1717	0	0.045	0	NO	0
1718	0	0.045	0	NO	0
1719	0	0.045	0	NO	0
172	0	0.045	0	NO	0
1742	0	0.045	0	NO	0
1743	0	0.045	0	NO	0
1745	0	0.045	0	NO	0
1746	0	1.32	0	NO	0
1747	0	0.045	0	NO	0
1748	0	0.045	0	NO	0
1749	0	0.21	0	NO	0
1750	0	1.32	0	NO	0
1751	0	0.21	0	NO	0
1752	0	0.045	0	NO	0
1755	0	0.045	0	NO	0
1756	0	1.32	0	NO	0
1757	0	1.32	0	NO	0
1759	0	1.32	0	NO	0
1760	0	0.045	0	NO	0
1761	0	0.045	0	NO	0
1766	0	1.32	0	NO	0
1772	0	0.045	0	NO	0
1773	0	0.045	0	NO	0
1774	0	0.045	0	NO	0
1775	0	1.32	0	NO	0
1776	0	0.045	0	NO	0
1777	0	0.02	0	NO	0
1778	0	0.045	0	NO	0
1779	0	1.32	0	NO	0
1802	0	1.32	0	NO	0
1803	0	0.045	0	NO	0
1804	0	0.045	0	NO	0
1805	0	0.045	0	NO	0
1806	0	0.045	0	NO	0
1807	0	0.045	0	NO	0
1808	0	0.118	0	NO	0
1809	0	0.118	0	NO	0
1821	0	0.118	0	NO	0
1877	0	0.045	0	NO	0
1878	0	0.045	0	NO	0
1879	0	0.045	0	NO	0
1880	0	0.045	0	NO	0
1881	0	0.045	0	NO	0
1882	0	0.045	0	NO	0
1883	0	0.045	0	NO	0
1884	0	0.21	0	NO	0
1885	0	0.325	0	NO	0
1886	0	0.325	0	NO	0
1887	0	0.045	0	NO	0
1888	0	0.045	0	NO	0
1891	0	0.045	0	NO	0
1893	0	0.045	0	NO	0
1905	0	0.045	0	NO	0
1912	0	0.21	0	NO	0

1925	0	0.21	0	NO	0
1926	0	0.21	0	NO	0
1927	0	0.045	0	NO	0
1929	0	0.045	0	NO	0
1931	0	0.045	0	NO	0
1933	0	0.46	0	NO	0
1934	0	0.635	0	NO	0
1935	0	0.045	0	NO	0
1946	0	0.045	0	NO	0
1947	0	0.045	0	NO	0
1948	0	0.045	0	NO	0
1949	0	0.045	0	NO	0
1950	0	0.045	0	NO	0
1951	0	0.118	0	NO	0
1956	0	0.118	0	NO	0
1957	0	0.045	0	NO	0
1958	0	0.045	0	NO	0
1959	0	0.118	0	NO	0
1960	0	1	0	NO	0
1977	0	0.045	0	NO	0
1978	0	0.045	0	NO	0
1979	0	0.045	0	NO	0
1980	0	0.045	0	NO	0
2015	0	0.118	0	NO	0
2016	0	0.84	0	NO	0
2017	0	0.045	0	NO	0
2018	0	0.045	0	NO	0
2019	0	0.045	0	NO	0
2020	0	0.045	0	NO	0
2021	0	0.118	0	NO	0
2029	0	0.045	0	NO	0
2048	0	0.045	0	NO	0
2049	0	0.46	0	NO	0
2056	0	0.84	0	NO	0
208	0	0.045	0	NO	0
2082	0	0.02	0	NO	0
2083	0	0.045	0	NO	0
2084	0	0.045	0	NO	0
2085	0	0.045	0	NO	0
2086	0	0.118	0	NO	0
2087	0	0.045	0	NO	0
209	0	0.045	0	NO	0
2099	0	0.045	0	NO	0
210	0	0.02	0	NO	0
2135	0	0.045	0	NO	0
2135_1	0	0.045	0	NO	0
2135_2	0	0.045	0	NO	0
2135_3	0	0.045	0	NO	0
2135_4	0	0.045	0	NO	0
2137	0	0.46	0	NO	0
2138	0	0.46	0	NO	0
2140	0	1.32	0	NO	0
2144	0	0.118	0	NO	0
2145	0	0.045	0	NO	0
2146	0	0.21	0	NO	0
2147	0	0.045	0	NO	0
2149	0	0.84	0	NO	0
2152	0	1.32	0	NO	0
2153	0	1.32	0	NO	0
216	0	0.045	0	NO	0
2175	0	0.045	0	NO	0
2176	0	0.045	0	NO	0
2177	0	0.045	0	NO	0
2178	0	0.118	0	NO	0
2179	0	0.21	0	NO	0
2180	0	0.045	0	NO	0
2181	0	0.045	0	NO	0
219	0	0.045	0	NO	0
2219	0	0.045	0	NO	0
2220	0	0.118	0	NO	0
2221	0	0.118	0	NO	0
2222	0	0.118	0	NO	0
2223	0	0.118	0	NO	0
2224	0	0.045	0	NO	0
2225	0	0.02	0	NO	0
2226	0	0.02	0	NO	0
2264	0	0.02	0	NO	0
2269	0	0.045	0	NO	0
2270	0	0.045	0	NO	0
2271	0	1.065	0	NO	0
2272	0	0.045	0	NO	0
2273	0	1.32	0	NO	0
2274	0	1.065	0	NO	0
2277	0	0.045	0	NO	0
2278	0	0.46	0	NO	0
2279	0	1.32	0	NO	0
2280	0	1.32	0	NO	0
2281	0	1.32	0	NO	0
2282	0	0.045	0	NO	0
2283	0	0.46	0	NO	0
2284	0	0.21	0	NO	0
2285	0	0.045	0	NO	0
2286	0	0.045	0	NO	0
2287	0	1.32	0	NO	0
2288	0	0.045	0	NO	0
2289	0	1.065	0	NO	0
229	0	0.045	0	NO	0
2292	0	1	0	NO	0
2339	0	1.32	0	NO	0
2340	0	1.065	0	NO	0
235	0	0.045	0	NO	0
2390_1	0	0.84	0	NO	0
273	0	0.045	0	NO	0
274	0	1.32	0	NO	0
275	0	0.045	0	NO	0
276	0	0.045	0	NO	0
277	0	0.045	0	NO	0
278	0	0.045	0	NO	0
283	0	0.045	0	NO	0
289	0	0.045	0	NO	0
290	0	1.32	0	NO	0
291	0	0.045	0	NO	0
292	0	0.045	0	NO	0
3300	0	0.325	0	NO	0
3301	0	0.325	0	NO	0
3302	0	0.325	0	NO	0
3303	0	0.325	0	NO	0
3304	0	0.045	0	NO	0
3305	0	0.045	0	NO	0
3306	0	0.045	0	NO	0
3307	0	0.118	0	NO	0
3309	0	0.21	0	NO	0
3310	0	0.118	0	NO	0
3311	0	0.21	0	NO	0
3312	0	0.118	0	NO	0
3313	0	0.045	0	NO	0
3314	0	0.02	0	NO	0
3315	0	0.045	0	NO	0
3317	0	0.045	0	NO	0
3318	0	0.02	0	NO	0
3319	0	0.045	0	NO	0
3320	0	0.045	0	NO	0
3321	0	0.02	0	NO	0
3339_10	0	0.118	0	NO	0
3339_3	0	0.02	0	NO	0
3339_5	0	0.02	0	NO	0
3339_6	0	0.02	0	NO	0
3340	0	0.045	0	NO	0
3341	0	0.045	0	NO	0
3342	0	0.045	0	NO	0
3343	0	0.045	0	NO	0
3344	0	0.045	0	NO	0
3345	0	0.045	0	NO	0
3346	0	0.045	0	NO	0
3347	0	0.045	0	NO	0
3348	0	0.045	0	NO	0
3364	0	1.32	0	NO	0
3365	0	1.065	0	NO	0
3366	0	0.21	0	NO	0
3367	0	0.045	0	NO	0
3368	0	0.045	0	NO	0
3369	0	0.118	0	NO	0
3370	0	0.118	0	NO	0
3371	0	0.045	0	NO	0
3372	0	0.84	0	NO	0
3373	0	0.84	0	NO	0
3374	0	0.045	0	NO	0
3375	0	0.045	0	NO	0
3376	0	0.045	0	NO	0
3377	0	0.045	0	NO	0
3378	0	0.045	0	NO	0
3379	0	0.045	0	NO	0
3380	0	0.045	0	NO	0
3381	0	0.84	0	NO	0
3382	0	0.325	0	NO	0
3383	0	1.32	0	NO	0
3384	0	0.045	0	NO	0
3385	0	1.32	0	NO	0
3386	0	0.045	0	NO	0
3387	0	1.32	0	NO	0
3388	0	0.045	0	NO	0
3389	0	0.045	0	NO	0
3390	0	0.045	0	NO	0
3391	0	0.045	0	NO	0
3392	0	0.045	0	NO	0
3393	0	1.32	0	NO	0
3394	0	0.045	0	NO	0
3395	0	0.045	0	NO	0
3396	0	0.045	0	NO	0
3398	0	1.32	0	NO	0
3399	0	0.045	0	NO	0
3400	0	0.045	0	NO	0
3401	0	0.045	0	NO	0
3402	0	0.045	0	NO	0
3403	0	0.045	0	NO	0
3500	0	1.32	0	NO	0
3502	0	0.045	0	NO	0
3503	0	1.32	0	NO	0
3504	0	1.32	0	NO	0
3505	0	0.045	0	NO	0
3690	0	0.02	0	NO	0
39	0	0.045	0	NO	0
391	0	0.045	0	NO	0
392	0	0.118	0	NO	0
393	0	0.045	0	NO	0
394	0	0.118	0	NO	0
395	0	0.045	0	NO	0
396	0	0.045	0	NO	0
400	0	1.32	0	NO	0
401	0	0.045	0	NO	0
403	0	1.32	0	NO	0
4035	0	0.21	0	NO	0
4036	0	0.21	0	NO	0
4037	0	0.118	0	NO	0
4038	0	0.045	0	NO	0
408	0	0.045	0	NO	0
412	0	0.045	0	NO	0
413	0	0.118	0	NO	0
414	0	0.635	0	NO	0
415	0	0.045	0	NO	0
417	0	0.045	0	NO	0
418	0	0.46	0	NO	0
419	0	0.118	0	NO	0
420	0	0.045	0	NO	0
421	0	0.045	0	NO	0
422	0	1.32	0	NO	0
423	0	0.045	0	NO	0
424	0	0.045	0	NO	0
425	0	1.32	0	NO	0
426	0	0.045	0	NO	0
427	0	0.045	0	NO	0
428	0	0.84	0	NO	0

```
429             0          1.32       0          NO         0
436             0          0.045      0          NO         0
437             0          0.045      0          NO         0
438             0          0.045      0          NO         0
439             0          1.32       0          NO         0
442             0          1.32       0          NO         0
443             0          0.045      0          NO         0
444             0          0.045      0          NO         0
445             0          1.32       0          NO         0
446             0          0.045      0          NO         0
447             0          0.045      0          NO         0
45              0          0.045      0          NO         0
452             0          1.065      0          NO         0
453             0          0.045      0          NO         0
454             0          0.045      0          NO         0
455             0          0.045      0          NO         0
456             0          0.045      0          NO         0
457             0          1.32       0          NO         0
458             0          1.32       0          NO         0
459             0          0.045      0          NO         0
460             0          1.065      0          NO         0
461             0          0.045      0          NO         0
465             0          0.045      0          NO         0
468             0          0.045      0          NO         0
469             0          1.065      0          NO         0
474             0          0.045      0          NO         0
475             0          0.045      0          NO         0
476             0          0.045      0          NO         0
477             0          0.045      0          NO         0
478             0          0.045      0          NO         0
499             0          0.045      0          NO         0
500             0          0.635      0          NO         0
502             0          0.045      0          NO         0
505             0          0.045      0          NO         0
5050            0          1.32       0          NO         0
506             0          0.045      0          NO         0
507             0          0.045      0          NO         0
51              0          0.045      0          NO         0
510             0          0.045      0          NO         0
511             0          0.045      0          NO         0
512             0          0.84       0          NO         0
513             0          0.045      0          NO         0
515             0          1.32       0          NO         0
520             0          1.065      0          NO         0
53_1            0          0.045      0          NO         0
53_2            0          0.045      0          NO         0
551             0          0.045      0          NO         0
552             0          0.045      0          NO         0
558             0          0.46       0          NO         0
560             0          0.325      0          NO         0
60              0          0.045      0          NO         0
61              0          0.045      0          NO         0
62              0          1.32       0          NO         0
63              0          1          0          NO         0
63_1            0          0.045      0          NO         0
64              0          1          0          NO         0
646             0          0.045      0          NO         0
647             0          0.045      0          NO         0
649             0          0.045      0          NO         0
650             0          0.045      0          NO         0
651             0          0.045      0          NO         0
663             0          0.045      0          NO         0
664             0          0.045      0          NO         0
665             0          1.32       0          NO         0
666             0          0.045      0          NO         0
667             0          0.045      0          NO         0
668             0          0.045      0          NO         0
669             0          1.32       0          NO         0
670             0          0.045      0          NO         0
672             0          0.045      0          NO         0
673             0          0.045      0          NO         0
675             0          1.32       0          NO         0
680             0          0.118      0          NO         0
681             0          0.045      0          NO         0
682             0          1.32       0          NO         0
683             0          0.045      0          NO         0
684             0          0.118      0          NO         0
688             0          0.045      0          NO         0
689             0          0.045      0          NO         0
779             0          0.045      0          NO         0
780             0          0.045      0          NO         0
781             0          0.045      0          NO         0
782             0          0.045      0          NO         0
854             0          0.045      0          NO         0
855             0          0.045      0          NO         0
860             0          0.045      0          NO         0
861             0          0.045      0          NO         0
862             0          0.045      0          NO         0
866             0          0.045      0          NO         0
867             0          0.045      0          NO         0
868             0          0.045      0          NO         0
880             0          0.045      0          NO         0
881             0          0.045      0          NO         0
882             0          0.045      0          NO         0
883             0          0.045      0          NO         0
884             0          0.045      0          NO         0
885             0          1.32       0          NO         0
886             0          0.045      0          NO         0
887             0          0.045      0          NO         0
888             0          0.21       0          NO         0
889             0          0.21       0          NO         0
890             0          0.045      0          NO         0
891             0          0.045      0          NO         0
892             0          0.045      0          NO         0
9013            0          1          0          NO         0
9014            0          0.46       0          NO         0
9015            0          0.46       0          NO         0
9016            0          0.045      0          NO         0
9017            0          0.84       0          NO         0
9018            0          0.21       0          NO         0
9019            0          0.045      0          NO         0
9020            0          0.46       0          NO         0
9021            0          0.045      0          NO         0
9022            0          0.045      0          NO         0
9023            0          0.045      0          NO         0
9024            0          0.118      0          NO         0
9025            0          0.21       0          NO         0
9026            0          0.635      0          NO         0
9027            0          1          0          NO         0
9028            0          1          0          NO         0
9029            0          1          0          NO         0
932             0          1.32       0          NO         0
946             0          0.045      0          NO         0
947             0          0.045      0          NO         0
948             0          0.02       0          NO         0
949             0          1.32       0          NO         0
952             0          0.045      0          NO         0
953             0          0.46       0          NO         0
955             0          0.045      0          NO         0
957             0          0.045      0          NO         0
958             0          0.045      0          NO         0
959             0          0.325      0          NO         0
960             0          0.045      0          NO         0
961             0          0.325      0          NO         0
962             0          0.045      0          NO         0
963             0          0.118      0          NO         0
964_1           0          0.02       0          NO         0
964_2           0          0.21       0          NO         0
965             0          0.045      0          NO         0
966             0          0.045      0          NO         0
967             0          0.118      0          NO         0
968             0          0.118      0          NO         0
969             0          0.045      0          NO         0
970             0          0.045      0          NO         0
971             0          0.635      0          NO         0
988             0          0.045      0          NO         0
989             0          0.045      0          NO         0
990             0          0.045      0          NO         0
990_1           0          0.045      0          NO         0
9902            0          1          0          NO         0
9904            0          0.02       0          NO         0
9905            0          1.32       0          YES        0
9906_1          0          0.02       0          NO         0
9907            0          1.32       0          YES        0
9908            0          1          0          NO         0
9910            0          0.21       0          NO         0
9911            0          0.325      0          YES        0
9912            0          1          0          NO         0
9915            0          0          0          YES        0
9916            0          0          0          YES        0
992_1           0          0.045      0          NO         0
992_2           0          0.045      0          NO         0
998             0          0.045      0          NO         0
999             0          0.045      0          NO         0

[CONTROLS]
RULE CONDUIT9027
IF SIMULATION TIME > 0:00:00
THEN CONDUIT 9027 STATUS = CLOSED
RULE CONDUIT9028
IF SIMULATION TIME > 0:00:00
THEN CONDUIT 9028 STATUS = CLOSED
RULE CONDUIT9911
IF SIMULATION TIME > 0:00:00
THEN CONDUIT 9911 STATUS = CLOSED
RULE CONDUIT9912
IF SIMULATION TIME > 0:00:00
THEN CONDUIT 9912 STATUS = CLOSED
RULE ORIFICE2282_c
IF SIMULATION TIME > 0:00:00
THEN ORIFICE 2282_c SETTING = 0

[INFLOWS]
;;Node           Constituent      Time Series      Type     Mfactor  Sfactor  Baseline Pattern
;;-------------- ---------------- ---------------- -------- -------- -------- -------- --------
2277             FLOW             ""               FLOW     1.0      1        0.49
1093             FLOW             ""               FLOW     1.0      1        0.003704
1208             FLOW             ""               FLOW     1.0      1        0.051283
1344             FLOW             ""               FLOW     1.0      1        0.000891
1745             FLOW             ""               FLOW     1.0      1        0.000197
2036             FLOW             ""               FLOW     1.0      1        0.000293
2312             FLOW             ""               FLOW     1.0      1        0.027847
2313             FLOW             ""               FLOW     1.0      1        9.7E-05
2321             FLOW             ""               FLOW     1.0      1        0.176296
2341             FLOW             ""               FLOW     1.0      1        0.013514
2348             FLOW             ""               FLOW     1.0      1        0.000776
9001             FLOW             ""               FLOW     1.0      1        0.014606

[DWF]
;;Node           Constituent      Baseline   Patterns
;;-------------- ---------------- ---------- ----------
1176             FLOW             0.000167   "AVE_Hourly" "AVE_Weekend" "" ""
2151             FLOW             0.000963   "AVE_Hourly" "AVE_Weekend" "" ""
2152             FLOW             0.000963   "AVE_Hourly" "AVE_Weekend" "" ""
1005             FLOW             0.005251   "AVE_Hourly" "AVE_Weekend" "" ""
1007             FLOW             0.000124   "AVE_Hourly" "AVE_Weekend" "" ""
1008             FLOW             2.1E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1020             FLOW             4.9E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1022             FLOW             5.9E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1023             FLOW             8.4E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1024             FLOW             8.4E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1029             FLOW             0.000336   "AVE_Hourly" "AVE_Weekend" "" ""
1030             FLOW             0.000235   "AVE_Hourly" "AVE_Weekend" "" ""
1031             FLOW             0.000103   "AVE_Hourly" "AVE_Weekend" "" ""
1042             FLOW             0.000593   "AVE_Hourly" "AVE_Weekend" "" ""
1044             FLOW             0.000308   "AVE_Hourly" "AVE_Weekend" "" ""
1045             FLOW             0.000313   "AVE_Hourly" "AVE_Weekend" "" ""
106              FLOW             6.9E-05    "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
107              FLOW             0.000917   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
1085             FLOW             0.000946   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1090             FLOW             0.000193   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1091             FLOW             0.000193   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
```

```
1092             FLOW             0.000193   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1093             FLOW             0.005124   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1096             FLOW             0.000487   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1101             FLOW             0.000595   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1111             FLOW             0.000201   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1114             FLOW             0.000274   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1115             FLOW             8.8E-05    "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1116             FLOW             8.8E-05    "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1117             FLOW             7E-05      "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
112              FLOW             6.9E-05    "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
1185             FLOW             0.000278   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1186             FLOW             0.00016    "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1187             FLOW             0.000245   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1190             FLOW             0.000245   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1191             FLOW             0.000245   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1192             FLOW             0.000764   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1193             FLOW             0.000157   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1195             FLOW             0.000148   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1196             FLOW             0.000269   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1199             FLOW             0.000355   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1202             FLOW             0.000764   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1203             FLOW             0.000764   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1204             FLOW             0.000764   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1205             FLOW             0.000764   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1206             FLOW             0.000764   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1208             FLOW             0.074365   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1209             FLOW             0.000323   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1210             FLOW             0.000323   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1211             FLOW             0.000323   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1212             FLOW             0.001441   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1216             FLOW             0.001873   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1217             FLOW             0.001873   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1218             FLOW             0.000413   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1219             FLOW             0.000413   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1220             FLOW             0.000413   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1221             FLOW             0.000413   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1222             FLOW             0.001873   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1241             FLOW             0.002553   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1242             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1243             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1244             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1245             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1246             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1247             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1248             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1249             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1252             FLOW             0.002508   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1253             FLOW             0.000199   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1286             FLOW             0.000199   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1287             FLOW             0.000199   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1288             FLOW             0.000199   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1289             FLOW             0.000199   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1290             FLOW             0.000199   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1291             FLOW             7E-05      "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1292             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1293             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1294             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1295             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1296             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1297             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1298             FLOW             0.000282   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1299             FLOW             0.0037     "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1303             FLOW             0.000101   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1306             FLOW             0.000166   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1307             FLOW             0.000166   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1308             FLOW             0.000166   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1309             FLOW             0.004743   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1310             FLOW             0.000341   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
1344             FLOW             0.006132   "AVE_Hourly" "AVE_Weekend" "" ""
1345             FLOW             7.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1346             FLOW             0.000167   "AVE_Hourly" "AVE_Weekend" "" ""
1347             FLOW             0.000831   "AVE_Hourly" "AVE_Weekend" "" ""
1348             FLOW             0.000224   "AVE_Hourly" "AVE_Weekend" "" ""
135              FLOW             6.9E-05    "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
1352             FLOW             0.000238   "AVE_Hourly" "AVE_Weekend" "" ""
136              FLOW             6.9E-05    "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
137              FLOW             6.9E-05    "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
1511             FLOW             0.009611   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1514             FLOW             0.000135   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
157              FLOW             0.014292   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
1593             FLOW             0.001405   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1745             FLOW             0.001051   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1746             FLOW             0.000823   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
1749             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1750             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1771             FLOW             0.006288   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1772             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1773             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1774             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1794             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1795             FLOW             0.000742   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1796             FLOW             0.010323   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1797             FLOW             0.000176   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1798             FLOW             0.000176   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1799             FLOW             0.000176   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1800             FLOW             0.000176   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1801             FLOW             0.000176   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1812             FLOW             0.006195   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1866             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1867             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1868             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1869             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1870             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1871             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1872             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1873             FLOW             0.000204   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1874             FLOW             0.00016    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1875             FLOW             0.00016    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1876             FLOW             0.00016    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1877             FLOW             0.000215   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1880             FLOW             0.001638   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1881             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1898             FLOW             0.00338    "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1899             FLOW             0.00338    "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1913             FLOW             0.00338    "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1914             FLOW             0.000723   "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1915             FLOW             0.003986   "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1916             FLOW             0.003004   "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1917             FLOW             0.002811   "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1918             FLOW             0.000133   "1949_(obs)_Hourly" "1949_(obs)_Weekend" "" ""
1920             FLOW             0.000231   "AVE_Hourly" "AVE_Weekend" "" ""
1923             FLOW             0.000435   "AVE_Hourly" "AVE_Weekend" "" ""
1927             FLOW             0.00037    "AVE_Hourly" "AVE_Weekend" "" ""
1932             FLOW             0.000468   "AVE_Hourly" "AVE_Weekend" "" ""
1933             FLOW             0.0012     "AVE_Hourly" "AVE_Weekend" "" ""
1938             FLOW             0.00171    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1939             FLOW             0.00016    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1940             FLOW             0.00016    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1941             FLOW             0.000462   "AVE_Hourly" "AVE_Weekend" "" ""
1942             FLOW             0.000462   "AVE_Hourly" "AVE_Weekend" "" ""
1943             FLOW             7.6E-05    "AVE_Hourly" "AVE_Weekend" "" ""
1968             FLOW             0.00018    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1969             FLOW             0.00018    "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
1970             FLOW             0.000149   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
2029             FLOW             0.000717   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2030             FLOW             0.000189   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2031             FLOW             0.001615   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2032             FLOW             0.000372   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2033             FLOW             0.000142   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2034             FLOW             0.000142   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2035             FLOW             0.000142   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2036             FLOW             0.004672   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2063             FLOW             2.6E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2096             FLOW             0.000881   "AVE_Hourly" "AVE_Weekend" "" ""
2097             FLOW             0.000115   "AVE_Hourly" "AVE_Weekend" "" ""
2105             FLOW             0.0001     "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
211              FLOW             0.000848   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
213              FLOW             0.000534   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
2140             FLOW             0.009386   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
2140_1           FLOW             0.000697   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
2140_2           FLOW             0.000697   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
2140_3           FLOW             0.000697   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
2140_4           FLOW             0.000697   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
2146             FLOW             0.008559   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2147             FLOW             0.008559   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2148             FLOW             0.008559   "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2154             FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
2155             FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
216              FLOW             0.001142   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
2179             FLOW             0.000323   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2180             FLOW             0.000323   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
2217             FLOW             0.00013    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2218             FLOW             4.9E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2219             FLOW             0.00018    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
222              FLOW             0.001015   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
2220             FLOW             0.000711   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2221             FLOW             9.5E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2222             FLOW             0.000141   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2223             FLOW             0.000141   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2224             FLOW             0.000141   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2259             FLOW             7.1E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2282_1           FLOW             3.4E-05    "AVE_Hourly" "AVE_Weekend" "" ""
2286             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
2300             FLOW             7E-05      "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2301             FLOW             7E-05      "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2302             FLOW             7E-05      "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2303             FLOW             7E-05      "1179_(obs)_Hourly" "1179_(obs)_Weekend" "" ""
2304             FLOW             6.6E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2305             FLOW             6.6E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2306             FLOW             6.6E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2307             FLOW             0.000567   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2309             FLOW             9.7E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
231              FLOW             0.000719   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
2310             FLOW             9.7E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2311             FLOW             9.7E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2312             FLOW             0.031231   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2313             FLOW             0.000166   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2314             FLOW             5.3E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2315             FLOW             5.3E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2317             FLOW             5.3E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2318             FLOW             5.3E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2319             FLOW             5.3E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2320             FLOW             5.3E-05    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2321             FLOW             0.116369   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2341             FLOW             0.02086    "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2342             FLOW             0.000734   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2343             FLOW             0.000734   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2344             FLOW             0.000734   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2345             FLOW             0.000734   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2346             FLOW             0.000734   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2347             FLOW             0.000734   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2348             FLOW             0.006309   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
2349             FLOW             0.002654   "3304_(obs)_Hourly" "3304_(obs)_Weekend" "" ""
236              FLOW             0.000583   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
2363             FLOW             2.7E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2364             FLOW             2.7E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2366             FLOW             2.7E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2367             FLOW             0.000701   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2368             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2369             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2370             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2371             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2372             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2373             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2374             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2375             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2376             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2377             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2378             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2379             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2380             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2381             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
```

```
2382             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2383             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2384             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2385             FLOW             0.000491   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2386             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2387             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2388             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2389             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2390             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2391             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2392             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2393             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2394             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2395             FLOW             0.000511   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2397             FLOW             0.000901   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2398             FLOW             0.000901   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2399             FLOW             0.000901   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2400             FLOW             0.000901   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2401             FLOW             0.000901   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2402             FLOW             0.000901   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2453             FLOW             0.000104   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
2474             FLOW             0.000465   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
2475             FLOW             0.00088    "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
2476             FLOW             0.000402   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
2477             FLOW             0.000402   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
284              FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
285              FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
286              FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
287              FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
288              FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
289              FLOW             0.000119   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
290              FLOW             0.00303    "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
300              FLOW             0.000525   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
3000             FLOW             0.000894   "AVE_Hourly" "AVE_Weekend" "" ""
3000A            FLOW             7.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
301              FLOW             0.00056    "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
302              FLOW             0.001526   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
303              FLOW             0.001324   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
360              FLOW             0.006289   "AVE_Hourly" "AVE_Weekend" "" ""
401              FLOW             0.00303    "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
402              FLOW             0.004076   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
403              FLOW             0.000421   "394_(obs)_Hourly" "394_(obs)_Weekend" "" ""
406              FLOW             3.4E-05    "AVE_Hourly" "AVE_Weekend" "" ""
409              FLOW             0.000306   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
411              FLOW             6.6E-05    "AVE_Hourly" "AVE_Weekend" "" ""
413              FLOW             0.000402   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
418              FLOW             5.8E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
419              FLOW             0.008736   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
421              FLOW             5.8E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
424              FLOW             4.3E-05    "AVE_Hourly" "AVE_Weekend" "" ""
425              FLOW             3.4E-05    "AVE_Hourly" "AVE_Weekend" "" ""
426              FLOW             3.4E-05    "AVE_Hourly" "AVE_Weekend" "" ""
428              FLOW             0.000164   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
429              FLOW             0.000157   "AVE_Hourly" "AVE_Weekend" "" ""
431              FLOW             0.000465   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
432              FLOW             0.00025    "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
434              FLOW             0.00025    "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
435              FLOW             0.000583   "423_(obs)_Hourly" "423_(obs)_Weekend" "" ""
436              FLOW             2.6E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
439              FLOW             5.8E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
44               FLOW             0.000346   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
446              FLOW             0.000244   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
447              FLOW             0.000244   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
448              FLOW             0.000244   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
449              FLOW             0.000166   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
45               FLOW             0.003073   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
451              FLOW             0.000244   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
452              FLOW             0.00025    "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
453              FLOW             0.000134   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
454              FLOW             0.000164   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
457              FLOW             0.00017    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
458              FLOW             7.7E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
459              FLOW             7.7E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
460              FLOW             7.7E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
462              FLOW             0.001946   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
463              FLOW             0.000268   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
464              FLOW             0.000227   "3505_(obs)_Hourly" "3505_(obs)_Weekend" "" ""
465              FLOW             0.000134   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
468              FLOW             0.000904   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
469              FLOW             0.000324   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
473              FLOW             0.00017    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
477              FLOW             0.000324   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
478              FLOW             0.000324   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
479              FLOW             0.000323   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
480              FLOW             0.000324   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
481              FLOW             0.000324   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
501              FLOW             0.002544   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
502              FLOW             0.000266   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
503              FLOW             0.000266   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
506              FLOW             0.001038   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
507              FLOW             0.000242   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
508              FLOW             0.000242   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
51               FLOW             0.000974   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
511              FLOW             0.014139   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
512              FLOW             0.000242   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
513              FLOW             0.00013    "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
514              FLOW             9.8E-05    "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
521              FLOW             0.000428   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
54               FLOW             0.000238   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
55_1             FLOW             0.000195   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
553              FLOW             0.003312   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
554              FLOW             0.000178   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
555              FLOW             0.000688   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
556              FLOW             7.2E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
56               FLOW             0.000195   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
563              FLOW             0.006556   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
63               FLOW             0.000195   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
64               FLOW             0.000195   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
649              FLOW             0.000231   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
65               FLOW             0.000195   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
650              FLOW             9.1E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
652              FLOW             7.9E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
653              FLOW             0.000221   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
654              FLOW             0.00014    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
666              FLOW             0.001026   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
667              FLOW             0.001      "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
668              FLOW             0.001      "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
669              FLOW             0.001302   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
670              FLOW             0.000691   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
671              FLOW             0.00029    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
672              FLOW             0.00029    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
673              FLOW             0.000275   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
675              FLOW             0.000105   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
676              FLOW             0.000243   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
678              FLOW             7.9E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
68               FLOW             0.001544   "61_(obs)_Hourly" "61_(obs)_Weekend" "" ""
682              FLOW             5.9E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
684              FLOW             0.000167   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
685              FLOW             5.8E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
686              FLOW             0.000367   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
689              FLOW             0.000164   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
690              FLOW             0.000399   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
708              FLOW             0.008494   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
780              FLOW             8.4E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
781              FLOW             0.000111   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
782              FLOW             0.000255   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
783              FLOW             0.000385   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
796              FLOW             0.005948   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
852              FLOW             0.001124   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
853              FLOW             0.000265   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
859              FLOW             0.000265   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
860              FLOW             0.000265   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
861              FLOW             0.000265   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
864              FLOW             0.003669   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
865              FLOW             0.000265   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
866              FLOW             0.000265   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
877              FLOW             0.000902   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
878              FLOW             8.1E-05    "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
879              FLOW             0.000184   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
880              FLOW             0.000131   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
881              FLOW             0.000131   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
882              FLOW             0.000616   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
883              FLOW             0.000141   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
884              FLOW             0.000141   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
885              FLOW             0.000141   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
886              FLOW             0.000323   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
887              FLOW             0.000278   "401_(obs)_Hourly" "401_(obs)_Weekend" "" ""
9001             FLOW             0.010645   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
9002             FLOW             0.000108   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
9003             FLOW             0.000108   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
9004             FLOW             0.000108   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
9005             FLOW             0.000108   "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
9006             FLOW             0.00078    "1749_(obs)_Hourly" "1749_(obs)_Weekend" "" ""
9050             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9051             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9052             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9053             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9054             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9055             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9056             FLOW             0.001658   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9057             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9058             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9059             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9060             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
9061             FLOW             0.000104   "1959_(obs)_Hourly" "1959_(obs)_Weekend" "" ""
924              FLOW             0.006918   "932_(obs)_Hourly" "932_(obs)_Weekend" "" ""
940              FLOW             0.000342   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
942              FLOW             0.000542   "415_(obs)_Hourly" "415_(obs)_Weekend" "" ""
978              FLOW             0.000483   "AVE_Hourly" "AVE_Weekend" "" ""
984              FLOW             0.000204   "AVE_Hourly" "AVE_Weekend" "" ""
985              FLOW             7.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
986              FLOW             7.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
987              FLOW             7.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
988              FLOW             7.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
991              FLOW             4.2E-05    "AVE_Hourly" "AVE_Weekend" "" ""
996              FLOW             0.000301   "AVE_Hourly" "AVE_Weekend" "" ""
997              FLOW             2E-05      "AVE_Hourly" "AVE_Weekend" "" ""
999              FLOW             0.000135   "AVE_Hourly" "AVE_Weekend" "" ""

[HYDROGRAPHS]
;;Hydrograph     Rain Gage/Month  Response R        T        K        Dmax     Drecov   Dinit
;;-------------- ---------------- -------- -------- -------- -------- -------- -------- --------
AVE              SCS_24hr_10yr
AVE              All              Short    0.064083333 0.643416667 34.06273333 0        0        0
AVE              All              Medium   0.065183333 14.60858333 5.119483333 0        0        0
AVE              All              Long     0.089575 40.1512  4.481225 0        0        0
FM1_3304         SCS_24hr_10yr
FM1_3304         All              Short    0.0426   0.25     32.9114  0        0        0
FM1_3304         All              Medium   0.0305   7.1856   2.6455   0        0        0
FM1_3304         All              Long     0.0762   14.7239  5.44     0        0        0
FM10_1959        SCS_24hr_10yr
FM10_1959        All              Short    0.0139   0.1935   67.5629  0        0        0
FM10_1959        All              Medium   0.0304   14.98    11.0663  0        0        0
FM10_1959        All              Long     0.0807   34.2815  5.08     0        0        0
FM11_61          SCS_24hr_10yr
FM11_61          All              Short    0.0159   0.3876   35.8621  0        0        0
FM11_61          All              Medium   0.0167   24       10       0        0        0
FM11_61          All              Long     0.02     44.4     5.72     0        0        0
FM12_1749        SCS_24hr_10yr
FM12_1749        All              Short    0.0102   0.39     18.5714  0        0        0
FM12_1749        All              Medium   0.01     12       5        0        0        0
FM12_1749        All              Long     0.0188   96       4        0        0        0
FM2_1179         SCS_24hr_10yr
FM2_1179         All              Short    0.005    0.96     40.7559  0        0        0
FM2_1179         All              Medium   0.0209   24       2.5      0        0        0
FM2_1179         All              Long     0.04     30.24    4.6      0        0        0
FM3_932          SCS_24hr_10yr
FM3_932          All              Short    0.0278   0.1436   35.7808  0        0        0
FM3_932          All              Medium   0.0216   3.3183   3.5      0        0        0
FM3_932          All              Long     0.0055   28.0702  2.2875   0        0        0
FM4_1949         SCS_24hr_10yr
FM4_1949         All              Short    0.06     0.25     26       0        0        0
```

```
FM4_1949         All              Medium  0.015   6        2.5      0        0        0
FM4_1949         All              Long    0.0283  48       2        0        0        0
FM5_423          SCS_24hr_10yr
FM5_423          All              Short   0.2     0.2273   33.02    0        0        0
FM5_423          All              Medium  0.1897  9.231    2        0        0        0
FM5_423          All              Long    0.4324  17.28    3        0        0        0
FM6_394          SCS_24hr_10yr
FM6_394          All              Short   0.0287  3.8621   1.0945   0        0        0
FM6_394          All              Medium  0.0946  40       0.995    0        0        0
FM6_394          All              Long    0.0344  47.28    2.9752   0        0        0
FM7_401          SCS_24hr_10yr
FM7_401          All              Short   0.0633  0.3521   52       0        0        0
FM7_401          All              Medium  0.1     22.44    10       0        0        0
FM7_401          All              Long    0.05    32.4     4        0        0        0
FM8_3505         SCS_24hr_10yr
FM8_3505         All              Short   0.2     0.3472   40.625   0        0        0
FM8_3505         All              Medium  0.147   6.7797   7.95     0        0        0
FM8_3505         All              Long    0.0541  34.08    4.92     0        0        0
FM9_415          SCS_24hr_10yr
FM9_415          All              Short   0.1016  0.3576   24.5688  0        0        0
FM9_415          All              Medium  0.1058  5.3684   3.277    0        0        0
FM9_415          All              Long    0.2345  55.0588  9.752    0        0        0


[RDII]
;;Node           Unit Hydrograph  Sewer Area
;;-------------- ---------------- ----------
1176             AVE              2.3168
2151             AVE              13.351733
2152             AVE              13.351733
1005             AVE              48.09806
1007             AVE              1.37734
1008             AVE              0.23238
1020             AVE              0.55044
1022             AVE              0.65137
1023             AVE              0.92914
1024             AVE              0.92914
1029             AVE              3.73878
1030             AVE              2.61457
1031             AVE              1.14429
1042             AVE              6.59274
1044             AVE              3.42811
1045             AVE              3.48514
106              FM11_61          1.968826
107              FM11_61          26.20339
1085             FM12_1749        4.70455
1090             FM12_1749        1.387917
1091             FM12_1749        1.387917
1092             FM12_1749        1.387917
1093             FM12_1749        1.33644
1096             FM12_1749        3.50381
1101             FM12_1749        4.27614
1111             FM12_1749        1.44357
1114             FM12_1749        1.96946
1115             FM12_1749        0.62976
1116             FM12_1749        0.62976
1117             FM12_1749        0.5061
112              FM11_61          1.968826
1185             FM2_1179         2.16062
1186             FM2_1179         1.24529
1187             FM2_1179         1.905997
1190             FM2_1179         1.905997
1191             FM2_1179         1.905997
1192             FM2_1179         5.94322
1193             FM2_1179         1.22241
1195             FM2_1179         1.14843
1196             FM2_1179         2.09075
1199             FM2_1179         2.76383
1202             FM2_1179         5.94322
1203             FM2_1179         5.94322
1204             FM2_1179         5.94322
1205             FM2_1179         5.94322
1206             FM2_1179         5.94322
1208             FM2_1179         66.590267
1209             FM2_1179         2.51629
1210             FM2_1179         2.51629
1211             FM2_1179         2.51629
1212             FM2_1179         11.20838
1216             FM2_1179         14.571337
1217             FM2_1179         14.571337
1218             FM2_1179         3.213075
1219             FM2_1179         3.213075
1220             FM2_1179         3.213075
1221             FM2_1179         3.213075
1222             FM2_1179         14.571337
1241             FM2_1179         19.509119
1242             FM2_1179         19.509119
1243             FM2_1179         19.509119
1244             FM2_1179         19.509119
1245             FM2_1179         19.509119
1246             FM2_1179         19.509119
1247             FM2_1179         19.509119
1248             FM2_1179         19.509119
1249             FM2_1179         19.509119
1252             FM2_1179         19.509119
1253             FM2_1179         1.546657
1286             FM2_1179         1.546657
1287             FM2_1179         1.546657
1288             FM2_1179         1.546657
1289             FM2_1179         1.546657
1290             FM2_1179         1.546657
1291             FM2_1179         0.542344
1292             FM2_1179         2.195119
1293             FM2_1179         2.195119
1294             FM2_1179         2.195119
1295             FM2_1179         2.195119
1296             FM2_1179         2.195119
1297             FM2_1179         2.195119
1298             FM2_1179         2.195119
1299             FM2_1179         28.60142
1303             FM2_1179         0.78196
1306             FM2_1179         1.291043
1307             FM2_1179         1.291043
1308             FM2_1179         1.291043
1309             FM2_1179         33.626
1310             FM2_1179         2.64992
1344             AVE              48.85831
1345             AVE              0.80619
1346             AVE              1.85917
1347             AVE              9.24477
1348             AVE              2.4958
135              FM11_61          1.968826
1352             AVE              2.65209
136              FM11_61          1.968826
137              FM11_61          1.968826
1511             FM10_1959        66.94026
1514             FM10_1959        1.08652
157              FM6_394          93.01851
1593             FM10_1959        11.33133
1745             FM12_1749        5.91787
1746             FM12_1749        5.91787
1749             FM10_1959        5.978593
1750             FM10_1959        5.978593
1771             FM10_1959        50.69609
1772             FM10_1959        5.978593
1773             FM10_1959        5.978593
1774             FM10_1959        5.978593
1794             FM10_1959        5.978593
1795             FM10_1959        5.978593
1796             FM10_1959        83.22801
1797             FM10_1959        1.416046
1798             FM10_1959        1.416046
1799             FM10_1959        1.416046
1800             FM10_1959        1.416046
1801             FM10_1959        1.416046
1812             FM10_1959        49.94893
1866             FM10_1959        1.642845
1867             FM10_1959        1.642845
1868             FM10_1959        1.642845
1869             FM10_1959        1.642845
1870             FM10_1959        1.642845
1871             FM10_1959        1.642845
1872             FM10_1959        1.642845
1873             FM10_1959        1.642845
1874             FM10_1959        1.288876
1875             FM10_1959        1.288876
1876             FM10_1959        1.288876
1877             FM10_1959        1.73107
1880             FM10_1959        13.20323
1881             FM10_1959        0.837132
1898             FM4_1949         12.94856
1899             FM4_1949         12.94856
1913             FM4_1949         12.94856
1914             FM4_1949         1.28126
1915             FM4_1949         15.27182
1916             FM4_1949         11.50849
1917             FM4_1949         10.77038
1918             FM4_1949         0.50809
1920             AVE              2.5725
1923             AVE              4.8388
1927             AVE              4.11521
1932             AVE              5.2082
1933             AVE              13.351733
1938             FM10_1959        5.94603
1939             FM10_1959        1.288876
1940             FM10_1959        1.288876
1941             AVE              5.144045
1942             AVE              5.144045
1943             AVE              0.84575
1968             FM10_1959        1.447975
1969             FM10_1959        1.447975
1970             FM10_1959        1.19807
2029             FM12_1749        5.15448
2030             FM12_1749        1.35722
2031             FM12_1749        11.61302
2032             FM12_1749        2.325863
2033             FM12_1749        1.018583
2034             FM12_1749        1.018583
2035             FM12_1749        1.018583
2036             FM12_1749        28.9872
2063             FM7_401          0.276565
2096             AVE              1.283545
2097             AVE              1.283545
2105             FM7_401          1.04924
211              FM5_423          2.41987
213              FM5_423          1.52334
2140             FM11_61          38.518136
2140_1           FM11_61          38.518136
2140_2           FM11_61          38.518136
2140_3           FM11_61          38.518136
2140_4           FM11_61          38.518136
2146             FM2_1179         66.590267
2147             FM2_1179         66.590267
2148             FM2_1179         66.590267
2154             FM6_394          0.952805
2155             FM6_394          0.952805
216              FM5_423          3.25991
2179             FM12_1749        2.325863
2180             FM12_1749        2.325863
2217             FM7_401          1.36545
2218             FM7_401          0.51418
2219             FM7_401          1.88836
222              FM5_423          2.89872
2220             FM7_401          7.26742
2221             FM7_401          1.00109
2222             FM7_401          1.485988
2223             FM7_401          1.485988
2224             FM7_401          1.485988
2259             FM7_401          0.74918
2282_1           AVE              0.38199
2286             FM10_1959        0.837132
2300             FM2_1179         0.542344
```

2301	FM2_1179	0.542344
2302	FM2_1179	0.542344
2303	FM2_1179	0.542344
2304	FM1_3304	1.529633
2305	FM1_3304	1.529633
2306	FM1_3304	1.529633
2307	FM1_3304	13.21042
2309	FM1_3304	2.25156
231	FM5_423	2.05182
2310	FM1_3304	2.25156
2311	FM1_3304	2.25156
2312	FM1_3304	8.88035
2313	FM1_3304	1.244889
2314	FM1_3304	1.244889
2315	FM1_3304	1.244889
2317	FM1_3304	1.244889
2318	FM1_3304	1.244889
2319	FM1_3304	1.244889
2320	FM1_3304	1.244889
2321	FM1_3304	90.99965
2341	FM1_3304	17.106259
2342	FM1_3304	17.106259
2343	FM1_3304	17.106259
2344	FM1_3304	17.106259
2345	FM1_3304	17.106259
2346	FM1_3304	17.106259
2347	FM1_3304	17.106259
2348	FM1_3304	61.825715
2349	FM1_3304	61.825715
236	FM5_423	1.66495
2363	FM7_401	0.282997
2364	FM7_401	0.282997
2366	FM7_401	0.282997
2367	FM7_401	7.37048
2368	FM7_401	5.156359
2369	FM7_401	5.156359
2370	FM7_401	5.156359
2371	FM7_401	5.156359
2372	FM7_401	5.156359
2373	FM7_401	5.156359
2374	FM7_401	5.156359
2375	FM7_401	5.156359
2376	FM7_401	5.156359
2377	FM7_401	5.156359
2378	FM7_401	5.156359
2379	FM7_401	5.156359
2380	FM7_401	5.156359
2381	FM7_401	5.156359
2382	FM7_401	5.156359
2383	FM7_401	5.156359
2384	FM7_401	5.156359
2385	FM7_401	5.156359
2386	FM7_401	5.370974
2387	FM7_401	5.370974
2388	FM7_401	5.370974
2389	FM7_401	5.370974
2390	FM7_401	5.370974
2391	FM7_401	5.370974
2392	FM7_401	5.370974
2393	FM7_401	5.370974
2394	FM7_401	5.370974
2395	FM7_401	5.370974
2397	FM7_401	9.465105
2398	FM7_401	9.465105
2399	FM7_401	9.465105
2400	FM7_401	9.465105
2401	FM7_401	9.465105
2402	FM7_401	9.465105
2453	FM7_401	1.08965
2474	FM8_3505	1.013745
2475	FM8_3505	0.874892
2476	FM8_3505	0.874892
2477	FM8_3505	0.874892
284	FM6_394	0.952805
285	FM6_394	0.952805
286	FM6_394	0.952805
287	FM6_394	0.952805
288	FM6_394	0.952805
289	FM6_394	0.952805
290	FM6_394	24.242385
300	FM5_423	1.49934
3000	AVE	0.799177
3000A	AVE	0.799177
301	FM5_423	1.59882
302	FM5_423	4.35561
303	FM5_423	3.77882
360	AVE	69.97333
401	FM6_394	24.242385
402	FM6_394	32.60696
403	FM6_394	3.29417
406	AVE	0.38199
409	FM7_401	3.21118
411	AVE	0.73571
413	FM8_3505	0.874892
418	FM7_401	0.613507
419	FM8_3505	15.52588
421	FM7_401	0.613507
424	AVE	0.48394
425	AVE	0.37584
426	AVE	0.37584
428	FM9_415	0.72637
429	AVE	1.74316
431	FM8_3505	1.013745
432	FM8_3505	0.5456
434	FM8_3505	0.5456
435	FM5_423	1.66495
436	FM7_401	0.276565
439	FM7_401	0.613507
44	FM11_61	9.88636
446	FM9_415	1.076795
447	FM9_415	1.076795
448	FM9_415	1.076795
449	FM7_401	1.74581
45	FM11_61	87.78245
451	FM9_415	1.076795
452	FM8_3505	0.5456
453	FM9_415	0.592765
454	FM9_415	0.72637
457	FM7_401	1.78572
458	FM7_401	0.804263
459	FM7_401	0.804263
460	FM7_401	0.804263
462	FM8_3505	4.23788
463	FM8_3505	0.494145
464	FM8_3505	0.494145
465	FM9_415	0.592765
468	FM7_401	9.50252
469	FM7_401	3.407234
473	FM7_401	1.78268
477	FM7_401	3.407234
478	FM7_401	3.407234
479	FM7_401	3.390195
480	FM7_401	3.407234
481	FM7_401	3.407234
501	FM9_415	11.24585
502	FM9_415	1.174675
503	FM9_415	1.174675
506	FM9_415	4.58965
507	FM9_415	1.068613
508	FM9_415	1.068613
51	FM11_61	22.28355
511	FM9_415	60.85824
512	FM9_415	1.068613
513	FM9_415	0.5754
514	FM9_415	0.43379
521	FM9_415	1.89307
54	FM11_61	6.80527
55_1	FM11_61	5.56663
553	FM7_401	34.8074
554	FM7_401	1.87003
555	FM7_401	2.25
556	FM7_401	0.75163
56	FM11_61	5.56663
563	FM7_401	48.80734
63	FM11_61	5.56663
64	FM11_61	5.56663
649	FM7_401	2.43179
65	FM11_61	5.56663
650	FM7_401	0.95621
652	FM7_401	0.8354
653	FM7_401	2.32162
654	FM7_401	1.47052
666	FM7_401	10.514943
667	FM7_401	10.514943
668	FM7_401	10.514943
669	FM7_401	13.68624
670	FM7_401	3.047313
671	FM7_401	3.047313
672	FM7_401	3.047313
673	FM7_401	2.88993
675	FM7_401	1.10437
676	FM7_401	2.55577
678	FM7_401	0.82681
68	FM11_61	44.11614
682	FM7_401	0.61597
684	FM7_401	1.75703
685	FM7_401	0.61117
686	FM7_401	3.85539
689	FM7_401	1.72463
690	FM7_401	4.19537
708	FM7_401	89.27405
780	FM7_401	0.88331
781	FM7_401	1.17141
782	FM7_401	2.67768
783	FM7_401	4.05026
796	FM7_401	52.377
852	FM7_401	2.786519
853	FM7_401	2.786519
859	FM7_401	2.786519
860	FM7_401	2.786519
861	FM7_401	2.786519
864	FM7_401	38.5642
865	FM7_401	2.786519
866	FM7_401	2.786519
877	FM7_401	9.47923
878	FM7_401	0.85493
879	FM7_401	1.93404
880	FM7_401	1.374815
881	FM7_401	1.374815
882	FM7_401	6.47608
883	FM7_401	1.485988
884	FM7_401	1.485988
885	FM7_401	1.485988
886	FM7_401	3.390195
887	FM7_401	2.92247
9001	FM12_1749	0.776782
9002	FM12_1749	0.776782
9003	FM12_1749	0.776782
9004	FM12_1749	0.776782
9005	FM12_1749	0.776782
9006	FM12_1749	5.60903
9050	FM10_1959	0.837132
9051	FM10_1959	0.837132
9052	FM10_1959	0.837132
9053	FM10_1959	0.837132
9054	FM10_1959	0.837132
9055	FM10_1959	0.837132
9056	FM10_1959	13.36993
9057	FM10_1959	0.837132
9058	FM10_1959	0.837132
9059	FM10_1959	0.837132
9060	FM10_1959	0.837132

```
9061             FM10_1959       0.837132
924              FM3_932         33.59186
940              FM9_415         1.51142
942              FM9_415         2.39708
978              AVE             5.3745
984              AVE             2.27206
985              AVE             0.799177
986              AVE             0.799177
987              AVE             0.799177
988              AVE             0.799177
991              AVE             0.467
996              AVE             2.80203
997              AVE             0.21781
999              AVE             1.49863

[CURVES]
;;Name           Type       X-Value    Y-Value
;;-------------- ---------- ---------- ----------
;Front Street PS - Pumps #1 & #3
100_D5731CW      Pump3      15.09      0.473
100_D5731CW                 16.46      0.442
100_D5731CW                 18.9       0.379
100_D5731CW                 20.73      0.315
100_D5731CW                 21.95      0.252
100_D5731CW                 22.86      0.189
100_D5731CW                 23.47      0.126
100_D5731CW                 23.77      0.063
100_D5731CW                 24.38      0

;Pump running at 100%
;Dundas Palmer PS
100_NT3202.090MT Pump3      7.5        0.245
100_NT3202.090MT            10         0.22
100_NT3202.090MT            12.5       0.193
100_NT3202.090MT            15         0.165
100_NT3202.090MT            17.5       0.135
100_NT3202.090MT            20         0.1
100_NT3202.090MT            22.5       0.06
100_NT3202.090MT            25         0.035
100_NT3202.090MT            27.5       0.015

;Front Street PS - Pump #2
100_NT3301LT3    Pump3      4          0.6
100_NT3301LT3               6.5        0.5
100_NT3301LT3               9          0.4
100_NT3301LT3               11.2       0.3
100_NT3301LT3               13         0.2
100_NT3301LT3               15         0.1
100_NT3301LT3               17.5       0

;Front Street PS - Pump #4
100_NT3315LT3_626 Pump3      10         0.5
100_NT3315LT3_626            12.8       0.45
100_NT3315LT3_626            15.6       0.4
100_NT3315LT3_626            18.5       0.35
100_NT3315LT3_626            21         0.3
100_NT3315LT3_626            23.2       0.25
100_NT3315LT3_626            24.6       0.2
100_NT3315LT3_626            26.8       0.15
100_NT3315LT3_626            30         0.1
100_NT3315LT3_626            33.4       0.05
100_NT3315LT3_626            35.7       0

;Pump running at 75%
;Dundas Palmer PS
;Q=Q100*0.75
;TDH=TDH100*(0.75^2)
75_NT3202.090MT  Pump3      4.22       0.184
75_NT3202.090MT             5.63       0.165
75_NT3202.090MT             7.03       0.145
75_NT3202.090MT             8.44       0.124
75_NT3202.090MT             9.84       0.101
75_NT3202.090MT             11.25      0.075
75_NT3202.090MT             12.66      0.045
75_NT3202.090MT             14.06      0.026
75_NT3202.090MT             15.47      0.011

;Curve constructed from testing undertaken in 1996 by Omega Public Works
K4D1-604400_#1   Pump4      1.08       0
K4D1-604400_#1              1.25       0.2

;Curve constructed from testing undertaken in 1996 by Omega Public Works
K4D1-604400_#2   Pump4      1.17       0
K4D1-604400_#2              1.4        0.2

;Curve constructed from testing undertaken in 1996 by Omega Public Works
K4D1-604400_#3   Pump3      6.3        0.2
K4D1-604400_#3              8.4        0.175
K4D1-604400_#3              21.8       0

;Curve constructed from testing undertaken in 1996 by Omega Public Works
K4D1-604400_#4   Pump3      6.2        0.2
K4D1-604400_#4              8.4        0.175
K4D1-604400_#4              21.8       0

[TIMESERIES]
;;Name           Date       Time       Value
;;-------------- ---------- ---------- ----------
;SCS_Type_II_104.4mm design storm, total rainfall = 104.4 mm, rain units = mm/hr.
100yrSCS                    0:00       1.148
100yrSCS                    0:15       1.148
100yrSCS                    0:30       1.148
100yrSCS                    0:45       1.148
100yrSCS                    1:00       1.148
100yrSCS                    1:15       1.148
100yrSCS                    1:30       1.148
100yrSCS                    1:45       1.148
100yrSCS                    2:00       1.357
100yrSCS                    2:15       1.357
100yrSCS                    2:30       1.357
100yrSCS                    2:45       1.357
100yrSCS                    3:00       1.357
100yrSCS                    3:15       1.357
100yrSCS                    3:30       1.357
100yrSCS                    3:45       1.357
100yrSCS                    4:00       1.67
100yrSCS                    4:15       1.67
100yrSCS                    4:30       1.67
100yrSCS                    4:45       1.67
100yrSCS                    5:00       1.67
100yrSCS                    5:15       1.67
100yrSCS                    5:30       1.67
100yrSCS                    5:45       1.67
100yrSCS                    6:00       1.879
100yrSCS                    6:15       1.879
100yrSCS                    6:30       1.879
100yrSCS                    6:45       1.879
100yrSCS                    7:00       2.297
100yrSCS                    7:15       2.297
100yrSCS                    7:30       2.297
100yrSCS                    7:45       2.297
100yrSCS                    8:00       2.714
100yrSCS                    8:15       2.714
100yrSCS                    8:30       2.923
100yrSCS                    8:45       2.923
100yrSCS                    9:00       3.341
100yrSCS                    9:15       3.341
100yrSCS                    9:30       3.758
100yrSCS                    9:45       3.758
100yrSCS                    10:00      4.802
100yrSCS                    10:15      4.802
100yrSCS                    10:30      6.473
100yrSCS                    10:45      6.473
100yrSCS                    11:00      10.022
100yrSCS                    11:15      10.022
100yrSCS                    11:30      30.902
100yrSCS                    11:45      127.786
100yrSCS                    12:00      15.034
100yrSCS                    12:15      15.034
100yrSCS                    12:30      7.726
100yrSCS                    12:45      7.726
100yrSCS                    13:00      5.638
100yrSCS                    13:15      5.638
100yrSCS                    13:30      4.385
100yrSCS                    13:45      4.385
100yrSCS                    14:00      3.132
100yrSCS                    14:15      3.132
100yrSCS                    14:30      3.132
100yrSCS                    14:45      3.132
100yrSCS                    15:00      3.132
100yrSCS                    15:15      3.132
100yrSCS                    15:30      3.132
100yrSCS                    15:45      3.132
100yrSCS                    16:00      1.879
100yrSCS                    16:15      1.879
100yrSCS                    16:30      1.879
100yrSCS                    16:45      1.879
100yrSCS                    17:00      1.879
100yrSCS                    17:15      1.879
100yrSCS                    17:30      1.879
100yrSCS                    17:45      1.879
100yrSCS                    18:00      1.879
100yrSCS                    18:15      1.879
100yrSCS                    18:30      1.879
100yrSCS                    18:45      1.879
100yrSCS                    19:00      1.879
100yrSCS                    19:15      1.879
100yrSCS                    19:30      1.879
100yrSCS                    19:45      1.879
100yrSCS                    20:00      1.253
100yrSCS                    20:15      1.253
100yrSCS                    20:30      1.253
100yrSCS                    20:45      1.253
100yrSCS                    21:00      1.253
100yrSCS                    21:15      1.253
100yrSCS                    21:30      1.253
100yrSCS                    21:45      1.253
100yrSCS                    22:00      1.253
100yrSCS                    22:15      1.253
100yrSCS                    22:30      1.253
100yrSCS                    22:45      1.253
100yrSCS                    23:00      1.253
100yrSCS                    23:15      1.253
100yrSCS                    23:30      1.253
100yrSCS                    23:45      1.253

;Rainfall (mm/hr)
CHI_3hr_100yr    03/13/2018 02:10:00   6.943
CHI_3hr_100yr    03/13/2018 02:20:00   8.39
CHI_3hr_100yr    03/13/2018 02:30:00   10.805
CHI_3hr_100yr    03/13/2018 02:40:00   15.817
CHI_3hr_100yr    03/13/2018 02:50:00   35.004
CHI_3hr_100yr    03/13/2018 03:00:00   143.732
CHI_3hr_100yr    03/13/2018 03:10:00   45.11
CHI_3hr_100yr    03/13/2018 03:20:00   24.942
CHI_3hr_100yr    03/13/2018 03:30:00   17.717
CHI_3hr_100yr    03/13/2018 03:40:00   13.95
CHI_3hr_100yr    03/13/2018 03:50:00   11.616
CHI_3hr_100yr    03/13/2018 04:00:00   10.017
CHI_3hr_100yr    03/13/2018 04:10:00   8.848
CHI_3hr_100yr    03/13/2018 04:20:00   7.952
CHI_3hr_100yr    03/13/2018 04:30:00   7.241
CHI_3hr_100yr    03/13/2018 04:40:00   6.662
CHI_3hr_100yr    03/13/2018 04:50:00   6.18
CHI_3hr_100yr    03/13/2018 05:00:00   5.772

;Rainfall (mm/hr)
Intensity        03/13/2018 02:10:00   0
Intensity        03/13/2018 02:15:00   0
Intensity        03/13/2018 02:20:00   0
Intensity        03/13/2018 02:25:00   0
Intensity        03/13/2018 02:30:00   0
```

```
Intensity       03/13/2018 02:35:00   0
Intensity       03/13/2018 02:40:00   0
Intensity       03/13/2018 02:45:00   0
Intensity       03/13/2018 02:50:00   0
Intensity       03/13/2018 02:55:00   0
Intensity       03/13/2018 03:00:00   0
......
Too many data points (26020 in total).

;Rainfall (mm/hr)
SCS_24hr_100yr   03/13/2018 02:10:00   1.148
SCS_24hr_100yr   03/13/2018 02:25:00   1.148
SCS_24hr_100yr   03/13/2018 02:40:00   1.148
SCS_24hr_100yr   03/13/2018 02:55:00   1.148
SCS_24hr_100yr   03/13/2018 03:10:00   1.148
SCS_24hr_100yr   03/13/2018 03:25:00   1.148
SCS_24hr_100yr   03/13/2018 03:40:00   1.148
SCS_24hr_100yr   03/13/2018 03:55:00   1.148
SCS_24hr_100yr   03/13/2018 04:10:00   1.357
SCS_24hr_100yr   03/13/2018 04:25:00   1.357
SCS_24hr_100yr   03/13/2018 04:40:00   1.357
SCS_24hr_100yr   03/13/2018 04:55:00   1.357
SCS_24hr_100yr   03/13/2018 05:10:00   1.357
SCS_24hr_100yr   03/13/2018 05:25:00   1.357
SCS_24hr_100yr   03/13/2018 05:40:00   1.357
SCS_24hr_100yr   03/13/2018 05:55:00   1.357
SCS_24hr_100yr   03/13/2018 06:10:00   1.67
SCS_24hr_100yr   03/13/2018 06:25:00   1.67
SCS_24hr_100yr   03/13/2018 06:40:00   1.67
SCS_24hr_100yr   03/13/2018 06:55:00   1.67
SCS_24hr_100yr   03/13/2018 07:10:00   1.67
SCS_24hr_100yr   03/13/2018 07:25:00   1.67
SCS_24hr_100yr   03/13/2018 07:40:00   1.67
SCS_24hr_100yr   03/13/2018 07:55:00   1.67
SCS_24hr_100yr   03/13/2018 08:10:00   1.879
SCS_24hr_100yr   03/13/2018 08:25:00   1.879
SCS_24hr_100yr   03/13/2018 08:40:00   1.879
SCS_24hr_100yr   03/13/2018 08:55:00   1.879
SCS_24hr_100yr   03/13/2018 09:10:00   2.297
SCS_24hr_100yr   03/13/2018 09:25:00   2.297
SCS_24hr_100yr   03/13/2018 09:40:00   2.297
SCS_24hr_100yr   03/13/2018 09:55:00   2.297
SCS_24hr_100yr   03/13/2018 10:10:00   2.714
SCS_24hr_100yr   03/13/2018 10:25:00   2.714
SCS_24hr_100yr   03/13/2018 10:40:00   2.923
SCS_24hr_100yr   03/13/2018 10:55:00   2.923
SCS_24hr_100yr   03/13/2018 11:10:00   3.341
SCS_24hr_100yr   03/13/2018 11:25:00   3.341
SCS_24hr_100yr   03/13/2018 11:40:00   3.758
SCS_24hr_100yr   03/13/2018 11:55:00   3.758
SCS_24hr_100yr   03/13/2018 12:10:00   4.802
SCS_24hr_100yr   03/13/2018 12:25:00   4.802
SCS_24hr_100yr   03/13/2018 12:40:00   6.473
SCS_24hr_100yr   03/13/2018 12:55:00   6.473
SCS_24hr_100yr   03/13/2018 13:10:00   10.022
SCS_24hr_100yr   03/13/2018 13:25:00   10.022
SCS_24hr_100yr   03/13/2018 13:40:00   30.902
SCS_24hr_100yr   03/13/2018 13:55:00   127.786
SCS_24hr_100yr   03/13/2018 14:10:00   15.034
SCS_24hr_100yr   03/13/2018 14:25:00   15.034
SCS_24hr_100yr   03/13/2018 14:40:00   7.726
SCS_24hr_100yr   03/13/2018 14:55:00   7.726
SCS_24hr_100yr   03/13/2018 15:10:00   5.638
SCS_24hr_100yr   03/13/2018 15:25:00   5.638
SCS_24hr_100yr   03/13/2018 15:40:00   4.385
SCS_24hr_100yr   03/13/2018 15:55:00   4.385
SCS_24hr_100yr   03/13/2018 16:10:00   3.132
SCS_24hr_100yr   03/13/2018 16:25:00   3.132
SCS_24hr_100yr   03/13/2018 16:40:00   3.132
SCS_24hr_100yr   03/13/2018 16:55:00   3.132
SCS_24hr_100yr   03/13/2018 17:10:00   3.132
SCS_24hr_100yr   03/13/2018 17:25:00   3.132
SCS_24hr_100yr   03/13/2018 17:40:00   3.132
SCS_24hr_100yr   03/13/2018 17:55:00   3.132
SCS_24hr_100yr   03/13/2018 18:10:00   1.879
SCS_24hr_100yr   03/13/2018 18:25:00   1.879
SCS_24hr_100yr   03/13/2018 18:40:00   1.879
SCS_24hr_100yr   03/13/2018 18:55:00   1.879
SCS_24hr_100yr   03/13/2018 19:10:00   1.879
SCS_24hr_100yr   03/13/2018 19:25:00   1.879
SCS_24hr_100yr   03/13/2018 19:40:00   1.879
SCS_24hr_100yr   03/13/2018 19:55:00   1.879
SCS_24hr_100yr   03/13/2018 20:10:00   1.879
SCS_24hr_100yr   03/13/2018 20:25:00   1.879
SCS_24hr_100yr   03/13/2018 20:40:00   1.879
SCS_24hr_100yr   03/13/2018 20:55:00   1.879
SCS_24hr_100yr   03/13/2018 21:10:00   1.879
SCS_24hr_100yr   03/13/2018 21:25:00   1.879
SCS_24hr_100yr   03/13/2018 21:40:00   1.879
SCS_24hr_100yr   03/13/2018 21:55:00   1.879
SCS_24hr_100yr   03/13/2018 22:10:00   1.253
SCS_24hr_100yr   03/13/2018 22:25:00   1.253
SCS_24hr_100yr   03/13/2018 22:40:00   1.253
SCS_24hr_100yr   03/13/2018 22:55:00   1.253
SCS_24hr_100yr   03/13/2018 23:10:00   1.253
SCS_24hr_100yr   03/13/2018 23:25:00   1.253
SCS_24hr_100yr   03/13/2018 23:40:00   1.253
SCS_24hr_100yr   03/13/2018 23:55:00   1.253
SCS_24hr_100yr   03/14/2018 00:10:00   1.253
SCS_24hr_100yr   03/14/2018 00:25:00   1.253
SCS_24hr_100yr   03/14/2018 00:40:00   1.253
SCS_24hr_100yr   03/14/2018 00:55:00   1.253
SCS_24hr_100yr   03/14/2018 01:10:00   1.253
SCS_24hr_100yr   03/14/2018 01:25:00   1.253
SCS_24hr_100yr   03/14/2018 01:40:00   1.253
SCS_24hr_100yr   03/14/2018 01:55:00   1.253

;SCS_Type_II_74.4mm design storm, total rainfall = 74.4 mm, rain units = mm/hr.
SCS_24hr_10yr              0:00       0.818
SCS_24hr_10yr              0:15       0.818
SCS_24hr_10yr              0:30       0.818
SCS_24hr_10yr              0:45       0.818
SCS_24hr_10yr              1:00       0.818
SCS_24hr_10yr              1:15       0.818
SCS_24hr_10yr              1:30       0.818
SCS_24hr_10yr              1:45       0.818
SCS_24hr_10yr              2:00       0.967
SCS_24hr_10yr              2:15       0.967
SCS_24hr_10yr              2:30       0.967
SCS_24hr_10yr              2:45       0.967
SCS_24hr_10yr              3:00       0.967
SCS_24hr_10yr              3:15       0.967
SCS_24hr_10yr              3:30       0.967
SCS_24hr_10yr              3:45       0.967
SCS_24hr_10yr              4:00       1.19
SCS_24hr_10yr              4:15       1.19
SCS_24hr_10yr              4:30       1.19
SCS_24hr_10yr              4:45       1.19
SCS_24hr_10yr              5:00       1.19
SCS_24hr_10yr              5:15       1.19
SCS_24hr_10yr              5:30       1.19
SCS_24hr_10yr              5:45       1.19
SCS_24hr_10yr              6:00       1.339
SCS_24hr_10yr              6:15       1.339
SCS_24hr_10yr              6:30       1.339
SCS_24hr_10yr              6:45       1.339
SCS_24hr_10yr              7:00       1.637
SCS_24hr_10yr              7:15       1.637
SCS_24hr_10yr              7:30       1.637
SCS_24hr_10yr              7:45       1.637
SCS_24hr_10yr              8:00       1.934
SCS_24hr_10yr              8:15       1.934
SCS_24hr_10yr              8:30       2.083
SCS_24hr_10yr              8:45       2.083
SCS_24hr_10yr              9:00       2.381
SCS_24hr_10yr              9:15       2.381
SCS_24hr_10yr              9:30       2.678
SCS_24hr_10yr              9:45       2.678
SCS_24hr_10yr              10:00      3.422
SCS_24hr_10yr              10:15      3.422
SCS_24hr_10yr              10:30      4.613
SCS_24hr_10yr              10:45      4.613
SCS_24hr_10yr              11:00      7.142
SCS_24hr_10yr              11:15      7.142
SCS_24hr_10yr              11:30      22.022
SCS_24hr_10yr              11:45      91.066
SCS_24hr_10yr              12:00      10.714
SCS_24hr_10yr              12:15      10.714
SCS_24hr_10yr              12:30      5.506
SCS_24hr_10yr              12:45      5.506
SCS_24hr_10yr              13:00      4.018
SCS_24hr_10yr              13:15      4.018
SCS_24hr_10yr              13:30      3.125
SCS_24hr_10yr              13:45      3.125
SCS_24hr_10yr              14:00      2.232
SCS_24hr_10yr              14:15      2.232
SCS_24hr_10yr              14:30      2.232
SCS_24hr_10yr              14:45      2.232
SCS_24hr_10yr              15:00      2.232
SCS_24hr_10yr              15:15      2.232
SCS_24hr_10yr              15:30      2.232
SCS_24hr_10yr              15:45      2.232
SCS_24hr_10yr              16:00      1.339
SCS_24hr_10yr              16:15      1.339
SCS_24hr_10yr              16:30      1.339
SCS_24hr_10yr              16:45      1.339
SCS_24hr_10yr              17:00      1.339
SCS_24hr_10yr              17:15      1.339
SCS_24hr_10yr              17:30      1.339
SCS_24hr_10yr              17:45      1.339
SCS_24hr_10yr              18:00      1.339
SCS_24hr_10yr              18:15      1.339
SCS_24hr_10yr              18:30      1.339
SCS_24hr_10yr              18:45      1.339
SCS_24hr_10yr              19:00      1.339
SCS_24hr_10yr              19:15      1.339
SCS_24hr_10yr              19:30      1.339
SCS_24hr_10yr              19:45      1.339
SCS_24hr_10yr              20:00      0.893
SCS_24hr_10yr              20:15      0.893
SCS_24hr_10yr              20:30      0.893
SCS_24hr_10yr              20:45      0.893
SCS_24hr_10yr              21:00      0.893
SCS_24hr_10yr              21:15      0.893
SCS_24hr_10yr              21:30      0.893
SCS_24hr_10yr              21:45      0.893
SCS_24hr_10yr              22:00      0.893
SCS_24hr_10yr              22:15      0.893
SCS_24hr_10yr              22:30      0.893
SCS_24hr_10yr              22:45      0.893
SCS_24hr_10yr              23:00      0.893
SCS_24hr_10yr              23:15      0.893
SCS_24hr_10yr              23:30      0.893
SCS_24hr_10yr              23:45      0.893

;Rainfall (mm/hr)
Zero_Rainfall    03/13/2018 02:10:00   0
Zero_Rainfall    03/13/2018 02:20:00   0
Zero_Rainfall    03/13/2018 02:30:00   0
Zero_Rainfall    03/13/2018 02:40:00   0
Zero_Rainfall    03/13/2018 02:50:00   0
Zero_Rainfall    03/13/2018 03:00:00   0
Zero_Rainfall    03/13/2018 03:10:00   0
Zero_Rainfall    03/13/2018 03:20:00   0
Zero_Rainfall    03/13/2018 03:30:00   0
Zero_Rainfall    03/13/2018 03:40:00   0
Zero_Rainfall    03/13/2018 03:50:00   0
Zero_Rainfall    03/13/2018 04:00:00   0
Zero_Rainfall    03/13/2018 04:10:00   0
Zero_Rainfall    03/13/2018 04:20:00   0
Zero_Rainfall    03/13/2018 04:30:00   0
Zero_Rainfall    03/13/2018 04:40:00   0
```

```
Zero_Rainfall    03/13/2018 04:50:00   0
Zero_Rainfall    03/13/2018 05:00:00   0

[PATTERNS]
;;Name           Type       Multipliers
;;-------------- ---------- -----------
;Daily pattern generated from time series '1179 (obs)'.  Average value was 0.0873 m³/s.
1179_(obs)_Daily DAILY      0.945 0.981 1.04  1.038 1.037 1.01  0.951
;
;Hourly pattern generated from time series '1179 (obs)'.  Average value was 0.0873 m³/s.
1179_(obs)_Hourly HOURLY     0.966 0.964 0.955 0.951 0.945 0.951
1179_(obs)_Hourly            0.965 0.979 1.032 1.029 1.047 1.041
1179_(obs)_Hourly            1.054 1.042 1.046 1.031 1.006 1.017
1179_(obs)_Hourly            1.01  1.022 0.988 1     0.985 0.974
;
;Weekend pattern generated from time series '0'.  Average value was 0.0873 m³/s.
1179_(obs)_Weekend HOURLY     0.994 1.003 0.975 1.004 0.985 0.986
1179_(obs)_Weekend            0.995 1.016 1.04  1.022 1.012 1.018
1179_(obs)_Weekend            1.008 1.018 1.019 0.999 0.999 0.987
1179_(obs)_Weekend            0.963 0.997 0.985 0.999 0.996 0.982
;
;Daily pattern generated from time series '1749 (obs)'.  Average value was 0.014 m³/s.
1749_(obs)_Daily DAILY      1.067 0.97  0.948 0.982 1.016 0.968 1.049
;
;Hourly pattern generated from time series '1749 (obs)'.  Average value was 0.014 m³/s.
1749_(obs)_Hourly HOURLY     0.85  0.698 0.636 0.665 0.665 0.747
1749_(obs)_Hourly            0.973 1.25  1.323 1.223 1.138 1.05
1749_(obs)_Hourly            1.02  1.004 0.973 0.964 0.995 1.048
1749_(obs)_Hourly            1.112 1.154 1.21  1.199 1.118 0.984
;
;Weekend pattern generated from time series '0'.  Average value was 0.014 m³/s.
1749_(obs)_Weekend HOURLY     0.785 0.708 0.658 0.638 0.646 0.669
1749_(obs)_Weekend            0.737 0.914 1.139 1.351 1.34  1.311
1749_(obs)_Weekend            1.229 1.118 1.074 1.068 1.048 1.081
1749_(obs)_Weekend            1.114 1.155 1.154 1.113 1.043 0.906
;
;Daily pattern generated from time series '1949 (obs)'.  Average value was 0.0202 m³/s.
1949_(obs)_Daily DAILY      1.04  1.008 0.914 0.964 1.015 0.985 1.073
;
;Hourly pattern generated from time series '1949 (obs)'.  Average value was 0.0202 m³/s.
1949_(obs)_Hourly HOURLY     0.83  0.767 0.77  0.754 0.763 0.838
1949_(obs)_Hourly            1.053 1.162 1.174 1.205 1.136 1.075
1949_(obs)_Hourly            1.076 1.038 1.057 1.027 1.04  1.059
1949_(obs)_Hourly            1.023 1.1   1.073 1.066 1.006 0.907
;
;Weekend pattern generated from time series '0'.  Average value was 0.0202 m³/s.
1949_(obs)_Weekend HOURLY     0.856 0.81  0.787 0.788 0.779 0.804
1949_(obs)_Weekend            0.885 1     1.167 1.11  1.193 1.175
1949_(obs)_Weekend            1.179 1.064 1.045 1.038 1.014 1.039
1949_(obs)_Weekend            1.03  1.115 1.115 1.068 1.019 0.92
;
;Daily pattern generated from time series '1959 (obs)'.  Average value was 0.0468 m³/s.
1959_(obs)_Daily DAILY      1.064 0.97  0.922 0.97  1.018 0.998 1.059
;
;Hourly pattern generated from time series '1959 (obs)'.  Average value was 0.0468 m³/s.
1959_(obs)_Hourly HOURLY     0.937 0.853 0.83  0.79  0.783 0.782
1959_(obs)_Hourly            0.822 0.971 1.139 1.2   1.161 1.139
1959_(obs)_Hourly            1.093 1.079 1.04  1.028 1.001 1.01
1959_(obs)_Hourly            1.039 1.041 1.09  1.108 1.057 1.006
;
;Weekend pattern generated from time series '0'.  Average value was 0.0468 m³/s.
1959_(obs)_Weekend HOURLY     0.925 0.897 0.832 0.794 0.783 0.768
1959_(obs)_Weekend            0.79  0.829 0.944 1.09  1.211 1.223
1959_(obs)_Weekend            1.201 1.17  1.13  1.075 1.046 1.04
1959_(obs)_Weekend            1.04  1.06  1.074 1.075 1.037 0.965
;
;Daily pattern generated from time series '3304 (obs)'.  Average value was 0.016 m³/s.
3304_(obs)_Daily DAILY      1.207 1.051 0.833 0.907 0.981 0.949 1.073
;
;Hourly pattern generated from time series '3304 (obs)'.  Average value was 0.016 m³/s.
3304_(obs)_Hourly HOURLY     0.801 0.706 0.637 0.635 0.633 0.668
3304_(obs)_Hourly            0.867 1.379 1.378 1.249 1.149 1.059
3304_(obs)_Hourly            1.024 1.028 1.01  0.933 0.989 1.048
3304_(obs)_Hourly            1.123 1.118 1.264 1.219 1.11  0.973
;
;Weekend pattern generated from time series '0'.  Average value was 0.016 m³/s.
3304_(obs)_Weekend HOURLY     0.762 0.67  0.686 0.581 0.59  0.587
3304_(obs)_Weekend            0.661 0.805 1.052 1.348 1.419 1.359
3304_(obs)_Weekend            1.26  1.155 1.159 1.087 1.072 1.078
3304_(obs)_Weekend            1.155 1.17  1.231 1.16  1.032 0.922
;
;Daily pattern generated from time series '3505 (obs)'.  Average value was 0.0127 m³/s.
3505_(obs)_Daily DAILY      1.024 0.984 0.931 1.001 1.072 0.995 0.993
;
;Hourly pattern generated from time series '3505 (obs)'.  Average value was 0.0127 m³/s.
3505_(obs)_Hourly HOURLY     0.871 0.825 0.833 0.824 0.833 0.927
3505_(obs)_Hourly            1.031 1.116 1.127 1.11  1.077 1.057
3505_(obs)_Hourly            1.049 1.045 1.011 1     1.018 1.023
3505_(obs)_Hourly            1.044 1.072 1.086 1.076 1.014 0.931
;
;Weekend pattern generated from time series '0'.  Average value was 0.0127 m³/s.
3505_(obs)_Weekend HOURLY     0.868 0.83  0.82  0.813 0.821 0.859
3505_(obs)_Weekend            0.927 1.008 1.085 1.128 1.154 1.122
3505_(obs)_Weekend            1.062 1.049 1.033 1.035 1.046 1.058
3505_(obs)_Weekend            1.08  1.093 1.092 1.063 1.018 0.936
;
;Daily pattern generated from time series '394 (obs)'.  Average value was 0.0229 m³/s.
394_(obs)_Daily  DAILY      1.046 1.016 0.943 0.998 1.052 0.952 0.993
;
;Hourly pattern generated from time series '394 (obs)'.  Average value was 0.0229 m³/s.
394_(obs)_Hourly HOURLY     0.609 0.527 0.406 0.41  0.41  0.576
394_(obs)_Hourly            0.922 1.419 1.455 1.357 1.388 1.309
394_(obs)_Hourly            1.231 1.199 1.144 1.062 1.043 1.029
394_(obs)_Hourly            1.117 1.109 1.193 1.138 1.088 0.857
;
;Weekend pattern generated from time series '0'.  Average value was 0.0229 m³/s.
394_(obs)_Weekend HOURLY     0.633 0.531 0.453 0.457 0.442 0.476
394_(obs)_Weekend            0.696 0.91  1.227 1.4   1.497 1.43
394_(obs)_Weekend            1.338 1.277 1.203 1.086 1.106 1.139
394_(obs)_Weekend            1.146 1.226 1.202 1.18  1.079 0.869
;
;Daily pattern generated from time series '401 (obs)'.  Average value was 0.0646 m³/s.
401_(obs)_Daily  DAILY      0.93  1.129 0.972 1.039 1.105 1.083 0.741
;
;Hourly pattern generated from time series '401 (obs)'.  Average value was 0.0646 m³/s.
401_(obs)_Hourly HOURLY     0.876 0.729 0.649 0.614 0.603 0.637
401_(obs)_Hourly            0.78  0.996 1.105 1.114 1.107 1.131
401_(obs)_Hourly            1.126 1.124 1.132 1.085 1.093 1.136
401_(obs)_Hourly            1.186 1.222 1.214 1.176 1.152 1.013
;
;Weekend pattern generated from time series '0'.  Average value was 0.0646 m³/s.
401_(obs)_Weekend HOURLY     0.8   0.727 0.622 0.586 0.569 0.556
401_(obs)_Weekend            0.628 0.749 0.945 1.099 1.184 1.266
401_(obs)_Weekend            1.266 1.222 1.335 1.242 1.214 1.231
401_(obs)_Weekend            1.206 1.217 1.167 1.141 1.083 0.946
;
;Daily pattern generated from time series '415 (obs)'.  Average value was 0.0215 m³/s.
415_(obs)_Daily  DAILY      1.048 0.953 0.9   0.978 1.055 1.015 1.052
;
;Hourly pattern generated from time series '415 (obs)'.  Average value was 0.0215 m³/s.
415_(obs)_Hourly HOURLY     0.831 0.794 0.763 0.763 0.765 0.806
415_(obs)_Hourly            0.902 1.209 1.221 1.162 1.129 1.093
415_(obs)_Hourly            1.065 1.027 0.991 1.01  0.992 0.972
415_(obs)_Hourly            1.046 1.093 1.157 1.153 1.128 0.929
;
;Weekend pattern generated from time series '0'.  Average value was 0.0215 m³/s.
415_(obs)_Weekend HOURLY     0.774 0.751 0.747 0.762 0.737 0.745
415_(obs)_Weekend            0.752 0.822 1.12  1.156 1.162 1.157
415_(obs)_Weekend            1.177 1.184 1.156 1.079 0.996 1.086
415_(obs)_Weekend            1.144 1.168 1.166 1.182 1.097 0.879
;
;Daily pattern generated from time series '423 (obs)'.  Average value was 0.00927 m³/s.
423_(obs)_Daily  DAILY      1.09  1.016 0.926 0.963 0.999 0.955 1.051
;
;Hourly pattern generated from time series '423 (obs)'.  Average value was 0.00927 m³/s.
423_(obs)_Hourly HOURLY     0.908 0.865 0.856 0.846 0.878 0.931
423_(obs)_Hourly            1.017 1.108 1.069 1.057 1.055 1.041
423_(obs)_Hourly            1.023 1.006 1.006 0.99  1.009 1.027
423_(obs)_Hourly            1.056 1.073 1.078 1.103 1.038 0.958
;
;Weekend pattern generated from time series '0'.  Average value was 0.00927 m³/s.
423_(obs)_Weekend HOURLY     0.889 0.864 0.834 0.815 0.821 0.857
423_(obs)_Weekend            0.901 0.993 1.056 1.111 1.104 1.076
423_(obs)_Weekend            1.049 1.037 1.044 1.043 1.049 1.049
423_(obs)_Weekend            1.074 1.116 1.134 1.118 1.025 0.94
;
;Daily pattern generated from time series '61 (obs)'.  Average value was 0.0116 m³/s.
61_(obs)_Daily   DAILY      1.058 1.015 0.945 0.971 0.998 0.969 1.045
;
;Hourly pattern generated from time series '61 (obs)'.  Average value was 0.0116 m³/s.
61_(obs)_Hourly  HOURLY     0.711 0.618 0.578 0.551 0.583 0.665
61_(obs)_Hourly             0.966 1.358 1.337 1.254 1.263 1.183
61_(obs)_Hourly             1.158 1.134 1.114 1.095 1.037 1.016
61_(obs)_Hourly             1.121 1.11  1.172 1.084 1.003 0.889
;
;Weekend pattern generated from time series '0'.  Average value was 0.0116 m³/s.
61_(obs)_Weekend HOURLY     0.729 0.674 0.642 0.59  0.601 0.642
61_(obs)_Weekend            0.751 0.944 1.161 1.338 1.372 1.309
61_(obs)_Weekend            1.247 1.19  1.092 1.108 1.061 1.052
61_(obs)_Weekend            1.126 1.13  1.139 1.13  1.095 0.879
;
;Daily pattern generated from time series '932 (obs)'.  Average value was 0.00589 m³/s.
932_(obs)_Daily  DAILY      0.984 1.021 1.002 0.991 1.021 1.001 0.979
;
;Hourly pattern generated from time series '932 (obs)'.  Average value was 0.00589 m³/s.
932_(obs)_Hourly HOURLY     0.921 0.912 0.911 0.901 0.906 0.929
932_(obs)_Hourly            0.996 1.076 1.083 1.05  1.045 1.038
932_(obs)_Hourly            1.026 1.028 1.007 1.013 1.031 1.028
932_(obs)_Hourly            1.043 1.068 1.044 1.025 0.975 0.945
;
;Weekend pattern generated from time series '0'.  Average value was 0.00589 m³/s.
932_(obs)_Weekend HOURLY     0.927 0.89  0.904 0.891 0.896 0.916
932_(obs)_Weekend            0.944 0.992 1.054 1.107 1.095 1.055
932_(obs)_Weekend            1.054 1.027 1.039 1.036 1.019 1.014
932_(obs)_Weekend            1.047 1.063 1.048 1.028 0.999 0.953
;
;Average pattern from all monitored flows
AVE_Hourly       HOURLY     0.829 0.752 0.728 0.713 0.713 0.787
AVE_Hourly                  0.95  1.171 1.207 1.173 1.146 1.106
AVE_Hourly                  1.085 1.066 1.051 1.022 1.026 1.042
AVE_Hourly                  1.083 1.103 1.139 1.118 1.049 0.943
;
;Average pattern from all monitored flows
AVE_Weekend      HOURLY     0.822 0.776 0.735 0.712 0.71  0.731
AVE_Weekend                 0.808 0.928 1.091 1.197 1.238 1.217
AVE_Weekend                 1.175 1.125 1.11  1.075 1.065 1.072
AVE_Weekend                 1.089 1.128 1.132 1.106 1.039 0.92

[REPORT]
;;Reporting Options
INPUT      YES
CONTROLS   NO
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL

[TAGS]
Node       1048             Pressured
Node       1050             Pressured
Node       1050_1           Pressured
Node       1050_2           Pressured
Node       1175             Pressured
Node       1176             Pressured
Node       1177             Pressured
Node       1178             Pressured
Node       1179             Pressured
Node       1180             Pressured
Node       1181             Pressured
Node       1182             Pressured
Node       2151             Pressured
Node       2152             Pressured
Node       2271             Pressured
```

Node	2272	Pressured
Node	2273	Pressured
Node	2275	Pressured
Node	2276	Pressured
Node	2277	Pressured
Node	2278	Pressured
Node	2279	Pressured
Node	2280	Pressured
Node	2339	Pressured
Node	2339_1	Pressured
Node	2339_2	Pressured
Node	2339_3	Pressured
Node	2340	Pressured
Node	2340_1	Pressured
Node	2340_2	Pressured
Node	2340_3	Pressured
Node	2340_4	Pressured
Node	2340_5	Pressured
Node	430	Pressured
Node	67	Pressured
Node	902	Pressured
Node	902a	Pressured
Node	905	Pressured
Node	950	Pressured
Node	951	Pressured
Node	952	Pressured
Node	953	Pressured
Node	954	Pressured
Node	955	Pressured
Node	956	Pressured
Node	957	Pressured
Node	958	Pressured
Node	959	Pressured
Node	960	Pressured
Node	961	Pressured
Node	962	Pressured
Node	963	Pressured
Node	964	Pressured
Node	965	Pressured
Node	9914	Pressured
Node	9915	Pressured
Node	9916	Pressured
Node	DundasFM_1	Pressured
Node	DundasFM_2	Pressured
Node	DundasFM_3	Pressured
Node	EastFM_1	Pressured
Node	EastFM_2	Pressured
Node	Dundas_Street_Outfall	Overflow
Node	Dundas_Street_PS_Overflow_1	Overflow
Node	Front_St_PS_Overflow_1	Overflow
Node	WWTP	WWTP
Node	1049	FrontSt_PS
Node	1131	OverflowMHs
Node	158	OverflowMHs
Node	161	OverflowMHs
Node	162	OverflowMHs
Node	163	OverflowMHs
Node	164	OverflowMHs
Node	165	OverflowMHs
Node	166	OverflowMHs
Node	167	OverflowMHs
Node	168	OverflowMHs
Node	169	OverflowMHs
Node	170	OverflowMHs
Node	1705	OverflowMHs
Node	171	OverflowMHs
Node	1718	OverflowMHs
Node	1719	OverflowMHs
Node	172	OverflowMHs
Node	1720	OverflowMHs
Node	1721	OverflowMHs
Node	1725	OverflowMHs
Node	173	OverflowMHs
Node	174	OverflowMHs
Node	1742	OverflowMHs
Node	1743	OverflowMHs
Node	175	OverflowMHs
Node	1754	OverflowMHs
Node	1755	OverflowMHs
Node	1756	OverflowMHs
Node	1757	OverflowMHs
Node	1758	OverflowMHs
Node	1759	OverflowMHs
Node	1763	OverflowMHs
Node	1768	OverflowMHs
Node	1769	OverflowMHs
Node	1770	OverflowMHs
Node	1942	East_PS
Node	2061	OverflowMHs
Node	212	OverflowMHs
Node	2264	OverflowMHs
Node	516	OverflowMHs
Node	66	Dundas_Street_PS
Node	945	OverflowMHs
Node	946	OverflowMHs
Node	948	OverflowMHs
Link	1001	Front_Street_PS
Link	1009	Front_Street_PS
Link	1010	Front_Street_PS
Link	1011	Front_Street_PS
Link	1023	Front_Street_PS
Link	1025	Front_Street_PS
Link	1026	Front_Street_PS
Link	1027	Front_Street_PS
Link	1028	Front_Street_PS
Link	1029	Front_Street_PS
Link	103	Dundas_Street_PS
Link	1030	Front_Street_PS
Link	1032	Front_Street_PS
Link	1033	Front_Street_PS
Link	104	Dundas_Street_PS
Link	1045	Front_Street_PS
Link	1046	Front_Street_PS
Link	1048	Front_Street_PS
Link	1050	Pressure_Sewer
Link	1052	Front_Street_PS
Link	1054_1	Pressure_Sewer
Link	1054_2	Pressure_Sewer
Link	109	Dundas_Street_PS
Link	1090	East_PS
Link	1091	East_PS
Link	1092	East_PS
Link	1093	East_PS
Link	1096	East_PS
Link	1103	East_PS
Link	1116	East_PS
Link	1117	East_PS
Link	1118	East_PS
Link	1119	East_PS
Link	1120	East_PS
Link	1179	Pressure_Sewer
Link	1180	Pressure_Sewer
Link	1181	Pressure_Sewer
Link	1182	Pressure_Sewer
Link	1183	Pressure_Sewer
Link	1184	Pressure_Sewer
Link	1185	Pressure_Sewer
Link	1186	Pressure_Sewer
Link	1189	Moira_Sewer
Link	1190	Moira_Sewer
Link	1193	Moira_Sewer
Link	1194	Moira_Sewer
Link	1195	Moira_Sewer
Link	1196	Moira_Sewer
Link	1198	Moira_Sewer
Link	1199	Moira_Sewer
Link	1202	Moira_Sewer
Link	1203	Moira_Sewer
Link	1206	Moira_Sewer
Link	1207	Moira_Sewer
Link	1208	Moira_Sewer
Link	1209	Moira_Sewer
Link	1210	Moira_Sewer
Link	1212	Moira_Sewer
Link	1213	Moira_Sewer
Link	1214	Moira_Sewer
Link	1215	Moira_Sewer
Link	1216	Moira_Sewer
Link	1220	Moira_Sewer
Link	1221	Moira_Sewer
Link	1222	Moira_Sewer
Link	1223	Moira_Sewer
Link	1224	Moira_Sewer
Link	1225	Moira_Sewer
Link	1226	Moira_Sewer
Link	1245	Moira_Sewer
Link	1246	Moira_Sewer
Link	1247	Moira_Sewer
Link	1248	Moira_Sewer
Link	1249	Moira_Sewer
Link	1250	Moira_Sewer
Link	1251	Moira_Sewer
Link	1252	Moira_Sewer
Link	1255	Moira_Sewer
Link	1256	Moira_Sewer
Link	1290	Moira_Sewer
Link	1291	Moira_Sewer
Link	1292	Moira_Sewer
Link	1293	Moira_Sewer
Link	1294	Moira_Sewer
Link	1295	Moira_Sewer
Link	1296	Moira_Sewer
Link	1297	Moira_Sewer
Link	1298	Moira_Sewer
Link	1299	Moira_Sewer
Link	1300	Moira_Sewer
Link	1301	Moira_Sewer
Link	1302	Moira_Sewer
Link	1303	Moira_Sewer
Link	1308	Moira_Sewer
Link	1311	Moira_Sewer
Link	1312	Moira_Sewer
Link	1313	Moira_Sewer
Link	1314	Moira_Sewer
Link	1315	Moira_Sewer
Link	1316	Moira_Sewer
Link	132	Dundas_Street_PS
Link	133	Dundas_Street_PS
Link	134	Dundas_Street_PS
Link	1348	Front_Street_PS
Link	1349	Front_Street_PS
Link	1350	Front_Street_PS
Link	1351	Front_Street_PS
Link	154	Front_Street_PS
Link	155	Model_Bypass
Link	156	Front_Street_PS
Link	158	Model_Bypass
Link	159	Model_Bypass
Link	160	Model_Bypass
Link	161	Model_Bypass
Link	162	Model_Bypass
Link	163	Model_Bypass
Link	164	Model_Bypass
Link	165	Model_Bypass
Link	166	Model_Bypass
Link	167	Model_Bypass
Link	168	Model_Bypass
Link	169	Model_Bypass
Link	170	Model_Bypass
Link	1703	Model_Bypass
Link	171	Model_Bypass
Link	1716	Model_Bypass

```
Link 1717 Model_Bypass
Link 1718 Model_Bypass
Link 1719 Model_Bypass
Link 172 Model_Bypass
Link 1742 Model_Bypass
Link 1743 Model_Bypass
Link 1745 Model_Bypass
Link 1746 Model_Bypass
Link 1747 East_PS
Link 1748 East_PS
Link 1749 East_PS
Link 1750 East_PS
Link 1751 East_PS
Link 1752 East_PS
Link 1755 Model_Bypass
Link 1756 Model_Bypass
Link 1757 Model_Bypass
Link 1759 Model_Bypass
Link 1760 Model_Bypass
Link 1761 Model_Bypass
Link 1766 Model_Bypass
Link 1772 Model_Bypass
Link 1773 Model_Bypass
Link 1774 Model_Bypass
Link 1775 Model_Bypass
Link 1776 East_PS
Link 1777 East_PS
Link 1778 East_PS
Link 1779 East_PS
Link 1802 East_PS
Link 1803 East_PS
Link 1804 East_PS
Link 1805 East_PS
Link 1806 East_PS
Link 1807 East_PS
Link 1808 East_PS
Link 1809 East_PS
Link 1821 East_PS
Link 1877 East_PS
Link 1878 East_PS
Link 1879 East_PS
Link 1880 East_PS
Link 1881 East_PS
Link 1882 East_PS
Link 1883 East_PS
Link 1884 East_PS
Link 1885 East_PS
Link 1886 East_PS
Link 1887 East_PS
Link 1888 East_PS
Link 1891 East_PS
Link 1893 East_PS
Link 1905 East_PS
Link 1912 East_PS
Link 1925 East_PS
Link 1926 East_PS
Link 1927 East_PS
Link 1929 East_PS
Link 1931 East_PS
Link 1933 East_PS
Link 1934 East_PS
Link 1935 Front_Street_PS
Link 1946 Front_Street_PS
Link 1947 Front_Street_PS
Link 1948 Front_Street_PS
Link 1949 East_PS
Link 1950 East_PS
Link 1951 East_PS
Link 1956 East_PS
Link 1957 East_PS
Link 1958 East_PS
Link 1959 East_PS
Link 1960 East_PS
Link 1977 East_PS
Link 1978 East_PS
Link 1979 East_PS
Link 1980 East_PS
Link 2015 East_PS
Link 2016 East_PS
Link 2017 East_PS
Link 2018 East_PS
Link 2019 East_PS
Link 2020 East_PS
Link 2021 East_PS
Link 2029 East_PS
Link 2048 Model_Bypass
Link 2049 Front_Street_PS
Link 2056 Front_Street_PS
Link 208 Model_Bypass
Link 2082 Front_Street_PS
Link 2083 Front_Street_PS
Link 2084 Front_Street_PS
Link 2085 Front_Street_PS
Link 2086 Front_Street_PS
Link 2087 Front_Street_PS
Link 209 Model_Bypass
Link 2099 Front_Street_PS
Link 210 Front_Street_PS
Link 2135 Dundas_Street_PS
Link 2135_1 Dundas_Street_PS
Link 2135_2 Dundas_Street_PS
Link 2135_3 Dundas_Street_PS
Link 2135_4 Dundas_Street_PS
Link 2136 Front_Street_PS
Link 2137 Front_Street_PS
Link 2138 Front_Street_PS
Link 2140 Pressure_Sewer
Link 2144 Moira_Sewer
Link 2145 Moira_Sewer
Link 2146 Moira_Sewer
Link 2147 Pressure_Sewer
Link 2149 Pressure_Sewer
Link 2152 Front_Street_PS
Link 2153 Front_Street_PS
Link 216 Front_Street_PS
Link 2175 East_PS
Link 2176 East_PS
Link 2177 East_PS
Link 2178 East_PS
Link 2179 East_PS
Link 2180 East_PS
Link 2181 East_PS
Link 219 Front_Street_PS
Link 2219 Front_Street_PS
Link 2220 Front_Street_PS
Link 2221 Front_Street_PS
Link 2222 Front_Street_PS
Link 2223 Front_Street_PS
Link 2224 Front_Street_PS
Link 2225 Front_Street_PS
Link 2226 Front_Street_PS
Link 2264 Front_Street_PS
Link 2269 Model_Bypass
Link 2270 Moira_Sewer
Link 2271 Moira_Sewer
Link 2272 Moira_Sewer
Link 2273 Model_Bypass
Link 2274 Moira_Sewer
Link 2277 Moira_Sewer
Link 2278 Moira_Sewer
Link 2279 Pressure_Sewer
Link 2280 Pressure_Sewer
Link 2281 Pressure_Sewer
Link 2282 Pressure_Sewer
Link 2283 Pressure_Sewer
Link 2284 Moira_Sewer
Link 2285 Moira_Sewer
Link 2286 Moira_Sewer
Link 2287 Pressure_Sewer
Link 2288 Pressure_Sewer
Link 2289 Pressure_Sewer
Link 229 Front_Street_PS
Link 2291 Front_Street_PS
Link 2292 Front_Street_PS
Link 2339 East_PS
Link 2340 East_PS
Link 235 Front_Street_PS
Link 2390_1 Pressure_Sewer
Link 2390_2 Pressure_Sewer
Link 2390_3 Pressure_Sewer
Link 2390_5 Pressure_Sewer
Link 273 Front_Street_PS
Link 274 Front_Street_PS
Link 275 Front_Street_PS
Link 276 Front_Street_PS
Link 277 Front_Street_PS
Link 278 Front_Street_PS
Link 283 Front_Street_PS
Link 289 Front_Street_PS
Link 290 Front_Street_PS
Link 291 Front_Street_PS
Link 292 Front_Street_PS
Link 3300 Moira_Sewer
Link 3301 Moira_Sewer
Link 3302 Moira_Sewer
Link 3303 Moira_Sewer
Link 3304 Moira_Sewer
Link 3305 Moira_Sewer
Link 3306 Moira_Sewer
Link 3307 Moira_Sewer
Link 3309 Moira_Sewer
Link 3310 Moira_Sewer
Link 3311 Moira_Sewer
Link 3312 Moira_Sewer
Link 3313 Moira_Sewer
Link 3314 Moira_Sewer
Link 3315 Moira_Sewer
Link 3317 Moira_Sewer
Link 3318 Moira_Sewer
Link 3319 Moira_Sewer
Link 3320 Moira_Sewer
Link 3321 Moira_Sewer
Link 3339_10 Pressure_Sewer
Link 3339_11 Pressure_Sewer
Link 3339_12 Pressure_Sewer
Link 3339_2 Pressure_Sewer
Link 3339_3 Pressure_Sewer
Link 3339_5 Pressure_Sewer
Link 3339_6 Pressure_Sewer
Link 3339_8 Pressure_Sewer
Link 3339_9 Pressure_Sewer
Link 3340 Moira_Sewer
Link 3341 Moira_Sewer
Link 3342 Moira_Sewer
Link 3343 Moira_Sewer
Link 3344 Moira_Sewer
Link 3345 Moira_Sewer
Link 3346 Moira_Sewer
Link 3347 Moira_Sewer
Link 3348 Moira_Sewer
Link 3364 Front_Street_PS
Link 3365 Front_Street_PS
Link 3366 Front_Street_PS
Link 3367 Front_Street_PS
Link 3368 Front_Street_PS
Link 3369 Front_Street_PS
Link 3370 Front_Street_PS
Link 3371 Front_Street_PS
Link 3372 Front_Street_PS
Link 3373 Front_Street_PS
Link 3374 Front_Street_PS
Link 3375 Front_Street_PS
```

```
Link       3376           Front_Street_PS
Link       3377           Front_Street_PS
Link       3378           Front_Street_PS
Link       3379           Front_Street_PS
Link       3380           Front_Street_PS
Link       3381           Front_Street_PS
Link       3382           Front_Street_PS
Link       3383           Front_Street_PS
Link       3384           Front_Street_PS
Link       3385           Front_Street_PS
Link       3386           Front_Street_PS
Link       3387           Front_Street_PS
Link       3388           Front_Street_PS
Link       3389           Front_Street_PS
Link       3390           Front_Street_PS
Link       3391           Front_Street_PS
Link       3392           Front_Street_PS
Link       3393           Front_Street_PS
Link       3394           Front_Street_PS
Link       3395           Front_Street_PS
Link       3396           Front_Street_PS
Link       3398           Front_Street_PS
Link       3399           Front_Street_PS
Link       3400           Front_Street_PS
Link       3401           Front_Street_PS
Link       3402           Front_Street_PS
Link       3403           Front_Street_PS
Link       3500           Moira_Sewer
Link       3502           Front_Street_PS
Link       3503           Front_Street_PS
Link       3504           Front_Street_PS
Link       3505           Front_Street_PS
Link       3690           Front_Street_PS
Link       39             Dundas_Street_PS
Link       391            Front_Street_PS
Link       392            Front_Street_PS
Link       393            Front_Street_PS
Link       394            Front_Street_PS
Link       395            Front_Street_PS
Link       396            Front_Street_PS
Link       400            Front_Street_PS
Link       401            Front_Street_PS
Link       403            Front_Street_PS
Link       4035           East_PS
Link       4036           East_PS
Link       4037           East_PS
Link       4038           East_PS
Link       408            Front_Street_PS
Link       412            Front_Street_PS
Link       413            Front_Street_PS
Link       414            Front_Street_PS
Link       415            Front_Street_PS
Link       417            Front_Street_PS
Link       418            Front_Street_PS
Link       419            Front_Street_PS
Link       420            Front_Street_PS
Link       421            Front_Street_PS
Link       422            Front_Street_PS
Link       423            Front_Street_PS
Link       424            Front_Street_PS
Link       425            Front_Street_PS
Link       426            Front_Street_PS
Link       427            Front_Street_PS
Link       428            Front_Street_PS
Link       429            Front_Street_PS
Link       436            Front_Street_PS
Link       437            Front_Street_PS
Link       438            Front_Street_PS
Link       439            Front_Street_PS
Link       442            Front_Street_PS
Link       443            Front_Street_PS
Link       444            Front_Street_PS
Link       445            Front_Street_PS
Link       446            Front_Street_PS
Link       447            Front_Street_PS
Link       448            Front_Street_PS
Link       449            Front_Street_PS
Link       45             Dundas_Street_PS
Link       450            Front_Street_PS
Link       451            Front_Street_PS
Link       452            Front_Street_PS
Link       453            Front_Street_PS
Link       454            Front_Street_PS
Link       455            Front_Street_PS
Link       456            Front_Street_PS
Link       457            Front_Street_PS
Link       458            Front_Street_PS
Link       459            Front_Street_PS
Link       460            Front_Street_PS
Link       461            Front_Street_PS
Link       465            Front_Street_PS
Link       468            Front_Street_PS
Link       469            Front_Street_PS
Link       474            Front_Street_PS
Link       475            Front_Street_PS
Link       476            Front_Street_PS
Link       477            Front_Street_PS
Link       478            Front_Street_PS
Link       499            Front_Street_PS
Link       500            Front_Street_PS
Link       502            Front_Street_PS
Link       505            Front_Street_PS
Link       5050           Front_Street_PS
Link       506            Front_Street_PS
Link       507            Front_Street_PS
Link       51             Dundas_Street_PS
Link       510            Front_Street_PS
Link       511            Front_Street_PS
Link       512            Front_Street_PS
Link       513            Front_Street_PS
Link       515            Model_Bypass
Link       520            Front_Street_PS
Link       53_1           Dundas_Street_PS
Link       53_2           Dundas_Street_PS
Link       551            Front_Street_PS
Link       552            Front_Street_PS
Link       558            Front_Street_PS
Link       560            Front_Street_PS
Link       60             Dundas_Street_PS
Link       61             Dundas_Street_PS
Link       62             Dundas_Street_PS
Link       63             Dundas_Street_PS
Link       63_1           Dundas_Street_PS
Link       64             Dundas_Street_PS
Link       646            Front_Street_PS
Link       647            Front_Street_PS
Link       649            Front_Street_PS
Link       650            Front_Street_PS
Link       651            Front_Street_PS
Link       663            Front_Street_PS
Link       664            Front_Street_PS
Link       665            Front_Street_PS
Link       666            Front_Street_PS
Link       667            Front_Street_PS
Link       668            Front_Street_PS
Link       669            Front_Street_PS
Link       670            Front_Street_PS
Link       672            Front_Street_PS
Link       673            Front_Street_PS
Link       675            Front_Street_PS
Link       680            Front_Street_PS
Link       681            Front_Street_PS
Link       682            Front_Street_PS
Link       683            Front_Street_PS
Link       684            Front_Street_PS
Link       688            Front_Street_PS
Link       689            Front_Street_PS
Link       779            Front_Street_PS
Link       780            Front_Street_PS
Link       781            Front_Street_PS
Link       782            Front_Street_PS
Link       854            Front_Street_PS
Link       855            Front_Street_PS
Link       860            Front_Street_PS
Link       861            Front_Street_PS
Link       862            Front_Street_PS
Link       866            Front_Street_PS
Link       867            Front_Street_PS
Link       868            Front_Street_PS
Link       880            Front_Street_PS
Link       881            Front_Street_PS
Link       882            Front_Street_PS
Link       883            Front_Street_PS
Link       884            Front_Street_PS
Link       885            Front_Street_PS
Link       886            Front_Street_PS
Link       887            Front_Street_PS
Link       888            Front_Street_PS
Link       889            Front_Street_PS
Link       890            Front_Street_PS
Link       891            Front_Street_PS
Link       892            Front_Street_PS
Link       9011           Pressure_Sewer
Link       9012           Pressure_Sewer
Link       9014           East_PS
Link       9015           East_PS
Link       9016           East_PS
Link       9017           East_PS
Link       9018           East_PS
Link       9019           East_PS
Link       9020           East_PS
Link       9021           East_PS
Link       9022           East_PS
Link       9023           East_PS
Link       9024           East_PS
Link       9025           East_PS
Link       9026           East_PS
Link       9027           Pressure_Sewer
Link       9028           Front_Street_PS
Link       9029           Front_Street_PS
Link       932            Moira_Sewer
Link       946            Front_Street_PS
Link       947            Front_Street_PS
Link       948            Front_Street_PS
Link       949            Front_Street_PS
Link       952            Model_Bypass
Link       953            Model_Bypass
Link       955            Model_Bypass
Link       957            Pressure_Sewer
Link       958            Pressure_Sewer
Link       959            Pressure_Sewer
Link       960            Pressure_Sewer
Link       961            Pressure_Sewer
Link       962            Pressure_Sewer
Link       963            Pressure_Sewer
Link       964_1          Pressure_Sewer
Link       964_2          Pressure_Sewer
Link       965            Pressure_Sewer
Link       966            Pressure_Sewer
Link       967            Pressure_Sewer
Link       968            Pressure_Sewer
Link       969            Pressure_Sewer
Link       970            Pressure_Sewer
Link       971            Pressure_Sewer
Link       988            Front_Street_PS
Link       989            Front_Street_PS
Link       990            Front_Street_PS
Link       990_1          Front_Street_PS
Link       9902           East_PS
Link       9904           Pressure_Sewer
Link       9905           Pressure_Sewer
Link       9906_1         Pressure_Sewer
```

```
Link       9906_2          Pressure_Sewer
Link       9907            Pressure_Sewer
Link       9908            Dundas_Street_PS
Link       9909            Pressure_Sewer
Link       9910            Pressure_Sewer
Link       9911            Front_Street_PS
Link       9912            Front_Street_PS
Link       9914            Pressure_Sewer
Link       9915            Pressure_Sewer
Link       9916            Pressure_Sewer
Link       992_1           Front_Street_PS
Link       992_2           Front_Street_PS
Link       998             Front_Street_PS
Link       999             Front_Street_PS
Link       Dundas_1        Dundas_Street_PS
Link       Dundas_2        Dundas_Street_PS
Link       Dundas_3        Dundas_Street_PS
Link       2282_c          Front_Street_PS
Link       3339_1          Pressure_Sewer
Link       3339_4          Pressure_Sewer

[MAP]
DIMENSIONS       304490.7517      4890447.5129     313360.0583      4897808.2971
UNITS            Meters

[COORDINATES]
;;Node           X-Coord            Y-Coord
;;-------------- ------------------ ------------------
1048             309467.55          4892467.053
1050             309485.335         4892459.902
1050_1           309486.195         4892460.393
1050_2           309486.267         4892459.677
1175             309779.196         4894590.102
1176             309754.985         4894572.424
1177             309714.07          4894504.084
1178             309677.039         4894415.386
1179             309654.546         4894354.28
1180             309617.27          4894252.824
1181             309552.622         4894205.983
1182             309526.851         4894124.484
2151             309980.396         4891980.206
2152             309814.993         4891940.446
2271             308951.009         4893286.715
2272             309043.949         4893261.142
2273             308932.896         4892922.68
2275             309062.861         4892961.389
2276             309096.555         4892864.316
2277             309179.187         4892894.601
2278             309220.837         4892854.111
2279             309090.56          4893272.271
2280             309146.75          4893269.542
2339             308786.017         4896626.302
2339_1           308771.046         4896634.311
2339_2           308774.239         4896620.698
2339_3           308787.885         4896608.117
2340             308644.453         4896558.948
2340_1           308649.429         4896577.245
2340_2           308661.591         4896549.18
2340_3           308665.664         4896584.863
2340_4           308671.405         4896571.771
2340_5           308677.721         4896556.707
430              309197.068         4892845.916
67               307944.676         4891260.89
902              309528.602         4892440.506
902a             309491.095         4892459.873
905              309828.944         4892239.413
950              309505.093         4894017.642
951              309478.638         4893875.802
952              309459.041         4893795.689
953              309412.38          4893647.237
954              309350.714         4893591.079
955              309276.612         4893541.179
956              309210.267         4893404.273
957              309154.156         4893303.047
958              309138.12          4893230.504
959              309170.433         4893123.525
960              309221.705         4892970.41
961              309260.175         4892867.653
962              309284.636         4892833.736
963              309348.54          4892696.523
964              309387.533         4892611.925
965              309451.125         4892471.348
9914             309475.22          4892466.914
9915             310351.368         4892229.233
9916             310352.466         4892225.769
DundasFM_1       308452.598         4891644.952
DundasFM_2       308460.223         4891652.036
DundasFM_3       308469.142         4891657.431
EastFM_1         310354.006         4892229.977
EastFM_2         310355.319         4892226.843
Dundas_Street_Outfall 309333.538         4892449.656
Dundas_Street_PS_Overflow_1 307948.965         4891219.17
Front_St_PS_Overflow_1 309447.331         4892470.22
WWTP             310229.373         4892170.176
1005             309508.118         4892846.634
1007             309460.715         4892833.472
1008             309381.943         4892808.928
1020             309409.907         4892721.985
1022             309411.046         4892717.957
1023             309433.024         4892637.521
1024             309464.62          4892544.444
1025             309459.926         4892487.428
1026             309464.501         4892478.621
1029             309604.259         4892528.903
1030             309601.62          4892528.251
1031             309508.375         4892501.681
1042             309723.759         4892565.915
1044             309944.966         4892612.885
1045             309845.177         4892598.041
1049             309476.638         4892458.198
1051             310223.394         4892183.883
106              308021.667         4891306.692
107              308075.777         4891340.6
1085             312901.515         4893508.243
1090             312833.849         4893735.188
1091             312852.627         4893669.63
1092             312881.961         4893574.434
1093             312807.339         4893822.344
1096             312784.231         4893906.339
1101             312761.429         4893982.515
1111             312714.766         4894140.471
1114             312719.404         4894121.408
1115             312724.53          4894101.961
1116             312758.325         4893991.199
1117             312702.099         4894180.75
112              308142.736         4891382.52
1131             312607.536         4893670.677
1185             310171.949         4894659.679
1186             310163.322         4894649.837
1187             310041.149         4894620.452
1190             309921.103         4894568.33
1191             309808.107         4894543.737
1192             310558.735         4894927.049
1193             310498.574         4894852.893
1195             310447.042         4894796.416
1196             310404.438         4894746.919
1199             310288.67          4894698.27
1202             310655.143         4895047.723
1203             310700.179         4895108.766
1204             310771.001         4895208.002
1205             310856.295         4895312.119
1206             310955.566         4895352.527
1208             311481.737         4895515.533
1209             311398.909         4895489.12
1210             311308.007         4895462.71
1211             311180.537         4895420.917
1212             311095.097         4895395.348
1216             311149.844         4895966.93
1217             311172.985         4895879.873
1218             311200.648         4895790.206
1219             311230.639         4895692.422
1220             311253.907         4895618.087
1221             311278.335         4895543.108
1222             311118.043         4896070.528
1241             310266.107         4896396.866
1242             310211.938         4896367.995
1243             310130.442         4896319.706
1244             310059.52          4896276.281
1245             309997.357         4896220.683
1246             309940.955         4896169.817
1247             309885.87          4896111.805
1248             309835.782         4896058.786
1249             309736.399         4896030.5
1252             309770.831         4895929.698
1253             309716.755         4895876.7
1286             309664.716         4895857.186
1287             309597.086         4895834.197
1288             309529.819         4895809.204
1289             309450.828         4895782.84
1290             309372.313         4895755.003
1291             309303.084         4895727.247
1292             309336.749         4895646.439
1293             309366.668         4895572.716
1294             309386.302         4895524.666
1295             309426.986         4895438.388
1296             309487.857         4895363.452
1297             309546.994         4895292.221
1298             309592.203         4895237.851
1299             309645.738         4895175.155
1303             309705.835         4895098.659
1306             309755.817         4895037.152
1307             309801.006         4894963.331
1308             309797.224         4894874.407
1309             309797.12          4894802.346
1310             309787.354         4894684.185
1344             309868.043         4894042.297
1345             309849.316         4894015.985
1346             309793.228         4893956.232
1347             309753.175         4893915.528
1348             309682.371         4893839.439
135              308230.961         4891444.604
1352             309623.694         4893776.029
136              308286.063         4891486.37
137              308392.688         4891578.613
138              308399.539         4891584.905
1511             310681.766         4893534.348
1514             310717.748         4893421.295
157              308470.615         4891653.972
158              308471.88          4891675.972
159              308481.983         4891649.669
1593             310785.143         4893214.981
161              308370.032         4892002.881
162              308393.87          4891914.258
163              308420.987         4891829.106
164              308446.774         4891751.486
165              308338.831         4892104.203
166              308313.395         4892187.714
167              308286.673         4892273.506
168              308255.618         4892367.763
169              308229.533         4892458.305
170              308217.809         4892501.486
1705             312582.477         4893752.249
171              308160.95          4892699.486
1718             312487.285         4894079.546
1719             312508.538         4894007.232
172              308157.177         4892691.867
1720             312534.094         4893920.81
1721             312557.956         4893843.018
1725             312513.573         4894164.027
173              308180.129         4892617.966
174              308211.243         4892515.399
1742             312465.783         4894149.639
```

1743	312600.262	4894192.476
1745	312906.66	4893489.93
1746	312935.454	4893394.578
1747	312956.908	4893298.572
1748	312953.748	4893281.093
1749	312807.25	4893292.929
175	308213.511	4892508.805
1750	312694.548	4893240.899
1754	312633.925	4893587.62
1755	312653.824	4893517.944
1756	312564.864	4893489.834
1757	312585.383	4893417.309
1758	312523.551	4893397.663
1759	312487.97	4893386.016
1763	312417.969	4893362.751
1768	312446.867	4893264.876
1769	312452.494	4893239.677
1770	312455.305	4893227.75
1771	312478.04	4893145.614
1772	312614.436	4893205.476
1773	312546.238	4893175.545
1774	312450.102	4893134.49
1794	312490.233	4893001.774
1795	312353.267	4892965.612
1796	312287.113	4892946.643
1797	312193.84	4892920.935
1798	312110.838	4892899.21
1799	312035.506	4892879.684
1800	311921.958	4892852.312
1801	311835.41	4892814.007
1812	311756.497	4892760.118
1866	311652.695	4892716.83
1867	311563.842	4892679.965
1868	311505.266	4892661.884
1869	311408.683	4892634.66
1870	311320.987	4892609.108
1871	311233.233	4892585.05
1872	311128.321	4892555.223
1873	311024.776	4892525.532
1874	310953.321	4892463.54
1875	310892.913	4892453.481
1876	310817.355	4892384.086
1877	310824.474	4893103.432
1880	310849.497	4893027.614
1881	310904.187	4892873.212
1898	310647.347	4892706.932
1899	310642.635	4892703.262
1913	310597.633	4892693.104
1914	310590.428	4892695.07
1915	310509.453	4892678.832
1916	310420.953	4892663.258
1917	310306.478	4892646.192
1918	310286.366	4892643.745
1919	310279.393	4892628.258
1920	310220.949	4892638.739
1923	310147	4892629.315
1927	310045.799	4892619.965
1931	310308.795	4892540.194
1932	310330.457	4892470.18
1933	310365.407	4892364.476
1938	310579.226	4892262.888
1939	310734.253	4892322.905
1940	310656.743	4892289.266
1941	310531.013	4892250.101
1942	310374.57	4892238.453
1943	310283.034	4892644.14
1968	310754.982	4893307.44
1969	310725.657	4893396.27
1970	310709.998	4893443.532
2029	312508.653	4894607.415
2030	312430.095	4894618.357
2031	312341.997	4894603.206
2032	312570.237	4894599.559
2033	312263.439	4894584.689
2034	312140.178	4894556.258
2035	312090.976	4894546.813
2036	311991.002	4894565.704
2061	308372.255	4891987.87
2062	308888.687	4892909.071
2063	308886.656	4892905.759
2096	309498.395	4893648.927
2097	309559.461	4893710.865
2105	308086.768	4895044.013
211	308343.765	4892751.506
212	308251.743	4892722.89
213	308433.403	4892776.062
2140	307124.318	4890919.077
2140_1	307018.698	4890872.229
2140_2	306931.079	4890835.282
2140_3	306834.499	4890800.583
2140_4	306777.639	4890782.094
2141	309309.626	4892461.522
2146	311517.586	4895515.043
2147	311630.467	4895557.374
2148	311740.846	4895586.888
2154	308717.404	4891886.837
2155	308779.638	4891985.363
216	308495.584	4892793.536
2176	312684.979	4894218.882
2177	312660.264	4894300.251
2178	312636.057	4894369.955
2179	312608.58	4894469.273
2180	312600.597	4894487.586
2217	308385.162	4895047.494
2218	308402.315	4894990.297
2219	308421.508	4894906.976
222	308588.723	4892820.732
2220	308386.854	4894642.944
2221	308388.277	4894717.87
2222	308449.414	4894429.358
2223	308466.213	4894379.228
2224	308504.916	4894252.48
2259	308283.346	4895104.32
2264	309344.376	4894134.146
2265	309336.765	4894132.654
2266	309505.606	4894118.88
2267	309515.826	4894129.099
2268	309319.405	4894195.257
2269	308701.644	4893280.332
2270	308822.463	4893276.092
2282	309310.468	4892454.505
2282_1	309311.669	4892454.597
2282_2	309310.767	4892453.259
2286	310935.252	4892784.425
2300	309285.645	4895738.397
2301	309217.169	4895888.298
2302	309219.132	4895908.332
2303	309176.247	4895982.992
2304	309170.912	4895992.151
2305	309111.441	4896084.808
2306	309034.445	4896188.309
2307	308951.132	4896266.708
2309	308892.309	4896417.973
231	308685.283	4892844.03
2310	308828.615	4896498.28
2311	308816.187	4896557.184
2312	308822.519	4896635.729
2313	308831.716	4896742.032
2314	308840.668	4896846.649
2315	308849.151	4896951.808
2317	308857.094	4897060.418
2318	308864.537	4897162.246
2319	308872.854	4897265.712
2320	308881.926	4897369.115
2321	308891.074	4897473.716
2341	308519.545	4896522.205
2342	308400.69	4896483.495
2343	308305.174	4896453.55
2344	308237.14	4896430.602
2345	308183.2	4896412.178
2346	308106.501	4896389.433
2347	307983.133	4896349.404
2348	307879.106	4896313.648
2349	307861.234	4896307.816
236	308775.213	4892872.907
2363	307376.93	4894977.448
2364	307355.158	4894976.341
2365	307250.587	4894917.478
2366	307143.643	4894863.044
2367	307019.503	4894798.319
2368	307005.03	4894784.516
2369	306956.446	4894759.602
2370	306851.885	4894706.659
2371	306842.009	4894715.266
2372	306734.741	4894661.473
2373	306627.645	4894607.34
2374	306521.329	4894551.691
2375	306414.71	4894496.624
2376	306307.856	4894442.014
2377	306201.089	4894387.235
2378	306094.264	4894332.569
2379	305982.514	4894275.232
2380	305974.728	4894280.527
2381	305936.774	4894407.684
2382	305845.426	4894377.836
2383	305753.029	4894351.419
2384	305722.986	4894451.09
2385	305691.23	4894550.228
2386	305582.419	4894510.717
2387	305465.684	4894482.912
2388	305349.29	4894453.716
2389	305232.715	4894425.252
2390	305116.578	4894395.05
2391	304978.114	4894353.721
2392	304969.035	4894381.052
2393	304939.983	4894472.97
2394	304916.208	4894549.356
2395	304893.902	4894623.054
2397	305799.283	4894606.872
2398	305904.095	4894665.306
2399	306009.275	4894723.072
2400	306113.796	4894782.026
2401	306218.708	4894840.278
2402	306324.029	4894897.79
2453	308412.83	4894855.192
2474	309103.693	4892710.744
2475	309130.967	4892609.824
2476	309158.636	4892506.414
2477	309231.036	4892525.853
284	308507.068	4891569.18
285	308511.91	4891554.602
286	308577.019	4891649.442
287	308638.713	4891738.292
288	308722.677	4891873.556
289	308785.646	4891979.673
290	308862.697	4892098.723
300	308294.061	4892920.322
3000	309256.715	4893229.905
3000A	309258.372	4893221.592
301	308319.157	4892833.638
302	308260.037	4893034.006
303	308274.368	4892982.892
360	308692.153	4893286.288
401	308913.464	4892191.556
402	308934.212	4892233.975
403	309011.941	4892323.254
404	309085.745	4892390.372
405	309131.514	4892409.153
406	309172.46	4892419
409	309125.022	4892589.476
411	309153.466	4892497.152
413	309233.673	4892517.313

```
414              309251.82          4892454.025
418              309060.182         4892711.5
419              309138.576         4892724.873
421              309098.682         4892702.14
424              309226.322         4892755.871
425              309268.495         4892626.178
426              309303.785         4892510.102
427              309303.08          4892465.873
428              309143.96          4892989.483
429              309177.576         4892891.574
431              309141.404         4892741.699
432              309099.837         4892862.39
433              309065.128         4892960.055
434              309063.98          4892964.47
435              308840.043         4892891.855
436              308937.071         4892920.805
437              308987.223         4892937.07
438              308992.157         4892938.87
439              309026.416         4892833.844
44               307220.783         4890959.254
446              308788.591         4893081.003
447              308831.478         4893095.736
448              308925.61          4893126.346
449              308955.548         4893025.938
45               307282.859         4890984.29
451              309002.124         4893150.958
452              309054.387         4892994.212
453              309077.167         4893175.842
454              309113.789         4893075.511
455              308783.947         4893269.851
456              308807.879         4893178.854
457              308815.537         4893274.462
458              308869.324         4893279.211
459              308882.946         4893281.338
460              308916.66          4893151.354
461              308934.618         4893287.26
462              308957.061         4893288.917
463              308960.288         4893274.016
464              308980.165         4893216.549
465              309036.027         4893296.248
468              308760.306         4893450.483
469              308756.248         4893464.632
473              308787.862         4893363.805
477              308705.908         4893621.342
478              308735.258         4893525.27
479              308627.772         4893865.562
480              308651.627         4893794.936
481              308663.915         4893755.224
501              309126.471         4893424.299
502              309102.896         4893392.887
503              309031.906         4893309.427
506              309173.222         4893480.61
507              309292.816         4893637.003
508              309224.164         4893547.141
51               307394.758         4891025.463
511              309448.294         4893863.359
512              309368.712         4893743.871
513              309337.619         4893806.982
514              309310.285         4893844.76
516              309417.326         4893883.218
521              309303.155         4893841.842
54               307515.073         4891068.605
55_1             307588.634         4891097.126
553              307414.962         4894858.679
554              307507.073         4894876.332
555              307588.561         4894894.598
556              307672.725         4894920.553
56               307665.954         4891129.707
563              307489.959         4894885.037
63               307742.853         4891160.923
64               307847.512         4891215.672
649              307771.085         4894948.993
65               307931.548         4891260.072
65_1             307934.444         4891254.567
650              307866.613         4894980.766
652              307959.343         4895007.363
653              307980.91          4895013.342
654              308056.482         4895035.612
66               307936.087         4891251.192
666              308013.527         4895441.525
667              307931.628         4895417.152
668              307835.294         4895390.418
669              307746.588         4895364.981
670              307776.372         4895270.411
671              307808.041         4895169.27
672              307836.768         4895075.285
673              308154.243         4895068.54
675              308183.627         4895076.876
676              308254.214         4895095.664
678              308359.489         4895126.945
68               307965.956         4891273.194
682              308474.559         4895185.28
684              308417.547         4895154.71
685              308382.497         4895056.577
686              308402.845         4894981.828
689              308417.319         4894932.609
690              308405.452         4894811.169
708              308594.386         4895222.011
780              308396.644         4894749.136
781              308389.831         4894611.937
782              308419.126         4894521.596
783              308441.453         4894458.692
796              307790.058         4893958.407
852              307850.042         4893974.047
853              307915.613         4893989.865
859              308035.671         4894022.578
860              307975.222         4894006.569
861              307992.725         4894011.538
864              308155.641         4894057.957
865              308105.529         4894042.235
866              308163.643         4894059.928
877              308253.786         4894086.617
878              308194.557         4894068.315
879              308314.071         4894103.334
880              308397.257         4894129.927
881              308465.979         4894149.77
882              308541.3           4894173.775
883              308476.81          4894344.243
884              308496.291         4894279.876
885              308522.022         4894198.148
886              308566.217         4894073.949
887              308591.447         4893975.048
9001             312787.556         4894589.555
9002             312748.583         4894579.712
9003             312716.436         4894573.576
9004             312671.977         4894578.708
9005             312646.601         4894593.332
9006             312632.996         4894614.453
9050             310946.759         4892752.81
9051             310956.014         4892749.053
9052             311012.716         4892770.867
9053             311068.456         4892792.637
9054             311077.957         4892782.518
9055             311089.829         4892746.492
9056             311108.199         4892691.968
9057             311098.273         4892674.008
9058             311080.156         4892644.448
9059             311060.573         4892611.81
9060             311024.044         4892550.526
9061             311022.182         4892541.121
924              309206.502         4894165.117
940              309258.305         4893995.688
941              309233.534         4894077.56
942              309277.898         4893928.533
945              309375.089         4894026.61
946              309394.482         4893962.636
948              309351.942         4894110.301
978              309414.823         4893571.057
984              309295.125         4893481.87
985              309262.941         4893433.14
986              309252.77          4893379.39
987              309254.939         4893279.375
988              309275.803         4893154.413
9902             309480.315         4892465.88
991              309289.129         4893109.262
996              309316.295         4893022.08
997              309343.171         4892938.889
999              309361.949         4892875.873

[VERTICES]
;;Link           X-Coord            Y-Coord
;;-------------- ------------------ ------------------
1054_1           309744.895         4892045.605
1054_1           309698.364         4892192.846
1054_1           309687.957         4892227.246
1054_1           309657.839         4892320.826
1054_1           309596.528         4892307.38
1054_1           309539.793         4892426.372
1054_1           309518.569         4892466.128
1210             310909.199         4895338.799
1210             310898.032         4895334.308
1210             310875.273         4895324.562
1315             309801.115         4894796.484
156              308474.877         4891653.074
161              308470.696         4891679.906
168              308160.749         4892696.711
172              308216.18          4892505.697
1742             312466.434         4894147.516
1757             312567.321         4893490.535
1772             312429.463         4893318.118
2021             312041.816         4894554.628
208              308171.314         4892702.254
2147             310101.292         4892072.495
2147             310093.014         4892070.121
2147             310104.449         4892004.09
2147             310002.663         4891983.415
216              308492.983         4892792.397
2179             312602.475         4894476.317
2180             312606.232         4894479.134
219              308557.615         4892811.679
2270             309345.031         4894132.081
2270             309504.909         4894116.673
2272             309508.863         4894130.841
2279             308948.54          4892927.694
2279             308960.975         4892926.29
2279             309002.692         4892940.731
2281             309196.41          4892849.363
2283             309229.692         4892856.768
2285             308715.72          4893277.349
2285             308741.757         4893274.659
2286             308891.887         4893280.407
2286             308885.792         4893286.013
2287             308957.603         4893287.358
2287             309031.341         4893294.556
2287             309036.456         4893287.797
2287             309037.704         4893283.874
2289             309096.842         4893273.413
2289             309142.532         4893271.985
2390_5           308355.79          4891554.889
2390_5           308243.024         4891463.455
2390_5           308069.775         4891345.435
2390_5           307946.217         4891270.531
283              308743.082         4891903.857
393              309001.437         4892310.724
418              309142.133         4892733.733
421              309064.647         4892962.033
427              308988.115         4892934.444
448              308747.401         4893270.582
457              308958.065         4893286.031
507              309168.635         4893474.935
510              309446.516         4893860.769
511              309364.913         4893738.726
```

```
558              307443.553         4894868.393
61               307790.14          4891183.727
64               307938.296         4891259.921
669              307863.652         4894990.417
854              307806.536         4893962.703
9011             310227.392         4892197.633
9012             310233.478         4892184.086
932              309210.152         4894166.444
988              309253.996         4893418.687
9904             309491.666         4892461.107
9904             309517.851         4892464.527
9904             309553.818         4892392.225
9904             309567.587         4892360.309
9904             309654.832         4892191.382
9905             309942.95          4892270.864
9905             310024.96          4892291.199
9905             310077.743         4892123.383
9905             310155.698         4892142.502
9905             310150.07          4892168.043
9905             310182.018         4892176.633
9905             310209.504         4892184.024
9906_1           309517.237         4892463.431
9906_2           309488.037         4892459.457
9907             309553.974         4892389.328
9907             309579.345         4892338.15
9907             309604.717         4892286.972
9907             309630.089         4892235.793
9907             309653.821         4892187.922
9907             309657.387         4892188.873
9907             309712.581         4892203.591
9907             309767.775         4892218.308
9907             309822.968         4892233.026
9907             309878.162         4892247.743
9907             309933.355         4892262.461
9907             309988.549         4892277.179
9907             310022.967         4892286.356
9907             310029.249         4892265.793
9907             310045.937         4892211.163
9907             310062.625         4892156.533
9907             310074.628         4892117.243
9907             310090.156         4892121.257
9907             310145.46          4892135.556
9907             310159.544         4892139.197
9907             310154.193         4892165.913
9907             310169.029         4892169.766
9908             307934.611         4891245.871
9914             308393.134         4891583.486
9914             308356.601         4891550.111
9914             308320.068         4891519.216
9914             308256.7           4891467.348
9914             308216.784         4891437.806
9914             308160.181         4891398.567
9914             308121.393         4891372.972
9914             308068.736         4891338.807
9914             308020.703         4891309.603
9914             307969.286         4891278.37
9914             307943.803         4891265.065
Dundas_1         307942.38          4891254.988
Dundas_2         307944.941         4891252.629
Dundas_3         307947.535         4891251.398
East_PS_1        310359.354         4892249.145
East_PS_2        310362.8           4892240.285
East_PS_3        310367.157         4892230.938
East_PS_4        310371.461         4892219.747
FrontSt#1        309483.928         4892457.624
FrontSt#2        309483.758         4892458.758
FrontSt#3        309483.418         4892459.666
FrontSt#4        309482.623         4892460.801

[POLYGONS]

;;Storage Node   X-Coord            Y-Coord
;;-------------- ------------------ ------------------

[SYMBOLS]
;;Gage           X-Coord            Y-Coord
;;-------------- ------------------ ------------------
```

```
EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)
------------------------------------------------------------

Existing Scenario Model Network. Model has been updated to account population up to 2023
WARNING 02: maximum depth increased for Node 1050_1

*************
Element Count
*************
Number of rain gages ...... 6
Number of subcatchments ... 0
Number of nodes ........... 574
Number of links ........... 600
Number of pollutants ...... 0
Number of land uses ....... 0


****************
Raingage Summary
****************
```

Name	Data Source	Data Type	Recording Interval
100yrSCS	100yrSCS	INTENSITY	15 min.
CHI_3hr_100yr	CHI_3hr_100yr	INTENSITY	10 min.
Intensity	Intensity	INTENSITY	5 min.
SCS_24hr_100yr	SCS_24hr_100yr	INTENSITY	15 min.
SCS_24hr_10yr	SCS_24hr_10yr	INTENSITY	15 min.
Zero_Rainfall	Zero_Rainfall	INTENSITY	10 min.

```
************
Node Summary
************
```

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
1048	JUNCTION	70.70	1.50	0.0	
1050	JUNCTION	69.50	6.66	0.0	
1050_1	JUNCTION	74.45	1.70	0.0	
1050_2	JUNCTION	74.45	0.68	0.0	
1175	JUNCTION	80.89	1.06	0.0	
1176	JUNCTION	80.68	1.08	0.0	Yes
1177	JUNCTION	80.53	1.10	0.0	
1178	JUNCTION	79.73	1.59	0.0	
1179	JUNCTION	79.49	1.05	0.0	
1180	JUNCTION	78.73	1.28	0.0	
1181	JUNCTION	78.39	1.16	0.0	
1182	JUNCTION	78.09	1.76	0.0	
2151	JUNCTION	71.56	1.50	0.0	Yes
2152	JUNCTION	71.39	1.50	0.0	Yes
2271	JUNCTION	79.28	0.40	0.0	
2272	JUNCTION	77.42	1.63	0.0	
2273	JUNCTION	78.79	1.70	0.0	
2275	JUNCTION	77.58	0.47	0.0	
2276	JUNCTION	77.36	0.55	0.0	
2277	JUNCTION	76.16	1.07	0.0	Yes
2278	JUNCTION	72.70	3.61	0.0	
2279	JUNCTION	77.12	0.41	0.0	
2280	JUNCTION	74.07	1.08	0.0	
2339	JUNCTION	92.39	0.81	0.0	
2339_1	JUNCTION	90.60	0.55	0.0	
2339_2	JUNCTION	90.60	0.35	0.0	
2339_3	JUNCTION	90.60	0.35	0.0	
2340	JUNCTION	93.51	1.11	0.0	
2340_1	JUNCTION	93.51	1.11	0.0	
2340_2	JUNCTION	93.52	1.11	0.0	
2340_3	JUNCTION	90.70	0.45	0.0	
2340_4	JUNCTION	90.70	0.25	0.0	
2340_5	JUNCTION	90.70	0.25	0.0	
430	JUNCTION	76.00	0.40	0.0	
67	JUNCTION	79.70	0.45	0.0	
902	JUNCTION	75.28	0.45	0.0	
902a	JUNCTION	75.29	0.45	0.0	
905	JUNCTION	75.45	0.61	0.0	
950	JUNCTION	77.69	1.14	0.0	
951	JUNCTION	76.83	1.05	0.0	
952	JUNCTION	76.34	1.21	0.0	
953	JUNCTION	75.80	1.20	0.0	
954	JUNCTION	75.50	1.18	0.0	
955	JUNCTION	75.04	1.19	0.0	
956	JUNCTION	74.49	1.10	0.0	
957	JUNCTION	74.14	1.14	0.0	
958	JUNCTION	73.79	1.18	0.0	
959	JUNCTION	73.41	1.15	0.0	
960	JUNCTION	72.84	1.21	0.0	
961	JUNCTION	72.45	1.18	0.0	
962	JUNCTION	71.75	1.68	0.0	
963	JUNCTION	71.31	1.05	0.0	
964	JUNCTION	71.15	1.05	0.0	
965	JUNCTION	70.73	1.07	0.0	
9914	JUNCTION	70.71	2.65	0.0	
9915	JUNCTION	74.50	2.63	0.0	
9916	JUNCTION	74.50	2.63	0.0	
DundasFM_1	JUNCTION	82.10	0.45	0.0	
DundasFM_2	JUNCTION	79.95	0.45	0.0	
DundasFM_3	JUNCTION	79.96	0.45	0.0	
EastFM_1	JUNCTION	76.63	0.45	0.0	
EastFM_2	JUNCTION	76.63	0.45	0.0	
Dundas_Street_Outfall	OUTFALL	72.50	0.91	0.0	
Dundas_Street_PS_Overflow_1	OUTFALL	77.00	0.45	0.0	
Front_St_PS_Overflow_1	OUTFALL	74.00	0.60	0.0	
WWTP	OUTFALL	73.42	1.00	0.0	
1005	STORAGE	76.82	6.22	0.0	Yes
1007	STORAGE	76.64	7.36	0.0	Yes
1008	STORAGE	76.40	7.86	0.0	Yes
1020	STORAGE	75.78	7.50	0.0	Yes
1022	STORAGE	75.73	7.47	0.0	Yes
1023	STORAGE	75.36	6.42	0.0	Yes
1024	STORAGE	74.84	7.34	0.0	Yes
1025	STORAGE	74.57	5.61	0.0	
1026	STORAGE	74.25	5.93	0.0	
1029	STORAGE	75.52	6.72	0.0	Yes
1030	STORAGE	75.43	6.82	0.0	Yes
1031	STORAGE	74.96	5.44	0.0	Yes
1042	STORAGE	76.67	5.53	0.0	Yes
1044	STORAGE	80.96	3.55	0.0	Yes
1045	STORAGE	78.78	4.23	0.0	Yes
1049	STORAGE	69.50	10.68	0.0	
1051	STORAGE	73.42	25.53	0.0	
106	STORAGE	77.86	6.00	0.0	Yes
107	STORAGE	78.11	5.38	0.0	Yes
1085	STORAGE	82.28	3.49	0.0	Yes
1090	STORAGE	82.75	3.98	0.0	Yes
1091	STORAGE	82.48	4.00	0.0	Yes
1092	STORAGE	82.33	3.98	0.0	Yes
1093	STORAGE	82.81	3.77	0.0	Yes
1096	STORAGE	83.04	3.42	0.0	Yes
1101	STORAGE	83.11	3.93	0.0	Yes
1111	STORAGE	83.39	4.34	0.0	Yes
1114	STORAGE	83.27	4.47	0.0	Yes
1115	STORAGE	83.35	3.96	0.0	Yes
1116	STORAGE	83.22	3.01	0.0	Yes
1117	STORAGE	83.44	3.62	0.0	Yes
112	STORAGE	78.78	4.52	0.0	Yes
1131	STORAGE	82.10	4.59	0.0	
1185	STORAGE	82.13	4.03	0.0	Yes
1186	STORAGE	82.09	4.07	0.0	Yes
1187	STORAGE	81.70	7.27	0.0	Yes
1190	STORAGE	81.36	6.64	0.0	Yes
1191	STORAGE	81.02	7.37	0.0	Yes
1192	STORAGE	85.13	6.10	0.0	Yes
1193	STORAGE	84.63	5.20	0.0	Yes
1195	STORAGE	84.34	6.25	0.0	Yes
1196	STORAGE	84.05	6.53	0.0	Yes
1199	STORAGE	83.08	5.70	0.0	Yes
1202	STORAGE	85.61	5.31	0.0	Yes
1203	STORAGE	85.98	5.23	0.0	Yes
1204	STORAGE	86.48	7.86	0.0	Yes
1205	STORAGE	87.00	8.79	0.0	Yes
1206	STORAGE	87.48	7.18	0.0	Yes
1208	STORAGE	89.69	3.34	0.0	Yes
1209	STORAGE	89.29	4.94	0.0	Yes
1210	STORAGE	88.90	5.15	0.0	Yes
1211	STORAGE	88.41	5.13	0.0	Yes
1212	STORAGE	87.93	5.65	0.0	Yes
1216	STORAGE	91.32	3.92	0.0	Yes
1217	STORAGE	90.66	5.20	0.0	Yes
1218	STORAGE	90.39	7.15	0.0	Yes
1219	STORAGE	90.09	8.60	0.0	Yes
1220	STORAGE	89.83	7.43	0.0	Yes
1221	STORAGE	89.52	5.28	0.0	Yes
1222	STORAGE	91.91	4.99	0.0	Yes
1241	STORAGE	92.91	3.81	0.0	Yes
1242	STORAGE	92.66	4.21	0.0	Yes
1243	STORAGE	92.15	4.88	0.0	Yes
1244	STORAGE	92.15	3.73	0.0	Yes
1245	STORAGE	91.84	3.48	0.0	Yes
1246	STORAGE	91.53	3.62	0.0	Yes
1247	STORAGE	91.18	3.32	0.0	Yes
1248	STORAGE	90.87	4.08	0.0	Yes
1249	STORAGE	90.53	3.76	0.0	Yes
1252	STORAGE	90.13	4.71	0.0	Yes
1253	STORAGE	89.76	4.89	0.0	Yes
1286	STORAGE	89.54	4.67	0.0	Yes
1287	STORAGE	89.32	5.71	0.0	Yes
1288	STORAGE	89.03	3.86	0.0	Yes
1289	STORAGE	88.78	5.38	0.0	Yes
1290	STORAGE	88.50	5.31	0.0	Yes
1291	STORAGE	87.78	5.67	0.0	Yes
1292	STORAGE	87.45	6.66	0.0	Yes
1293	STORAGE	87.12	6.59	0.0	Yes
1294	STORAGE	86.84	7.09	0.0	Yes
1295	STORAGE	86.39	5.70	0.0	Yes
1296	STORAGE	86.02	5.73	0.0	Yes
1297	STORAGE	85.66	3.43	0.0	Yes
1298	STORAGE	85.30	5.45	0.0	Yes
1299	STORAGE	84.95	5.90	0.0	Yes
1303	STORAGE	84.55	7.28	0.0	Yes
1306	STORAGE	84.17	5.87	0.0	Yes
1307	STORAGE	83.73	5.38	0.0	Yes
1308	STORAGE	83.34	5.64	0.0	Yes
1309	STORAGE	82.13	6.78	0.0	Yes
1310	STORAGE	81.58	6.27	0.0	Yes
1344	STORAGE	81.51	5.79	0.0	Yes
1345	STORAGE	81.34	6.14	0.0	Yes
1346	STORAGE	81.00	6.41	0.0	Yes
1347	STORAGE	80.82	6.94	0.0	Yes
1348	STORAGE	80.39	7.46	0.0	Yes
135	STORAGE	80.15	3.94	0.0	Yes
1352	STORAGE	79.90	7.34	0.0	Yes
136	STORAGE	80.48	3.39	0.0	Yes
137	STORAGE	81.14	4.39	0.0	Yes
138	STORAGE	82.38	3.19	0.0	
1511	STORAGE	88.06	3.59	0.0	Yes
1514	STORAGE	87.89	3.41	0.0	Yes
157	STORAGE	80.89	3.23	0.0	Yes
158	STORAGE	81.50	2.62	0.0	
159	STORAGE	80.69	3.67	0.0	
1593	STORAGE	87.44	5.16	0.0	Yes
161	STORAGE	87.16	2.06	0.0	

162	STORAGE	85.79	1.81	0.0	
163	STORAGE	82.39	4.78	0.0	
164	STORAGE	84.11	1.69	0.0	
165	STORAGE	88.44	2.40	0.0	
166	STORAGE	89.92	1.47	0.0	
167	STORAGE	91.14	2.34	0.0	
168	STORAGE	91.64	1.16	0.0	
169	STORAGE	92.30	1.22	0.0	
170	STORAGE	92.56	2.94	0.0	
1705	STORAGE	82.31	3.19	0.0	
171	STORAGE	93.24	3.00	0.0	
1718	STORAGE	84.19	2.95	0.0	
1719	STORAGE	83.65	3.60	0.0	
172	STORAGE	93.22	3.00	0.0	
1720	STORAGE	83.29	4.49	0.0	
1721	STORAGE	82.82	3.98	0.0	
1725	STORAGE	84.54	3.88	0.0	
173	STORAGE	93.03	1.85	0.0	
174	STORAGE	92.77	2.74	0.0	
1742	STORAGE	84.57	3.08	0.0	
1743	STORAGE	84.23	4.55	0.0	
1745	STORAGE	82.13	3.64	0.0	Yes
1746	STORAGE	82.04	3.51	0.0	Yes
1747	STORAGE	81.74	2.65	0.0	
1748	STORAGE	81.66	2.73	0.0	
1749	STORAGE	81.41	3.31	0.0	Yes
175	STORAGE	92.71	2.80	0.0	
1750	STORAGE	81.03	3.10	0.0	Yes
1754	STORAGE	81.97	3.93	0.0	
1755	STORAGE	81.70	3.51	0.0	
1756	STORAGE	81.45	2.71	0.0	
1757	STORAGE	81.32	3.15	0.0	
1758	STORAGE	81.11	3.72	0.0	
1759	STORAGE	80.78	4.29	0.0	
1763	STORAGE	80.10	5.30	0.0	
1768	STORAGE	79.69	4.12	0.0	
1769	STORAGE	79.43	4.00	0.0	
1770	STORAGE	78.95	4.49	0.0	
1771	STORAGE	77.81	4.04	0.0	Yes
1772	STORAGE	79.98	3.51	0.0	Yes
1773	STORAGE	78.90	3.93	0.0	Yes
1774	STORAGE	76.67	5.17	0.0	Yes
1794	STORAGE	75.12	4.04	0.0	Yes
1795	STORAGE	74.84	3.25	0.0	Yes
1796	STORAGE	74.76	3.77	0.0	Yes
1797	STORAGE	74.70	1.58	0.0	Yes
1798	STORAGE	74.56	5.74	0.0	Yes
1799	STORAGE	74.46	4.03	0.0	Yes
1800	STORAGE	74.35	4.22	0.0	Yes
1801	STORAGE	74.22	3.60	0.0	Yes
1812	STORAGE	74.17	6.44	0.0	Yes
1866	STORAGE	74.12	5.95	0.0	Yes
1867	STORAGE	74.00	5.46	0.0	Yes
1868	STORAGE	74.02	5.82	0.0	Yes
1869	STORAGE	73.77	5.38	0.0	Yes
1870	STORAGE	73.67	7.57	0.0	Yes
1871	STORAGE	73.61	8.02	0.0	Yes
1872	STORAGE	73.51	8.09	0.0	Yes
1873	STORAGE	73.36	7.01	0.0	Yes
1874	STORAGE	73.29	8.61	0.0	Yes
1875	STORAGE	73.24	9.87	0.0	Yes
1876	STORAGE	73.01	10.11	0.0	Yes
1877	STORAGE	87.16	3.43	0.0	Yes
1880	STORAGE	86.97	2.29	0.0	Yes
1881	STORAGE	86.77	1.77	0.0	Yes
1898	STORAGE	84.28	1.99	0.0	Yes
1899	STORAGE	84.25	2.02	0.0	Yes
1913	STORAGE	83.87	2.01	0.0	Yes
1914	STORAGE	83.81	2.07	0.0	Yes
1915	STORAGE	83.48	1.69	0.0	Yes
1916	STORAGE	82.90	2.23	0.0	Yes
1917	STORAGE	81.98	3.49	0.0	Yes
1918	STORAGE	81.71	3.75	0.0	Yes
1919	STORAGE	81.19	3.40	0.0	
1920	STORAGE	81.43	3.69	0.0	Yes
1923	STORAGE	81.50	3.10	0.0	Yes
1927	STORAGE	81.23	4.37	0.0	Yes
1931	STORAGE	79.20	3.77	0.0	
1932	STORAGE	77.25	4.45	0.0	Yes
1933	STORAGE	72.74	7.58	0.0	Yes
1938	STORAGE	72.65	11.36	0.0	Yes
1939	STORAGE	72.88	7.85	0.0	Yes
1940	STORAGE	72.73	11.82	0.0	Yes
1941	STORAGE	72.59	8.26	0.0	Yes
1942	STORAGE	71.63	5.87	0.0	Yes
1943	STORAGE	81.74	3.72	0.0	Yes
1968	STORAGE	87.51	4.81	0.0	Yes
1969	STORAGE	87.88	3.59	0.0	Yes
1970	STORAGE	88.00	3.12	0.0	Yes
2029	STORAGE	84.07	3.58	0.0	Yes
2030	STORAGE	84.14	4.38	0.0	Yes
2031	STORAGE	84.22	4.42	0.0	Yes
2032	STORAGE	83.90	3.04	0.0	Yes
2033	STORAGE	84.31	3.98	0.0	Yes
2034	STORAGE	84.39	4.48	0.0	Yes
2035	STORAGE	84.50	3.98	0.0	Yes
2036	STORAGE	84.67	4.40	0.0	Yes
2061	STORAGE	86.95	2.17	0.0	
2062	STORAGE	81.50	3.63	0.0	
2063	STORAGE	81.57	3.56	0.0	Yes
2096	STORAGE	79.55	3.56	0.0	Yes
2097	STORAGE	79.71	5.98	0.0	Yes
2105	STORAGE	87.33	5.61	0.0	Yes
211	STORAGE	91.69	2.37	0.0	Yes
212	STORAGE	92.16	1.48	0.0	
213	STORAGE	91.47	0.65	0.0	Yes
2140	STORAGE	78.65	4.05	0.0	Yes
2140_1	STORAGE	78.77	4.52	0.0	Yes
2140_2	STORAGE	78.86	5.11	0.0	Yes
2140_3	STORAGE	78.96	4.78	0.0	Yes
2140_4	STORAGE	79.02	5.08	0.0	Yes
2141	STORAGE	73.43	5.64	0.0	
2146	STORAGE	89.89	3.13	0.0	Yes
2147	STORAGE	90.42	3.00	0.0	Yes
2148	STORAGE	90.85	2.11	0.0	Yes
2154	STORAGE	77.90	3.12	0.0	Yes
2155	STORAGE	76.81	5.96	0.0	Yes
216	STORAGE	91.30	0.88	0.0	Yes
2176	STORAGE	83.55	3.99	0.0	
2177	STORAGE	83.61	3.40	0.0	
2178	STORAGE	83.68	3.95	0.0	
2179	STORAGE	83.76	3.14	0.0	Yes
2180	STORAGE	83.79	2.39	0.0	Yes
2217	STORAGE	86.78	6.84	0.0	Yes
2218	STORAGE	86.62	5.79	0.0	Yes
2219	STORAGE	86.46	5.71	0.0	Yes
222	STORAGE	90.98	1.20	0.0	Yes
2220	STORAGE	85.95	7.46	0.0	Yes
2221	STORAGE	86.08	7.46	0.0	Yes
2222	STORAGE	85.57	7.31	0.0	Yes
2223	STORAGE	85.41	5.81	0.0	Yes
2224	STORAGE	85.16	5.82	0.0	Yes
2259	STORAGE	87.05	7.71	0.0	Yes
2264	STORAGE	84.89	3.22	0.0	
2265	STORAGE	81.87	6.23	0.0	
2266	STORAGE	81.18	4.98	0.0	
2267	STORAGE	78.90	7.18	0.0	
2268	STORAGE	85.46	4.36	0.0	
2269	STORAGE	81.25	4.53	0.0	
2270	STORAGE	80.01	6.04	0.0	
2282	STORAGE	71.01	8.05	0.0	
2282_1	STORAGE	71.01	8.05	0.0	Yes
2282_2	STORAGE	73.30	5.76	0.0	
2286	STORAGE	86.62	2.84	0.0	Yes
2300	STORAGE	88.20	5.25	0.0	Yes
2301	STORAGE	88.80	5.26	0.0	Yes
2302	STORAGE	88.90	5.16	0.0	Yes
2303	STORAGE	89.17	4.30	0.0	Yes
2304	STORAGE	89.20	4.28	0.0	Yes
2305	STORAGE	89.60	6.65	0.0	Yes
2306	STORAGE	90.08	7.69	0.0	Yes
2307	STORAGE	90.45	6.29	0.0	Yes
2309	STORAGE	91.00	6.95	0.0	Yes
231	STORAGE	90.64	0.50	0.0	Yes
2310	STORAGE	91.36	4.81	0.0	Yes
2311	STORAGE	91.31	4.96	0.0	Yes
2312	STORAGE	91.99	4.47	0.0	Yes
2313	STORAGE	93.94	1.49	0.0	Yes
2314	STORAGE	94.55	3.71	0.0	Yes
2315	STORAGE	94.98	3.90	0.0	Yes
2317	STORAGE	95.20	4.56	0.0	Yes
2318	STORAGE	97.15	4.24	0.0	Yes
2319	STORAGE	97.64	3.73	0.0	Yes
2320	STORAGE	97.85	6.30	0.0	Yes
2321	STORAGE	98.07	4.75	0.0	Yes
2341	STORAGE	93.87	2.99	0.0	Yes
2342	STORAGE	94.15	3.65	0.0	Yes
2343	STORAGE	94.36	4.00	0.0	Yes
2344	STORAGE	94.50	3.50	0.0	Yes
2345	STORAGE	94.60	3.40	0.0	Yes
2346	STORAGE	94.79	3.54	0.0	Yes
2347	STORAGE	95.25	3.61	0.0	Yes
2348	STORAGE	95.56	4.75	0.0	Yes
2349	STORAGE	95.74	4.57	0.0	Yes
236	STORAGE	89.70	1.54	0.0	Yes
2363	STORAGE	89.17	5.05	0.0	Yes
2364	STORAGE	89.30	4.92	0.0	Yes
2365	STORAGE	89.63	4.90	0.0	
2366	STORAGE	89.93	4.65	0.0	Yes
2367	STORAGE	90.29	3.86	0.0	Yes
2368	STORAGE	90.37	3.78	0.0	Yes
2369	STORAGE	90.53	4.10	0.0	Yes
2370	STORAGE	90.83	3.29	0.0	Yes
2371	STORAGE	90.89	3.23	0.0	Yes
2372	STORAGE	91.22	3.42	0.0	Yes
2373	STORAGE	91.53	6.21	0.0	Yes
2374	STORAGE	91.83	5.57	0.0	Yes
2375	STORAGE	92.14	4.36	0.0	Yes
2376	STORAGE	92.44	3.88	0.0	Yes
2377	STORAGE	92.74	5.38	0.0	Yes
2378	STORAGE	93.05	3.52	0.0	Yes
2379	STORAGE	93.37	3.79	0.0	Yes
2380	STORAGE	93.42	3.74	0.0	Yes
2381	STORAGE	93.78	4.14	0.0	Yes
2382	STORAGE	94.08	4.71	0.0	Yes
2383	STORAGE	94.32	3.41	0.0	Yes
2384	STORAGE	94.64	3.79	0.0	Yes
2385	STORAGE	94.91	4.33	0.0	Yes
2386	STORAGE	95.27	3.70	0.0	Yes
2387	STORAGE	95.58	3.88	0.0	Yes
2388	STORAGE	95.88	5.13	0.0	Yes
2389	STORAGE	96.19	4.92	0.0	Yes
2390	STORAGE	96.49	3.71	0.0	Yes
2391	STORAGE	96.86	4.20	0.0	Yes
2392	STORAGE	97.01	4.18	0.0	Yes
2393	STORAGE	98.13	4.06	0.0	Yes
2394	STORAGE	98.33	3.35	0.0	Yes
2395	STORAGE	98.53	3.33	0.0	Yes
2397	STORAGE	95.36	5.26	0.0	Yes
2398	STORAGE	95.67	4.44	0.0	Yes
2399	STORAGE	95.97	6.56	0.0	Yes
2400	STORAGE	96.27	6.40	0.0	Yes

2401	STORAGE	96.65	4.58	0.0	Yes
2402	STORAGE	96.95	3.83	0.0	Yes
2453	STORAGE	86.38	5.97	0.0	Yes
2474	STORAGE	75.54	6.17	0.0	Yes
2475	STORAGE	75.17	6.93	0.0	Yes
2476	STORAGE	74.77	8.26	0.0	Yes
2477	STORAGE	74.50	6.37	0.0	Yes
284	STORAGE	78.39	3.19	0.0	Yes
285	STORAGE	78.34	2.70	0.0	Yes
286	STORAGE	77.88	3.69	0.0	Yes
287	STORAGE	75.99	6.89	0.0	Yes
288	STORAGE	75.74	4.52	0.0	Yes
289	STORAGE	75.38	7.39	0.0	Yes
290	STORAGE	75.25	6.26	0.0	Yes
300	STORAGE	92.78	0.58	0.0	Yes
3000	STORAGE	77.83	6.67	0.0	Yes
3000A	STORAGE	77.76	6.72	0.0	Yes
301	STORAGE	92.26	1.28	0.0	Yes
302	STORAGE	93.43	0.50	0.0	Yes
303	STORAGE	93.14	0.51	0.0	Yes
360	STORAGE	81.29	4.50	0.0	Yes
401	STORAGE	75.07	6.09	0.0	Yes
402	STORAGE	74.70	5.59	0.0	Yes
403	STORAGE	74.37	8.10	0.0	Yes
404	STORAGE	73.64	9.63	0.0	
405	STORAGE	73.46	9.62	0.0	
406	STORAGE	73.16	7.76	0.0	Yes
409	STORAGE	74.11	8.16	0.0	Yes
411	STORAGE	73.68	9.35	0.0	Yes
413	STORAGE	74.42	6.08	0.0	Yes
414	STORAGE	73.98	5.08	0.0	
418	STORAGE	75.72	6.85	0.0	Yes
419	STORAGE	75.86	5.53	0.0	Yes
421	STORAGE	74.79	6.93	0.0	Yes
424	STORAGE	75.33	8.20	0.0	Yes
425	STORAGE	74.16	7.58	0.0	Yes
426	STORAGE	73.45	7.05	0.0	Yes
427	STORAGE	73.45	5.61	0.0	
428	STORAGE	76.99	5.06	0.0	Yes
429	STORAGE	75.79	5.52	0.0	Yes
431	STORAGE	75.96	5.43	0.0	Yes
432	STORAGE	76.58	5.83	0.0	Yes
433	STORAGE	77.16	7.42	0.0	
434	STORAGE	77.17	7.40	0.0	Yes
435	STORAGE	87.39	0.50	0.0	Yes
436	STORAGE	79.22	4.47	0.0	Yes
437	STORAGE	76.85	7.84	0.0	
438	STORAGE	77.84	6.85	0.0	
439	STORAGE	76.72	5.85	0.0	Yes
44	STORAGE	78.55	4.43	0.0	Yes
446	STORAGE	80.39	5.28	0.0	Yes
447	STORAGE	80.17	5.49	0.0	Yes
448	STORAGE	79.63	4.13	0.0	Yes
449	STORAGE	77.08	7.79	0.0	Yes
45	STORAGE	78.33	4.77	0.0	Yes
451	STORAGE	78.04	6.15	0.0	Yes
452	STORAGE	77.25	7.32	0.0	Yes
453	STORAGE	77.99	6.34	0.0	Yes
454	STORAGE	77.52	6.70	0.0	Yes
455	STORAGE	80.10	5.94	0.0	
456	STORAGE	80.92	5.58	0.0	
457	STORAGE	78.03	8.01	0.0	Yes
458	STORAGE	77.73	6.25	0.0	Yes
459	STORAGE	78.85	7.12	0.0	Yes
460	STORAGE	77.49	8.10	0.0	Yes
461	STORAGE	78.68	7.69	0.0	
462	STORAGE	78.51	7.86	0.0	Yes
463	STORAGE	78.51	4.17	0.0	Yes
464	STORAGE	78.33	5.28	0.0	Yes
465	STORAGE	78.35	7.38	0.0	Yes
468	STORAGE	78.45	5.74	0.0	Yes
469	STORAGE	78.59	6.05	0.0	Yes
473	STORAGE	78.17	7.74	0.0	Yes
477	STORAGE	79.73	5.42	0.0	Yes
478	STORAGE	79.34	6.56	0.0	Yes
479	STORAGE	82.09	5.69	0.0	Yes
480	STORAGE	81.51	5.74	0.0	Yes
481	STORAGE	80.30	5.88	0.0	Yes
501	STORAGE	78.90	5.18	0.0	Yes
502	STORAGE	78.83	5.59	0.0	Yes
503	STORAGE	78.55	7.18	0.0	Yes
506	STORAGE	79.32	5.61	0.0	Yes
507	STORAGE	79.92	4.54	0.0	Yes
508	STORAGE	79.58	5.12	0.0	Yes
51	STORAGE	78.21	4.44	0.0	Yes
511	STORAGE	80.89	5.46	0.0	Yes
512	STORAGE	80.33	5.45	0.0	Yes
513	STORAGE	80.81	4.92	0.0	Yes
514	STORAGE	81.03	6.63	0.0	Yes
516	STORAGE	81.16	5.98	0.0	
521	STORAGE	81.11	6.55	0.0	Yes
54	STORAGE	78.08	5.09	0.0	Yes
55_1	STORAGE	78.01	5.20	0.0	Yes
553	STORAGE	88.78	4.67	0.0	Yes
554	STORAGE	88.19	6.05	0.0	Yes
555	STORAGE	88.09	7.15	0.0	Yes
556	STORAGE	87.89	7.88	0.0	Yes
56	STORAGE	77.92	4.78	0.0	Yes
563	STORAGE	88.55	5.55	0.0	Yes
63	STORAGE	77.84	4.55	0.0	Yes
64	STORAGE	77.72	4.55	0.0	Yes
649	STORAGE	87.76	8.21	0.0	Yes
65	STORAGE	77.56	4.71	0.0	Yes
65_1	STORAGE	77.51	4.76	0.0	
650	STORAGE	87.66	6.65	0.0	Yes
652	STORAGE	87.58	7.40	0.0	Yes
653	STORAGE	87.54	6.07	0.0	Yes
654	STORAGE	87.37	5.56	0.0	Yes
66	STORAGE	72.15	10.00	0.0	
666	STORAGE	89.45	4.46	0.0	Yes
667	STORAGE	89.10	4.95	0.0	Yes
668	STORAGE	88.83	7.17	0.0	Yes
669	STORAGE	88.47	7.53	0.0	Yes
670	STORAGE	88.32	5.83	0.0	Yes
671	STORAGE	88.15	4.81	0.0	Yes
672	STORAGE	88.01	5.74	0.0	Yes
673	STORAGE	87.21	7.38	0.0	Yes
675	STORAGE	87.17	6.11	0.0	Yes
676	STORAGE	87.11	7.66	0.0	Yes
678	STORAGE	86.92	7.80	0.0	Yes
68	STORAGE	77.79	5.68	0.0	Yes
682	STORAGE	88.91	4.77	0.0	Yes
684	STORAGE	88.59	6.49	0.0	Yes
685	STORAGE	86.79	6.83	0.0	Yes
686	STORAGE	86.61	5.80	0.0	Yes
689	STORAGE	86.50	6.05	0.0	Yes
690	STORAGE	86.30	4.15	0.0	Yes
708	STORAGE	89.24	5.43	0.0	Yes
780	STORAGE	86.18	6.09	0.0	Yes
781	STORAGE	85.88	5.96	0.0	Yes
782	STORAGE	85.72	5.33	0.0	Yes
783	STORAGE	85.56	6.65	0.0	Yes
796	STORAGE	91.99	3.01	0.0	Yes
852	STORAGE	91.32	2.84	0.0	Yes
853	STORAGE	90.65	3.48	0.0	Yes
859	STORAGE	89.28	3.53	0.0	Yes
860	STORAGE	89.96	3.81	0.0	Yes
861	STORAGE	89.77	4.01	0.0	Yes
864	STORAGE	87.81	3.70	0.0	Yes
865	STORAGE	88.46	3.20	0.0	Yes
866	STORAGE	87.66	2.52	0.0	Yes
877	STORAGE	86.55	4.23	0.0	Yes
878	STORAGE	87.35	2.83	0.0	Yes
879	STORAGE	86.06	4.72	0.0	Yes
880	STORAGE	85.65	3.21	0.0	Yes
881	STORAGE	85.27	5.05	0.0	Yes
882	STORAGE	84.88	4.81	0.0	Yes
883	STORAGE	85.30	5.20	0.0	Yes
884	STORAGE	85.18	5.80	0.0	Yes
885	STORAGE	84.96	4.73	0.0	Yes
886	STORAGE	84.12	6.09	0.0	Yes
887	STORAGE	83.52	5.34	0.0	Yes
9001	STORAGE	84.48	2.50	0.0	Yes
9002	STORAGE	84.27	1.90	0.0	Yes
9003	STORAGE	84.24	3.24	0.0	Yes
9004	STORAGE	84.20	3.38	0.0	Yes
9005	STORAGE	84.17	3.41	0.0	Yes
9006	STORAGE	84.05	3.02	0.0	Yes
9050	STORAGE	86.45	3.48	0.0	Yes
9051	STORAGE	86.34	3.46	0.0	Yes
9052	STORAGE	85.93	4.09	0.0	Yes
9053	STORAGE	85.52	4.50	0.0	Yes
9054	STORAGE	85.38	4.67	0.0	Yes
9055	STORAGE	82.51	4.93	0.0	Yes
9056	STORAGE	79.67	3.78	0.0	Yes
9057	STORAGE	77.26	4.76	0.0	Yes
9058	STORAGE	76.56	5.16	0.0	Yes
9059	STORAGE	76.25	5.22	0.0	Yes
9060	STORAGE	75.75	4.50	0.0	Yes
9061	STORAGE	75.63	4.62	0.0	Yes
924	STORAGE	87.50	3.47	0.0	Yes
940	STORAGE	83.56	3.54	0.0	Yes
941	STORAGE	86.78	3.69	0.0	
942	STORAGE	81.50	5.09	0.0	Yes
945	STORAGE	81.58	6.31	0.0	
946	STORAGE	81.38	6.64	0.0	
948	STORAGE	83.04	4.96	0.0	
978	STORAGE	79.32	3.97	0.0	Yes
984	STORAGE	78.73	4.27	0.0	Yes
985	STORAGE	78.50	4.50	0.0	Yes
986	STORAGE	78.25	6.06	0.0	Yes
987	STORAGE	77.94	6.67	0.0	Yes
988	STORAGE	77.53	6.95	0.0	Yes
9902	STORAGE	70.78	9.49	0.0	
991	STORAGE	77.50	7.03	0.0	Yes
996	STORAGE	77.09	4.97	0.0	Yes
997	STORAGE	76.77	7.31	0.0	Yes
999	STORAGE	76.51	8.02	0.0	Yes

****
Link Summary
****

Name	From Node	To Node	Type	Length	%Slope	Roughness
1001	997	999	CONDUIT	65.8	0.4106	0.0130
1009	1005	1007	CONDUIT	49.2	0.3619	0.0130
1010	1007	1008	CONDUIT	82.5	0.2703	0.0130
1011	999	1008	CONDUIT	69.9	0.1288	0.0130
1023	1008	1020	CONDUIT	91.3	0.6460	0.0130
1025	1020	1022	CONDUIT	4.2	0.2387	0.0130
1026	1022	1023	CONDUIT	83.4	0.3958	0.0130
1027	1023	1024	CONDUIT	98.3	0.4884	0.0130
1028	1024	1025	CONDUIT	57.2	0.4772	0.0130
1029	1025	1026	CONDUIT	9.9	0.9880	0.0130
103	106	68	CONDUIT	65.0	0.0585	0.0130
1030	1026	9902	CONDUIT	11.5	2.0004	0.0130
1032	1029	1030	CONDUIT	2.7	1.1030	0.0130
1033	1030	1031	CONDUIT	97.0	0.4817	0.0130
104	107	106	CONDUIT	63.9	0.3383	0.0130
1045	1042	1029	CONDUIT	125.1	0.9161	0.0130
1046	1044	1045	CONDUIT	100.9	1.3899	0.0130

1048	1045	1042	CONDUIT	125.6	1.4979	0.0130
1050	965	1048	CONDUIT	17.0	0.1767	0.0130
1052	1031	1026	CONDUIT	49.6	0.3834	0.0130
1054_1	2152	9914	CONDUIT	698.0	0.0980	0.0130
1054_2	9914	1048	CONDUIT	7.7	0.1043	0.0130
109	112	107	CONDUIT	79.0	0.8051	0.0130
1090	1090	1091	CONDUIT	68.2	0.3974	0.0130
1091	1091	1092	CONDUIT	99.6	0.1566	0.0130
1092	1092	1085	CONDUIT	69.0	0.0652	0.0130
1093	1093	1090	CONDUIT	91.1	0.0571	0.0130
1096	1096	1093	CONDUIT	87.1	0.2732	0.0130
1103	1101	1096	CONDUIT	79.5	0.0843	0.0130
1116	1111	1114	CONDUIT	19.6	0.6371	0.0130
1117	1114	1115	CONDUIT	20.1	-0.4277	0.0130
1118	1115	1116	CONDUIT	115.8	0.1166	0.0130
1119	1116	1101	CONDUIT	9.2	1.1498	0.0130
1120	1117	1111	CONDUIT	42.2	0.1232	0.0130
1179	1175	1176	CONDUIT	30.0	0.6004	0.0130
1180	1176	1177	CONDUIT	79.7	0.1255	0.0130
1181	1177	1178	CONDUIT	96.1	0.2705	0.0130
1182	1178	1179	CONDUIT	65.1	0.3686	0.0130
1183	1179	1180	CONDUIT	108.1	0.4904	0.0130
1184	1180	1181	CONDUIT	79.8	0.2881	0.0130
1185	1181	1182	CONDUIT	85.5	0.2621	0.0130
1186	1182	950	CONDUIT	109.0	0.2871	0.0130
1189	1185	1186	CONDUIT	13.1	0.3209	0.0130
1190	1186	1187	CONDUIT	125.7	0.3104	0.0130
1193	1187	1190	CONDUIT	130.9	0.2415	0.0130
1194	1190	1191	CONDUIT	115.6	0.2983	0.0130
1195	1191	1175	CONDUIT	54.6	0.2343	0.0130
1196	1192	1193	CONDUIT	95.5	0.5236	0.0130
1198	1193	1195	CONDUIT	76.5	0.3584	0.0130
1199	1195	1196	CONDUIT	65.3	0.4410	0.0130
1202	1196	1199	CONDUIT	125.6	0.7773	0.0130
1203	1199	1185	CONDUIT	122.9	0.7069	0.0130
1206	1202	1192	CONDUIT	154.4	0.3075	0.0130
1207	1203	1202	CONDUIT	75.9	0.4864	0.0130
1208	1204	1203	CONDUIT	121.9	0.4151	0.0130
1209	1205	1204	CONDUIT	134.6	0.3826	0.0130
1210	1206	1205	CONDUIT	107.8	0.4442	0.0130
1212	1208	1209	CONDUIT	86.9	0.4590	0.0130
1213	1209	1210	CONDUIT	94.7	0.0961	0.0130
1214	1210	1211	CONDUIT	134.1	0.3683	0.0130
1215	1211	1212	CONDUIT	89.2	0.5326	0.0130
1216	1212	1206	CONDUIT	145.9	0.3111	0.0130
1220	1216	1217	CONDUIT	90.1	0.6594	0.0130
1221	1217	1218	CONDUIT	93.8	0.2931	0.0130
1222	1218	1219	CONDUIT	102.3	0.2855	0.0130
1223	1219	1220	CONDUIT	77.9	0.3325	0.0130
1224	1220	1221	CONDUIT	78.9	0.4020	0.0130
1225	1221	1210	CONDUIT	85.7	0.3734	0.0130
1226	1222	1216	CONDUIT	108.4	0.5454	0.0130
1245	1241	1242	CONDUIT	61.4	0.4171	0.0130
1246	1242	1243	CONDUIT	94.7	0.5342	0.0130
1247	1243	1244	CONDUIT	83.2	0.3078	0.0130
1248	1244	1245	CONDUIT	83.4	0.3729	0.0130
1249	1245	1246	CONDUIT	76.0	0.4134	0.0130
1250	1246	1247	CONDUIT	80.0	0.4376	0.0130
1251	1247	1248	CONDUIT	72.9	0.4182	0.0130
1252	1248	1249	CONDUIT	103.3	0.3358	0.0130
1255	1249	1252	CONDUIT	106.5	0.3783	0.0130
1256	1252	1253	CONDUIT	75.7	0.4966	0.0130
1290	1253	1286	CONDUIT	55.6	0.3958	0.0130
1291	1286	1287	CONDUIT	71.4	0.3024	0.0130
1292	1287	1288	CONDUIT	71.8	0.4041	0.0130
1293	1288	1289	CONDUIT	83.3	0.3074	0.0130
1294	1289	1290	CONDUIT	83.3	0.3253	0.0130
1295	1290	1291	CONDUIT	74.6	0.9078	0.0130
1296	1291	1292	CONDUIT	87.5	0.3199	0.0130
1297	1292	1293	CONDUIT	79.6	0.3394	0.0130
1298	1293	1294	CONDUIT	51.9	0.4239	0.0130
1299	1294	1295	CONDUIT	95.4	0.3670	0.0130
1300	1295	1296	CONDUIT	96.5	0.3211	0.0130
1301	1296	1297	CONDUIT	92.6	0.3240	0.0130
1302	1297	1298	CONDUIT	70.7	0.4243	0.0130
1303	1298	1299	CONDUIT	82.4	0.3396	0.0130
1308	1299	1303	CONDUIT	97.3	0.3495	0.0130
1311	1303	1306	CONDUIT	79.2	0.4038	0.0130
1312	1306	1307	CONDUIT	86.5	0.3813	0.0130
1313	1307	1308	CONDUIT	89.0	0.3708	0.0130
1314	1308	1309	CONDUIT	72.1	0.9021	0.0130
1315	1309	1310	CONDUIT	120.2	0.3826	0.0130
1316	1310	1175	CONDUIT	94.4	0.4871	0.0130
132	135	112	CONDUIT	107.9	1.2469	0.0130
133	136	135	CONDUIT	69.1	0.3052	0.0130
134	137	136	CONDUIT	141.0	0.4455	0.0130
1348	1344	1345	CONDUIT	32.3	0.5110	0.0130
1349	1345	1346	CONDUIT	82.0	0.4112	0.0130
1350	1346	1347	CONDUIT	57.1	0.2627	0.0130
1351	1347	1348	CONDUIT	103.9	0.3801	0.0130
154	138	157	CONDUIT	99.1	0.1968	0.0130
155	158	157	CONDUIT	22.0	1.7974	0.0130
156	157	159	CONDUIT	12.2	1.4474	0.0130
158	2061	162	CONDUIT	76.7	1.5175	0.0130
159	162	163	CONDUIT	89.4	3.8064	0.0130
160	163	164	CONDUIT	81.8	0.7630	0.0130
161	164	158	CONDUIT	79.6	3.2816	0.0130
162	165	161	CONDUIT	106.0	1.2047	0.0130
163	166	165	CONDUIT	87.3	1.7002	0.0130
164	167	166	CONDUIT	89.9	1.3501	0.0130
165	168	167	CONDUIT	99.2	0.5069	0.0130
166	169	168	CONDUIT	94.2	0.6888	0.0130
167	170	169	CONDUIT	44.7	0.6012	0.0130
168	171	172	CONDUIT	8.8	2.8759	0.0130
169	172	173	CONDUIT	77.4	0.2520	0.0130
170	173	174	CONDUIT	107.2	0.2221	0.0130
1703	1705	1131	CONDUIT	85.3	0.1395	0.0130
171	174	175	CONDUIT	7.0	-0.3442	0.0130
1716	1718	1719	CONDUIT	75.4	0.7125	0.0130
1717	1719	1720	CONDUIT	90.1	0.3984	0.0130
1718	1720	1721	CONDUIT	81.4	0.5813	0.0130
1719	1721	1705	CONDUIT	94.0	0.5446	0.0130
172	175	170	CONDUIT	8.6	1.5562	0.0130
1742	1742	1718	CONDUIT	73.3	0.5401	0.0130
1743	1743	2176	CONDUIT	88.7	0.7945	0.0130
1745	1725	1743	CONDUIT	91.2	0.3376	0.0130
1746	1725	1742	CONDUIT	49.9	-0.0521	0.0130
1747	1085	1745	CONDUIT	19.0	0.7729	0.0130
1748	1745	1746	CONDUIT	99.6	0.0974	0.0130
1749	1746	1747	CONDUIT	98.4	0.3040	0.0130
1750	1747	1748	CONDUIT	17.8	0.4448	0.0130
1751	1748	1749	CONDUIT	147.0	0.1721	0.0130
1752	1749	1750	CONDUIT	124.1	0.3045	0.0130
1755	1131	1754	CONDUIT	87.1	0.1503	0.0130
1756	1754	1755	CONDUIT	72.5	0.3285	0.0130
1757	1755	1756	CONDUIT	93.3	0.2583	0.0130
1759	1756	1757	CONDUIT	75.4	0.1659	0.0130
1760	1757	1758	CONDUIT	64.9	0.3252	0.0130
1761	1758	1759	CONDUIT	37.4	0.4300	0.0130
1766	1759	1763	CONDUIT	73.8	0.3105	0.0130
1772	1763	1768	CONDUIT	102.1	-0.0362	0.0130
1773	1768	1769	CONDUIT	25.8	1.0265	0.0130
1774	1769	1770	CONDUIT	12.3	3.9368	0.0130
1775	1770	1771	CONDUIT	85.2	1.3343	0.0130
1776	1750	1772	CONDUIT	87.6	1.1966	0.0130
1777	1772	1773	CONDUIT	74.5	1.4448	0.0130
1778	1773	1771	CONDUIT	74.5	1.4663	0.0130
1779	1771	1774	CONDUIT	30.1	3.7839	0.0130
1802	1774	1794	CONDUIT	138.7	1.1209	0.0130
1803	1794	1795	CONDUIT	141.7	0.1977	0.0130
1804	1795	1796	CONDUIT	68.8	0.1206	0.0130
1805	1796	1797	CONDUIT	96.8	0.0630	0.0130
1806	1797	1798	CONDUIT	85.8	0.1562	0.0130
1807	1798	1799	CONDUIT	77.8	0.1324	0.0130
1808	1799	1800	CONDUIT	116.8	0.0967	0.0130
1809	1800	1801	CONDUIT	94.6	0.1321	0.0130
1821	1801	1812	CONDUIT	95.6	0.0544	0.0130
1877	1812	1866	CONDUIT	112.5	0.0409	0.0130
1878	1866	1867	CONDUIT	96.2	0.1268	0.0130
1879	1867	1868	CONDUIT	61.3	-0.0261	0.0130
1880	1868	1869	CONDUIT	100.3	0.2521	0.0130
1881	1869	1870	CONDUIT	91.3	0.1007	0.0130
1882	1870	1871	CONDUIT	91.0	0.0703	0.0130
1883	1871	1872	CONDUIT	109.1	0.0889	0.0130
1884	1872	1873	CONDUIT	107.7	0.1448	0.0130
1885	1873	1874	CONDUIT	94.6	0.1649	0.0130
1886	1874	1875	CONDUIT	61.2	0.0800	0.0130
1887	1875	1876	CONDUIT	102.6	0.1716	0.0130
1888	1593	1877	CONDUIT	118.3	0.2291	0.0130
1891	1877	1880	CONDUIT	79.8	0.2330	0.0130
1893	1880	1881	CONDUIT	163.8	0.1227	0.0130
1905	1881	2286	CONDUIT	94.1	0.1595	0.0130
1912	1898	1899	CONDUIT	6.0	0.1508	0.0130
1925	1899	1913	CONDUIT	46.1	0.7934	0.0130
1926	1913	1914	CONDUIT	7.5	0.2008	0.0130
1927	1914	1915	CONDUIT	82.6	0.3839	0.0130
1929	1915	1916	CONDUIT	89.9	0.6110	0.0130
1931	1916	1917	CONDUIT	115.7	0.7664	0.0130
1933	1918	1919	CONDUIT	17.0	3.2526	0.0130
1934	1917	1918	CONDUIT	20.3	1.3229	0.0130
1935	1943	1920	CONDUIT	62.3	0.4204	0.0130
1946	1920	1923	CONDUIT	74.5	-0.0859	0.0130
1947	1923	1927	CONDUIT	101.6	0.2735	0.0130
1948	1927	1044	CONDUIT	101.1	0.2622	0.0130
1949	1919	1931	CONDUIT	92.8	2.0912	0.0130
1950	1931	1932	CONDUIT	73.3	2.6575	0.0130
1951	1932	1933	CONDUIT	111.3	1.8462	0.0130
1956	1876	1939	CONDUIT	103.2	0.1299	0.0130
1957	1939	1940	CONDUIT	84.5	0.1740	0.0130
1958	1940	1938	CONDUIT	81.9	0.1001	0.0130
1959	1938	1941	CONDUIT	49.9	0.1163	0.0130
1960	1941	1942	CONDUIT	156.9	0.1243	0.0130
1977	1514	1969	CONDUIT	26.2	0.0457	0.0130
1978	1969	1968	CONDUIT	93.5	0.4009	0.0130
1979	1968	1593	CONDUIT	97.2	0.0751	0.0130
1980	1970	1514	CONDUIT	23.6	0.4416	0.0130
2015	2031	2030	CONDUIT	89.4	0.0839	0.0130
2016	2029	2032	CONDUIT	62.1	0.1015	0.0130
2017	2030	2029	CONDUIT	79.3	0.0681	0.0130
2018	2033	2031	CONDUIT	80.7	0.1066	0.0130
2019	2034	2033	CONDUIT	126.5	0.0648	0.0130
2020	2035	2034	CONDUIT	50.1	0.2216	0.0130
2021	2036	2035	CONDUIT	101.8	0.1356	0.0130
2029	1511	1970	CONDUIT	95.1	0.0652	0.0130
2048	161	2061	CONDUIT	15.2	1.4104	0.0130
2049	435	2063	CONDUIT	48.6	9.3456	0.0130
2056	418	421	CONDUIT	39.6	2.3454	0.0130
208	171	212	CONDUIT	93.8	1.4208	0.0130
2082	1352	2097	CONDUIT	91.5	0.2098	0.0130
2083	2097	2096	CONDUIT	87.0	0.1817	0.0130
2084	2096	978	CONDUIT	114.2	0.2040	0.0130
2085	1348	1352	CONDUIT	86.4	0.5348	0.0130
2086	978	984	CONDUIT	149.3	0.3919	0.0130
2087	984	985	CONDUIT	58.4	0.3870	0.0130
209	212	211	CONDUIT	96.4	0.4805	0.0130
2099	654	2105	CONDUIT	31.4	0.1464	0.0130
210	211	213	CONDUIT	92.9	0.2356	0.0130
2135	2140	44	CONDUIT	104.5	0.0957	0.0130
2135_1	2140_1	2140	CONDUIT	115.5	0.1039	0.0130
2135_2	2140_2	2140_1	CONDUIT	95.1	0.0947	0.0130
2135_3	2140_3	2140_2	CONDUIT	102.6	0.0974	0.0130
2135_4	2140_4	2140_3	CONDUIT	59.8	0.1004	0.0130

2136	2141	2282	CONDUIT	7.1	1.7259	0.0130
2137	414	427	CONDUIT	52.6	0.9732	0.0130
2138	427	2141	CONDUIT	7.9	0.5471	0.0130
2140	2276	2277	CONDUIT	88.0	0.7727	0.0130
2144	2146	1208	CONDUIT	35.9	0.3208	0.0130
2145	2148	2147	CONDUIT	114.2	0.3834	0.0130
2146	2147	2146	CONDUIT	120.6	0.3965	0.0130
2147	1051	2151	CONDUIT	367.2	0.5087	0.0130
2149	2151	2152	CONDUIT	170.1	0.0970	0.0130
2152	2154	2155	CONDUIT	116.5	0.9337	0.0130
2153	2155	289	CONDUIT	8.3	0.5200	0.0130
216	213	216	CONDUIT	64.6	0.2646	0.0130
2175	2178	2177	CONDUIT	73.8	0.0949	0.0130
2176	2176	1117	CONDUIT	41.8	0.2584	0.0130
2177	2177	2176	CONDUIT	85.0	0.0706	0.0130
2178	2032	2180	CONDUIT	116.0	0.0948	0.0130
2179	2180	2179	CONDUIT	20.7	0.1446	0.0130
2180	2180	2179	CONDUIT	20.3	0.1479	0.0130
2181	2179	2178	CONDUIT	103.0	0.0776	0.0130
219	216	222	CONDUIT	97.0	0.3329	0.0130
2219	685	2217	CONDUIT	9.5	0.1056	0.0130
2220	2218	686	CONDUIT	8.5	0.1179	0.0130
2221	689	2219	CONDUIT	26.0	0.1540	0.0130
2222	2220	781	CONDUIT	31.1	0.2247	0.0130
2223	780	2221	CONDUIT	32.4	1.9163	0.0130
2224	783	2222	CONDUIT	30.4	0.1645	0.0130
2225	2223	883	CONDUIT	36.5	0.3010	0.0130
2226	884	2224	CONDUIT	28.7	0.0696	0.0130
2264	676	2259	CONDUIT	30.4	0.1711	0.0130
2269	2264	948	CONDUIT	25.0	2.9794	0.0130
2270	2265	2266	CONDUIT	171.2	0.4018	0.0130
2271	2267	1182	CONDUIT	11.9	0.8117	0.0130
2272	2266	2267	CONDUIT	19.6	1.5485	0.0130
2273	2264	2265	CONDUIT	7.8	42.1814	0.0130
2274	2268	2265	CONDUIT	65.0	0.3910	0.0130
2277	2062	2273	CONDUIT	46.2	3.1605	0.0130
2278	2063	2062	CONDUIT	3.9	1.9591	0.0130
2279	2273	2275	CONDUIT	136.7	0.8735	0.0130
2280	2275	2276	CONDUIT	102.8	0.2151	0.0130
2281	2277	430	CONDUIT	51.9	0.3217	0.0130
2282	430	2278	CONDUIT	25.1	0.3421	0.0130
2283	2278	962	CONDUIT	68.8	0.4723	0.0130
2284	360	2269	CONDUIT	11.2	0.1696	0.0130
2285	2269	2270	CONDUIT	121.3	1.0250	0.0130
2286	2270	2271	CONDUIT	131.8	0.5477	0.0130
2287	2271	2272	CONDUIT	116.9	0.5493	0.0130
2288	2272	2279	CONDUIT	47.9	0.6114	0.0130
2289	2279	2280	CONDUIT	57.0	5.3050	0.0130
229	222	231	CONDUIT	99.3	0.3443	0.0130
2291	406	2282	CONDUIT	142.5	0.3207	0.0130
2292	2282_1	1049	CONDUIT	165.0	0.1788	0.0130
2339	9006	2032	CONDUIT	64.5	0.2310	0.0130
2340	9005	9006	CONDUIT	25.1	0.5056	0.0130
235	231	236	CONDUIT	94.5	0.9932	0.0130
2390_1	159	DundasFM_3	CONDUIT	15.0	5.6073	0.0130
2390_2	DundasFM_1	DundasFM_2	CONDUIT	10.4	21.1147	0.0130
2390_3	DundasFM_3	DundasFM_2	CONDUIT	10.4	0.0959	0.0130
2390_5	DundasFM_1	67	CONDUIT	641.3	0.3743	0.0130
273	159	284	CONDUIT	84.3	2.4349	0.0130
274	284	285	CONDUIT	15.4	0.2734	0.0130
275	285	286	CONDUIT	115.0	0.4034	0.0130
276	286	287	CONDUIT	108.2	0.7045	0.0130
277	287	288	CONDUIT	159.2	0.1533	0.0130
278	289	290	CONDUIT	141.8	0.0860	0.0130
283	288	289	CONDUIT	123.5	0.2964	0.0130
289	300	301	CONDUIT	90.2	0.5774	0.0130
290	301	211	CONDUIT	85.7	0.6217	0.0130
291	302	303	CONDUIT	53.1	0.5445	0.0130
292	303	300	CONDUIT	65.6	0.5443	0.0130
3300	2300	1291	CONDUIT	20.7	0.4831	0.0130
3301	2301	2300	CONDUIT	164.8	0.3641	0.0130
3302	2302	2301	CONDUIT	20.1	0.4968	0.0130
3303	2303	2302	CONDUIT	86.1	0.3484	0.0130
3304	2304	2303	CONDUIT	10.6	0.2830	0.0130
3305	2305	2304	CONDUIT	110.1	0.3633	0.0130
3306	2306	2305	CONDUIT	129.0	0.3876	0.0130
3307	2307	2306	CONDUIT	114.4	0.3235	0.0130
3309	2309	2307	CONDUIT	162.3	0.3327	0.0130
3310	2310	2309	CONDUIT	102.5	0.3512	0.0130
3311	2311	2310	CONDUIT	60.2	0.3987	0.0130
3312	2312	2311	CONDUIT	78.8	0.8630	0.0130
3313	2313	2312	CONDUIT	106.7	0.5155	0.0130
3314	2314	2313	CONDUIT	105.0	0.5810	0.0130
3315	2315	2314	CONDUIT	105.5	0.4076	0.0130
3317	2317	2315	CONDUIT	108.9	0.2020	0.0130
3318	2318	2317	CONDUIT	102.1	1.9102	0.0130
3319	2319	2318	CONDUIT	103.8	0.4721	0.0130
3320	2320	2319	CONDUIT	103.8	0.2023	0.0130
3321	2321	2320	CONDUIT	105.0	0.2095	0.0130
3339_10	2339	2339_2	CONDUIT	13.0	15.8832	0.0130
3339_11	2339	2339_1	CONDUIT	17.0	12.7662	0.0130
3339_12	2339	2339_3	CONDUIT	18.3	10.8789	0.0130
3339_2	2340_4	2339_2	CONDUIT	113.9	0.0878	0.0130
3339_3	2340_2	2340_5	CONDUIT	17.8	16.0171	0.0130
3339_5	2340	2340_4	CONDUIT	29.8	9.4913	0.0130
3339_6	2340_1	2340_3	CONDUIT	17.9	15.8895	0.0130
3339_8	2340_5	2339_3	CONDUIT	121.6	0.0823	0.0130
3339_9	2340_3	2339_1	CONDUIT	116.4	0.0859	0.0130
3340	2341	2340	CONDUIT	130.2	0.2228	0.0130
3341	2342	2341	CONDUIT	125.0	0.2240	0.0130
3342	2343	2342	CONDUIT	100.1	0.1998	0.0130
3343	2344	2343	CONDUIT	71.8	0.1950	0.0130
3344	2345	2344	CONDUIT	57.0	0.1754	0.0130
3345	2346	2345	CONDUIT	80.0	0.2375	0.0130
3346	2347	2346	CONDUIT	129.7	0.3547	0.0130
3347	2348	2347	CONDUIT	110.0	0.2364	0.0130

3348	2349	2348	CONDUIT	18.8	0.6915	0.0130
3364	2363	553	CONDUIT	124.7	0.2486	0.0130
3365	2364	2363	CONDUIT	21.8	0.4587	0.0130
3366	2365	2364	CONDUIT	120.0	0.2500	0.0130
3367	2366	2365	CONDUIT	120.0	0.2500	0.0130
3368	2367	2366	CONDUIT	140.0	0.2572	0.0130
3369	2368	2367	CONDUIT	20.0	0.2500	0.0130
3370	2369	2368	CONDUIT	54.6	0.2381	0.0130
3371	2370	2369	CONDUIT	117.2	0.2475	0.0130
3372	2371	2370	CONDUIT	13.1	0.4580	0.0130
3373	2372	2371	CONDUIT	120.0	0.2500	0.0130
3374	2373	2372	CONDUIT	120.0	0.2500	0.0130
3375	2374	2373	CONDUIT	120.0	0.2500	0.0130
3376	2375	2374	CONDUIT	120.0	0.2500	0.0130
3377	2376	2375	CONDUIT	120.0	0.2500	0.0130
3378	2377	2376	CONDUIT	120.0	0.2500	0.0130
3379	2378	2377	CONDUIT	120.0	0.2500	0.0130
3380	2379	2378	CONDUIT	125.6	0.2548	0.0130
3381	2380	2379	CONDUIT	9.4	0.2123	0.0130
3382	2381	2380	CONDUIT	132.7	0.2487	0.0130
3383	2382	2381	CONDUIT	96.1	0.2498	0.0130
3384	2383	2382	CONDUIT	96.1	0.2498	0.0130
3385	2384	2383	CONDUIT	104.1	0.2498	0.0130
3386	2385	2384	CONDUIT	104.1	0.2498	0.0130
3387	2386	2385	CONDUIT	115.8	0.2505	0.0130
3388	2387	2386	CONDUIT	120.0	0.2500	0.0130
3389	2388	2387	CONDUIT	120.0	0.2500	0.0130
3390	2389	2388	CONDUIT	120.0	0.2500	0.0130
3391	2390	2389	CONDUIT	120.0	0.2500	0.0130
3392	2391	2390	CONDUIT	144.5	0.2492	0.0130
3393	2392	2391	CONDUIT	28.8	0.2778	0.0130
3394	2393	2392	CONDUIT	96.4	0.2490	0.0130
3395	2394	2393	CONDUIT	80.0	0.2500	0.0130
3396	2395	2394	CONDUIT	77.0	0.2468	0.0130
3398	2397	2385	CONDUIT	122.0	0.2459	0.0130
3399	2398	2397	CONDUIT	120.0	0.2500	0.0130
3400	2399	2398	CONDUIT	120.0	0.2500	0.0130
3401	2400	2399	CONDUIT	120.0	0.2500	0.0130
3402	2401	2400	CONDUIT	120.0	0.2500	0.0130
3403	2402	2401	CONDUIT	120.0	0.2500	0.0130
3500	2339	2312	CONDUIT	37.7	0.1645	0.0130
3502	2474	2475	CONDUIT	104.5	0.3281	0.0130
3503	2475	2476	CONDUIT	107.0	0.3204	0.0130
3504	2476	2477	CONDUIT	75.0	0.2828	0.0130
3505	2477	413	CONDUIT	8.9	0.1119	0.0130
3690	2219	2453	CONDUIT	52.5	0.1524	0.0130
39	44	45	CONDUIT	66.9	0.1046	0.0130
391	290	401	CONDUIT	105.8	0.1730	0.0130
392	401	402	CONDUIT	47.2	0.2901	0.0130
393	402	403	CONDUIT	118.4	0.2779	0.0130
394	403	404	CONDUIT	99.8	0.3058	0.0130
395	404	405	CONDUIT	49.5	0.3699	0.0130
396	405	406	CONDUIT	42.1	0.3633	0.0130
400	411	406	CONDUIT	80.4	0.6516	0.0130
401	409	411	CONDUIT	96.6	0.4451	0.0130
403	413	414	CONDUIT	65.8	0.6713	0.0130
4035	9004	9005	CONDUIT	29.3	0.0990	0.0130
4036	9003	9004	CONDUIT	44.8	0.0916	0.0130
4037	9002	9003	CONDUIT	32.7	0.5561	0.0130
4038	9001	9002	CONDUIT	40.2	0.5299	0.0130
408	421	409	CONDUIT	115.7	0.5851	0.0130
412	424	425	CONDUIT	136.4	0.8514	0.0130
413	425	426	CONDUIT	121.3	0.5877	0.0130
414	426	427	CONDUIT	44.2	0.0407	0.0130
415	428	429	CONDUIT	103.5	1.1575	0.0130
417	429	424	CONDUIT	144.2	0.3204	0.0130
418	431	419	CONDUIT	17.6	0.6382	0.0130
419	432	431	CONDUIT	127.6	0.5061	0.0130
420	433	432	CONDUIT	103.7	0.9648	0.0130
421	434	433	CONDUIT	4.6	1.1404	0.0130
422	433	428	CONDUIT	84.1	0.7832	0.0130
423	236	435	CONDUIT	67.5	3.4059	0.0130
424	2063	436	CONDUIT	52.6	2.9170	0.0130
425	436	437	CONDUIT	52.7	2.1800	0.0130
426	437	438	CONDUIT	5.2	2.9727	0.0130
427	437	439	CONDUIT	110.4	0.1141	0.0130
428	439	418	CONDUIT	126.9	0.4846	0.0130
429	438	434	CONDUIT	76.2	0.8722	0.0130
436	446	447	CONDUIT	45.3	0.4698	0.0130
437	447	448	CONDUIT	99.0	0.5516	0.0130
438	460	449	CONDUIT	131.3	0.3062	0.0130
439	449	437	CONDUIT	94.3	0.2480	0.0130
442	448	451	CONDUIT	80.4	1.9725	0.0130
443	451	452	CONDUIT	165.2	0.4739	0.0130
444	452	434	CONDUIT	31.2	0.1088	0.0130
445	451	453	CONDUIT	79.1	0.0658	0.0130
446	453	454	CONDUIT	106.3	0.4468	0.0130
447	454	428	CONDUIT	91.8	0.5788	0.0130
448	360	455	CONDUIT	94.0	0.9725	0.0100
449	456	455	CONDUIT	400.0	0.1370	0.0100
45	45	51	CONDUIT	119.2	0.1006	0.0130
450	456	447	CONDUIT	86.4	0.5359	0.0100
451	455	457	CONDUIT	31.9	2.2811	0.0100
452	457	458	CONDUIT	54.0	0.5649	0.0130
453	458	459	CONDUIT	13.8	0.1740	0.0130
454	458	460	CONDUIT	136.3	1.0915	0.0130
455	459	461	CONDUIT	52.0	0.3230	0.0130
456	461	462	CONDUIT	22.5	0.4488	0.0130
457	463	462	CONDUIT	15.3	0.3995	0.0130
458	464	451	CONDUIT	69.2	0.4366	0.0130
459	463	464	CONDUIT	60.8	0.2993	0.0130
460	462	465	CONDUIT	79.3	0.2913	0.0130
461	465	453	CONDUIT	127.2	0.3403	0.0130
465	469	468	CONDUIT	14.7	0.9987	0.0130
468	468	473	CONDUIT	90.9	0.3079	0.0130
469	473	457	CONDUIT	93.5	0.1433	0.0130

474	477	478	CONDUIT	100.5	0.3922	0.0130
475	478	469	CONDUIT	64.2	1.1628	0.0130
476	479	480	CONDUIT	74.5	0.7728	0.0130
477	480	481	CONDUIT	41.6	0.3151	0.0130
478	481	477	CONDUIT	140.3	0.4062	0.0130
499	501	502	CONDUIT	39.3	0.1859	0.0130
500	502	503	CONDUIT	109.6	0.2583	0.0130
502	503	465	CONDUIT	13.8	1.3542	0.0130
505	507	508	CONDUIT	113.1	0.3051	0.0130
5050	419	2474	CONDUIT	37.6	0.9567	0.0130
506	508	506	CONDUIT	83.8	0.3019	0.0130
507	506	501	CONDUIT	73.2	0.5725	0.0130
51	51	54	CONDUIT	127.8	0.1017	0.0130
510	511	512	CONDUIT	143.6	0.4235	0.0130
511	512	507	CONDUIT	131.1	0.2815	0.0130
512	513	512	CONDUIT	70.3	0.5245	0.0130
513	514	513	CONDUIT	46.6	0.4890	0.0130
515	516	511	CONDUIT	36.8	0.7285	0.0130
520	521	514	CONDUIT	7.7	0.3896	0.0130
53_1	54	55_1	CONDUIT	78.9	0.0887	0.0130
53_2	55_1	56	CONDUIT	83.9	0.1073	0.0130
551	554	555	CONDUIT	83.5	0.1245	0.0130
552	555	556	CONDUIT	88.1	0.2248	0.0130
558	553	563	CONDUIT	79.5	0.2516	0.0130
560	563	554	CONDUIT	19.2	0.2083	0.0130
60	56	63	CONDUIT	83.0	0.0964	0.0130
61	63	64	CONDUIT	118.2	0.1016	0.0130
62	64	65	CONDUIT	95.0	0.0947	0.0130
63	65_1	66	CONDUIT	3.8	3.4641	0.0130
63_1	65	65_1	CONDUIT	6.2	0.1608	0.0130
64	68	66	CONDUIT	39.7	0.5670	0.0130
646	556	649	CONDUIT	102.4	0.1221	0.0130
647	649	650	CONDUIT	100.7	0.0993	0.0130
649	650	652	CONDUIT	96.5	0.2467	0.0130
650	652	653	CONDUIT	22.4	0.1475	0.0130
651	653	654	CONDUIT	78.8	0.2133	0.0130
663	666	667	CONDUIT	85.5	0.3113	0.0130
664	667	668	CONDUIT	100.0	0.2741	0.0130
665	668	669	CONDUIT	92.3	0.3143	0.0130
666	669	670	CONDUIT	99.1	0.1563	0.0130
667	670	671	CONDUIT	106.0	0.1529	0.0130
668	671	672	CONDUIT	98.3	0.1425	0.0130
669	672	650	CONDUIT	99.1	0.2028	0.0130
670	2105	673	CONDUIT	103.2	0.1095	0.0130
672	673	675	CONDUIT	30.5	0.1375	0.0130
673	675	676	CONDUIT	73.0	0.0917	0.0130
675	2259	678	CONDUIT	79.4	0.1725	0.0130
680	708	682	CONDUIT	125.3	0.2601	0.0130
681	682	684	CONDUIT	64.7	0.4993	0.0130
682	684	678	CONDUIT	64.3	0.2455	0.0130
683	678	685	CONDUIT	74.0	0.1756	0.0130
684	2217	2218	CONDUIT	59.7	0.2680	0.0130
688	686	689	CONDUIT	51.3	0.2144	0.0130
689	2453	690	CONDUIT	44.6	0.1568	0.0130
779	690	780	CONDUIT	62.6	0.1915	0.0130
780	2221	2220	CONDUIT	74.9	0.1735	0.0130
781	781	782	CONDUIT	95.0	0.1685	0.0130
782	782	783	CONDUIT	66.8	0.2397	0.0130
854	796	852	CONDUIT	62.0	1.0809	0.0130
855	852	853	CONDUIT	67.5	0.9904	0.0130
860	853	860	CONDUIT	61.9	1.1051	0.0130
861	860	861	CONDUIT	18.2	1.0611	0.0130
862	861	859	CONDUIT	44.3	1.1119	0.0130
866	859	865	CONDUIT	72.6	1.1286	0.0130
867	865	864	CONDUIT	52.5	1.2244	0.0130
868	864	866	CONDUIT	8.2	1.8814	0.0130
880	866	878	CONDUIT	32.0	0.9773	0.0130
881	878	877	CONDUIT	62.0	1.2842	0.0130
882	877	879	CONDUIT	62.6	0.7833	0.0130
883	879	880	CONDUIT	87.3	0.4741	0.0130
884	880	881	CONDUIT	71.5	0.5313	0.0130
885	881	882	CONDUIT	79.0	0.4402	0.0130
886	2222	2223	CONDUIT	52.9	0.3026	0.0130
887	883	884	CONDUIT	67.2	0.1784	0.0130
888	2224	885	CONDUIT	57.0	0.3511	0.0130
889	885	882	CONDUIT	31.1	0.2575	0.0130
890	882	886	CONDUIT	102.9	0.7757	0.0130
891	886	887	CONDUIT	102.1	0.5918	0.0130
892	887	479	CONDUIT	115.3	0.7924	0.0130
9011	1051	9915	CONDUIT	142.3	1.2373	0.0130
9012	1051	9916	CONDUIT	136.2	1.2927	0.0130
9013	1051	WWTP	CONDUIT	14.9	0.0334	0.0130
9014	2286	9050	CONDUIT	33.6	0.3567	0.0130
9015	9050	9051	CONDUIT	10.0	0.6007	0.0130
9016	9051	9052	CONDUIT	60.8	0.5926	0.0130
9017	9052	9053	CONDUIT	59.8	0.6016	0.0130
9018	9053	9054	CONDUIT	13.9	0.6556	0.0130
9019	9054	9055	CONDUIT	37.9	1.8141	0.0130
9020	9055	9056	CONDUIT	57.5	1.8079	0.0130
9021	9056	9057	CONDUIT	20.5	1.7791	0.0130
9022	9057	9058	CONDUIT	34.7	1.7857	0.0130
9023	9058	9059	CONDUIT	38.1	0.6989	0.0130
9024	9059	9060	CONDUIT	71.3	0.6322	0.0130
9025	9060	9061	CONDUIT	9.6	0.6780	0.0130
9026	9061	1873	CONDUIT	15.8	0.7721	0.0130
9027	1048	1049	CONDUIT	12.7	0.0788	0.0130
9028	1026	Front_St_PS_Overflow_1	CONDUIT	19.1	7.4444	0.0130
9029	9902	1049	CONDUIT	8.5	1.0804	0.0130
932	924	2268	CONDUIT	116.9	1.1124	0.0130
946	924	941	CONDUIT	91.6	1.3075	0.0130
947	941	940	CONDUIT	85.5	3.7698	0.0130
948	940	942	CONDUIT	70.0	2.9477	0.0130
949	942	521	CONDUIT	90.3	0.3876	0.0130
952	945	946	CONDUIT	66.8	0.3052	0.0130
953	946	516	CONDUIT	82.6	0.2590	0.0130
955	948	945	CONDUIT	86.8	1.4789	0.0130
957	950	951	CONDUIT	144.3	0.5961	0.0130
958	951	952	CONDUIT	82.5	0.4001	0.0130
959	952	953	CONDUIT	155.6	0.2506	0.0130
960	953	954	CONDUIT	83.4	0.2038	0.0130
961	954	955	CONDUIT	89.3	0.3582	0.0130
962	955	956	CONDUIT	152.1	0.3615	0.0130
963	956	957	CONDUIT	115.7	0.2679	0.0130
964_1	957	2280	CONDUIT	34.3	0.1982	0.0130
964_2	2280	958	CONDUIT	40.0	0.3802	0.0130
965	958	959	CONDUIT	111.8	0.2506	0.0130
966	959	960	CONDUIT	161.5	0.2539	0.0130
967	960	961	CONDUIT	109.7	0.2370	0.0130
968	961	962	CONDUIT	41.8	0.2869	0.0130
969	962	963	CONDUIT	151.4	0.2907	0.0130
970	963	964	CONDUIT	93.1	0.1718	0.0130
971	964	965	CONDUIT	154.3	0.2593	0.0130
988	985	986	CONDUIT	56.3	0.4085	0.0130
989	986	987	CONDUIT	100.0	0.1999	0.0130
990	987	3000	CONDUIT	49.5	0.1212	0.0130
990_1	3000	3000A	CONDUIT	8.5	0.2360	0.0130
9902	1933	1942	CONDUIT	126.3	0.2374	0.0130
9904	1050_1	905	CONDUIT	518.2	0.0174	0.0130
9905	905	1051	CONDUIT	560.5	0.3006	0.0130
9906_1	902a	902	CONDUIT	52.0	0.0192	0.0130
9906_2	1050_2	902a	CONDUIT	4.9	-12.6461	0.0130
9907	902	1051	CONDUIT	1027.2	0.1065	0.0130
9908	66	Dundas_Street_PS_Overflow_1	CONDUIT	35.8	5.0407	0.0130
9909	1050	1050_2	CONDUIT	1.0	0.1044	0.0130
9910	1050	1050_1	CONDUIT	1.0	0.1014	0.0130
9911	1050	9914	CONDUIT	12.3	28.2155	0.0130
9912	2282_2	Dundas_Street_Outfall	CONDUIT	23.1	3.4897	0.0130
9914	138	67	CONDUIT	562.9	0.4763	0.0130
9915	EastFM_1	9915	CONDUIT	2.7	101.5167	0.0130
9916	EastFM_2	9916	CONDUIT	3.0	83.3853	0.0130
992_1	3000A	988	CONDUIT	69.4	0.2161	0.0130
992_2	988	991	CONDUIT	47.1	0.0722	0.0130
998	991	996	CONDUIT	91.3	0.4052	0.0130
999	996	997	CONDUIT	87.4	0.3661	0.0130
Dundas_1	66	67	TYPE3 PUMP			
Dundas_2	66	67	TYPE3 PUMP			
Dundas_3	66	67	TYPE3 PUMP			
East_PS_1	1942	EastFM_1	TYPE4 PUMP			
East_PS_2	1942	EastFM_1	TYPE4 PUMP			
East_PS_3	1942	EastFM_2	TYPE3 PUMP			
East_PS_4	1942	EastFM_2	TYPE3 PUMP			
FrontSt#1	1049	1050_1	TYPE3 PUMP			
FrontSt#2	1049	1050_2	TYPE3 PUMP			
FrontSt#3	1049	1050_1	TYPE3 PUMP			
FrontSt#4	1049	1050	TYPE3 PUMP			
2282_c	2282	2282_2	ORIFICE			
9913	2282	2282_1	ORIFICE			
3339_1	2340	2340_2	WEIR			
3339_4	2340	2340_1	WEIR			

****
Cross Section Summary
****

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow
1001	CIRCULAR	0.53	0.22	0.13	0.53	1	0.28
1009	CIRCULAR	0.50	0.20	0.12	0.50	1	0.23
1010	CIRCULAR	0.50	0.20	0.12	0.50	1	0.20
1011	CIRCULAR	0.53	0.22	0.13	0.53	1	0.15
1023	CIRCULAR	0.50	0.20	0.12	0.50	1	0.30
1025	CIRCULAR	0.50	0.20	0.12	0.50	1	0.18
1026	CIRCULAR	0.50	0.20	0.12	0.50	1	0.24
1027	CIRCULAR	0.50	0.20	0.12	0.50	1	0.26
1028	CIRCULAR	0.50	0.20	0.12	0.50	1	0.26
1029	CIRCULAR	0.60	0.28	0.15	0.60	1	0.61
103	CIRCULAR	0.38	0.11	0.09	0.38	1	0.04
1030	CIRCULAR	0.60	0.28	0.15	0.60	1	0.87
1032	CIRCULAR	0.53	0.22	0.13	0.53	1	0.45
1033	CIRCULAR	0.53	0.22	0.13	0.53	1	0.30
104	CIRCULAR	0.38	0.11	0.09	0.38	1	0.10
1045	CIRCULAR	0.53	0.22	0.13	0.53	1	0.41
1046	CIRCULAR	0.45	0.16	0.11	0.45	1	0.34
1048	CIRCULAR	0.45	0.16	0.11	0.45	1	0.35
1050	CIRCULAR	1.05	0.87	0.26	1.05	1	1.15
1052	CIRCULAR	0.60	0.28	0.15	0.60	1	0.38
1054_1	CIRCULAR	1.50	1.77	0.38	1.50	1	2.21
1054_2	CIRCULAR	1.50	1.77	0.38	1.50	1	2.28
109	CIRCULAR	0.38	0.11	0.09	0.38	1	0.16
1090	CIRCULAR	0.60	0.28	0.15	0.60	1	0.39
1091	CIRCULAR	0.60	0.28	0.15	0.60	1	0.24
1092	CIRCULAR	0.60	0.28	0.15	0.60	1	0.16
1093	CIRCULAR	0.60	0.28	0.15	0.60	1	0.15
1096	CIRCULAR	0.60	0.28	0.15	0.60	1	0.32
1103	CIRCULAR	0.60	0.28	0.15	0.60	1	0.18
1116	CIRCULAR	0.60	0.28	0.15	0.60	1	0.49
1117	CIRCULAR	0.60	0.28	0.15	0.60	1	0.40
1118	CIRCULAR	0.60	0.28	0.15	0.60	1	0.21
1119	CIRCULAR	0.60	0.28	0.15	0.60	1	0.66
1120	CIRCULAR	0.60	0.28	0.15	0.60	1	0.22
1179	CIRCULAR	1.05	0.87	0.26	1.05	1	2.12
1180	CIRCULAR	1.05	0.87	0.26	1.05	1	0.97
1181	CIRCULAR	1.05	0.87	0.26	1.05	1	1.42
1182	CIRCULAR	1.05	0.87	0.26	1.05	1	1.66
1183	CIRCULAR	1.05	0.87	0.26	1.05	1	1.91
1184	CIRCULAR	1.05	0.87	0.26	1.05	1	1.47
1185	CIRCULAR	1.05	0.87	0.26	1.05	1	1.40
1186	CIRCULAR	1.05	0.87	0.26	1.05	1	1.46
1189	CIRCULAR	0.75	0.44	0.19	0.75	1	0.63
1190	CIRCULAR	0.75	0.44	0.19	0.75	1	0.62
1193	CIRCULAR	0.75	0.44	0.19	0.75	1	0.55

1194	CIRCULAR	0.75	0.44	0.19	0.75	1	0.61
1195	CIRCULAR	0.75	0.44	0.19	0.75	1	0.54
1196	CIRCULAR	0.68	0.36	0.17	0.68	1	0.61
1198	CIRCULAR	0.68	0.36	0.17	0.68	1	0.50
1199	CIRCULAR	0.68	0.36	0.17	0.68	1	0.56
1202	CIRCULAR	0.68	0.36	0.17	0.68	1	0.74
1203	CIRCULAR	0.68	0.36	0.17	0.68	1	0.71
1206	CIRCULAR	0.68	0.36	0.17	0.68	1	0.47
1207	CIRCULAR	0.68	0.36	0.17	0.68	1	0.59
1208	CIRCULAR	0.68	0.36	0.17	0.68	1	0.54
1209	CIRCULAR	0.68	0.36	0.17	0.68	1	0.52
1210	CIRCULAR	0.68	0.36	0.17	0.68	1	0.56
1212	CIRCULAR	0.68	0.36	0.17	0.68	1	0.57
1213	CIRCULAR	0.68	0.36	0.17	0.68	1	0.26
1214	CIRCULAR	0.68	0.36	0.17	0.68	1	0.51
1215	CIRCULAR	0.68	0.36	0.17	0.68	1	0.61
1216	CIRCULAR	0.68	0.36	0.17	0.68	1	0.47
1220	CIRCULAR	0.30	0.07	0.07	0.30	1	0.08
1221	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
1222	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
1223	CIRCULAR	0.38	0.11	0.09	0.38	1	0.10
1224	CIRCULAR	0.38	0.11	0.09	0.38	1	0.11
1225	CIRCULAR	0.38	0.11	0.09	0.38	1	0.11
1226	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
1245	CIRCULAR	0.35	0.10	0.09	0.35	1	0.09
1246	CIRCULAR	0.35	0.10	0.09	0.35	1	0.11
1247	CIRCULAR	0.35	0.10	0.09	0.35	1	0.08
1248	CIRCULAR	0.35	0.10	0.09	0.35	1	0.09
1249	CIRCULAR	0.35	0.10	0.09	0.35	1	0.09
1250	CIRCULAR	0.35	0.10	0.09	0.35	1	0.10
1251	CIRCULAR	0.35	0.10	0.09	0.35	1	0.09
1252	CIRCULAR	0.35	0.10	0.09	0.35	1	0.08
1255	CIRCULAR	0.35	0.10	0.09	0.35	1	0.09
1256	CIRCULAR	0.35	0.10	0.09	0.35	1	0.10
1290	CIRCULAR	0.40	0.13	0.10	0.40	1	0.13
1291	CIRCULAR	0.40	0.13	0.10	0.40	1	0.11
1292	CIRCULAR	0.40	0.13	0.10	0.40	1	0.13
1293	CIRCULAR	0.40	0.13	0.10	0.40	1	0.12
1294	CIRCULAR	0.40	0.13	0.10	0.40	1	0.12
1295	CIRCULAR	0.40	0.13	0.10	0.40	1	0.20
1296	CIRCULAR	0.82	0.53	0.21	0.82	1	0.81
1297	CIRCULAR	0.82	0.53	0.21	0.82	1	0.84
1298	CIRCULAR	0.82	0.53	0.21	0.82	1	0.93
1299	CIRCULAR	0.82	0.53	0.21	0.82	1	0.87
1300	CIRCULAR	0.82	0.53	0.21	0.82	1	0.81
1301	CIRCULAR	0.82	0.53	0.21	0.82	1	0.82
1302	CIRCULAR	0.82	0.53	0.21	0.82	1	0.94
1303	CIRCULAR	0.82	0.53	0.21	0.82	1	0.84
1308	CIRCULAR	0.82	0.53	0.21	0.82	1	0.85
1311	CIRCULAR	0.82	0.53	0.21	0.82	1	0.91
1312	CIRCULAR	0.82	0.53	0.21	0.82	1	0.89
1313	CIRCULAR	0.82	0.53	0.21	0.82	1	0.87
1314	CIRCULAR	0.82	0.53	0.21	0.82	1	1.36
1315	CIRCULAR	0.82	0.53	0.21	0.82	1	0.89
1316	CIRCULAR	0.82	0.53	0.21	0.82	1	1.00
132	CIRCULAR	0.38	0.11	0.09	0.38	1	0.20
133	CIRCULAR	0.38	0.11	0.09	0.38	1	0.10
134	CIRCULAR	0.38	0.11	0.09	0.38	1	0.12
1348	CIRCULAR	0.40	0.13	0.10	0.40	1	0.15
1349	CIRCULAR	0.40	0.13	0.10	0.40	1	0.13
1350	CIRCULAR	0.40	0.13	0.10	0.40	1	0.11
1351	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
154	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
155	CIRCULAR	0.30	0.07	0.07	0.30	1	0.13
156	CIRCULAR	0.45	0.16	0.11	0.45	1	0.34
158	CIRCULAR	0.25	0.05	0.06	0.25	1	0.07
159	CIRCULAR	0.30	0.07	0.07	0.30	1	0.19
160	CIRCULAR	0.30	0.07	0.07	0.30	1	0.08
161	CIRCULAR	0.30	0.07	0.07	0.30	1	0.18
162	CIRCULAR	0.25	0.05	0.06	0.25	1	0.07
163	CIRCULAR	0.25	0.05	0.06	0.25	1	0.08
164	CIRCULAR	0.25	0.05	0.06	0.25	1	0.07
165	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
166	CIRCULAR	0.30	0.07	0.07	0.30	1	0.08
167	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
168	CIRCULAR	0.30	0.07	0.07	0.30	1	0.16
169	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
170	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
1703	CIRCULAR	0.30	0.07	0.07	0.30	1	0.04
171	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
1716	CIRCULAR	0.25	0.05	0.06	0.25	1	0.05
1717	CIRCULAR	0.25	0.05	0.06	0.25	1	0.04
1718	CIRCULAR	0.25	0.05	0.06	0.25	1	0.05
1719	CIRCULAR	0.25	0.05	0.06	0.25	1	0.04
172	CIRCULAR	0.30	0.07	0.07	0.30	1	0.12
1742	CIRCULAR	0.25	0.05	0.06	0.25	1	0.04
1743	CIRCULAR	0.25	0.05	0.06	0.25	1	0.05
1745	CIRCULAR	0.25	0.05	0.06	0.25	1	0.03
1746	CIRCULAR	0.25	0.05	0.06	0.25	1	0.01
1747	CIRCULAR	0.60	0.28	0.15	0.60	1	0.54
1748	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
1749	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
1750	CIRCULAR	0.60	0.28	0.15	0.60	1	0.41
1751	CIRCULAR	0.60	0.28	0.15	0.60	1	0.25
1752	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
1755	CIRCULAR	0.30	0.07	0.07	0.30	1	0.04
1756	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
1757	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
1759	CIRCULAR	0.30	0.07	0.07	0.30	1	0.04
1760	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
1761	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
1766	CIRCULAR	0.25	0.05	0.06	0.25	1	0.03
1772	CIRCULAR	0.25	0.05	0.06	0.25	1	0.01
1773	CIRCULAR	0.30	0.07	0.07	0.30	1	0.10
1774	CIRCULAR	0.20	0.03	0.05	0.20	1	0.07
1775	CIRCULAR	0.20	0.03	0.05	0.20	1	0.04
1776	CIRCULAR	0.60	0.28	0.15	0.60	1	0.67
1777	CIRCULAR	0.60	0.28	0.15	0.60	1	0.74
1778	CIRCULAR	0.60	0.28	0.15	0.60	1	0.74
1779	CIRCULAR	0.60	0.28	0.15	0.60	1	1.19
1802	CIRCULAR	0.60	0.28	0.15	0.60	1	0.65
1803	CIRCULAR	0.60	0.28	0.15	0.60	1	0.27
1804	CIRCULAR	0.60	0.28	0.15	0.60	1	0.21
1805	CIRCULAR	0.60	0.28	0.15	0.60	1	0.15
1806	CIRCULAR	0.90	0.64	0.23	0.90	1	0.72
1807	CIRCULAR	0.90	0.64	0.23	0.90	1	0.66
1808	CIRCULAR	0.90	0.64	0.23	0.90	1	0.56
1809	CIRCULAR	0.90	0.64	0.23	0.90	1	0.66
1821	CIRCULAR	0.90	0.64	0.23	0.90	1	0.42
1877	CIRCULAR	0.90	0.64	0.23	0.90	1	0.37
1878	CIRCULAR	0.90	0.64	0.23	0.90	1	0.64
1879	CIRCULAR	0.90	0.64	0.23	0.90	1	0.29
1880	CIRCULAR	0.90	0.64	0.23	0.90	1	0.91
1881	CIRCULAR	0.90	0.64	0.23	0.90	1	0.57
1882	CIRCULAR	0.90	0.64	0.23	0.90	1	0.48
1883	CIRCULAR	0.90	0.64	0.23	0.90	1	0.54
1884	CIRCULAR	0.90	0.64	0.23	0.90	1	0.69
1885	CIRCULAR	0.90	0.64	0.23	0.90	1	0.74
1886	CIRCULAR	0.90	0.64	0.23	0.90	1	0.51
1887	CIRCULAR	0.90	0.64	0.23	0.90	1	0.75
1888	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
1891	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
1893	CIRCULAR	0.53	0.22	0.13	0.53	1	0.15
1905	CIRCULAR	0.53	0.22	0.13	0.53	1	0.17
1912	CIRCULAR	0.30	0.07	0.07	0.30	1	0.04
1925	CIRCULAR	0.30	0.07	0.07	0.30	1	0.09
1926	CIRCULAR	0.38	0.11	0.09	0.38	1	0.08
1927	CIRCULAR	0.38	0.11	0.09	0.38	1	0.11
1929	CIRCULAR	0.38	0.11	0.09	0.38	1	0.14
1931	CIRCULAR	0.38	0.11	0.09	0.38	1	0.15
1933	CIRCULAR	0.45	0.16	0.11	0.45	1	0.51
1934	CIRCULAR	0.38	0.11	0.09	0.38	1	0.20
1935	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
1946	CIRCULAR	0.38	0.11	0.09	0.38	1	0.05
1947	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
1948	CIRCULAR	0.45	0.16	0.11	0.45	1	0.15
1949	CIRCULAR	0.45	0.16	0.11	0.45	1	0.41
1950	CIRCULAR	0.45	0.16	0.11	0.45	1	0.46
1951	CIRCULAR	0.45	0.16	0.11	0.45	1	0.39
1956	CIRCULAR	0.90	0.64	0.23	0.90	1	0.65
1957	CIRCULAR	0.87	0.60	0.22	0.87	1	0.70
1958	CIRCULAR	0.90	0.64	0.23	0.90	1	0.57
1959	CIRCULAR	0.90	0.64	0.23	0.90	1	0.62
1960	CIRCULAR	0.90	0.64	0.23	0.90	1	0.64
1977	CIRCULAR	0.45	0.16	0.11	0.45	1	0.06
1978	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
1979	CIRCULAR	0.45	0.16	0.11	0.45	1	0.08
1980	CIRCULAR	0.45	0.16	0.11	0.45	1	0.19
2015	CIRCULAR	0.53	0.22	0.13	0.53	1	0.12
2016	CIRCULAR	0.53	0.22	0.13	0.53	1	0.14
2017	CIRCULAR	0.53	0.22	0.13	0.53	1	0.11
2018	CIRCULAR	0.53	0.22	0.13	0.53	1	0.14
2019	CIRCULAR	0.53	0.22	0.13	0.53	1	0.11
2020	CIRCULAR	0.53	0.22	0.13	0.53	1	0.20
2021	CIRCULAR	0.45	0.16	0.11	0.45	1	0.10
2029	CIRCULAR	0.45	0.16	0.11	0.45	1	0.07
2048	CIRCULAR	0.25	0.05	0.06	0.25	1	0.07
2049	CIRCULAR	0.38	0.11	0.09	0.38	1	0.54
2056	CIRCULAR	0.90	0.64	0.23	0.90	1	2.77
208	CIRCULAR	0.23	0.04	0.06	0.23	1	0.05
2082	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
2083	CIRCULAR	0.45	0.16	0.11	0.45	1	0.12
2084	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
2085	CIRCULAR	0.45	0.16	0.11	0.45	1	0.21
2086	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
2087	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
209	CIRCULAR	0.23	0.04	0.06	0.23	1	0.03
2099	CIRCULAR	0.60	0.28	0.15	0.60	1	0.23
210	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
2135	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
2135_1	CIRCULAR	0.60	0.28	0.15	0.60	1	0.20
2135_2	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
2135_3	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
2135_4	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
2136	CIRCULAR	0.53	0.22	0.13	0.53	1	0.57
2137	CIRCULAR	0.53	0.22	0.13	0.53	1	0.42
2138	CIRCULAR	0.53	0.22	0.13	0.53	1	0.32
2140	CIRCULAR	0.45	0.16	0.11	0.45	1	0.25
2144	CIRCULAR	0.68	0.36	0.17	0.68	1	0.48
2145	CIRCULAR	0.68	0.36	0.17	0.68	1	0.52
2146	CIRCULAR	0.68	0.36	0.17	0.68	1	0.53
2147	CIRCULAR	1.50	1.77	0.38	1.50	1	5.04
2149	CIRCULAR	1.50	1.77	0.38	1.50	1	2.20
2152	CIRCULAR	0.30	0.07	0.07	0.30	1	0.09
2153	CIRCULAR	0.38	0.11	0.09	0.38	1	0.13
216	CIRCULAR	0.40	0.13	0.10	0.40	1	0.11
2175	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
2176	CIRCULAR	0.60	0.28	0.15	0.60	1	0.31
2177	CIRCULAR	0.60	0.28	0.15	0.60	1	0.16
2178	CIRCULAR	0.53	0.22	0.13	0.53	1	0.13
2179	CIRCULAR	0.38	0.11	0.09	0.38	1	0.07
2180	CIRCULAR	0.38	0.11	0.09	0.38	1	0.07
2181	CIRCULAR	0.60	0.28	0.15	0.60	1	0.17
219	CIRCULAR	0.40	0.13	0.10	0.40	1	0.12
2219	CIRCULAR	0.60	0.28	0.15	0.60	1	0.20
2220	CIRCULAR	0.60	0.28	0.15	0.60	1	0.21
2221	CIRCULAR	0.60	0.28	0.15	0.60	1	0.24
2222	CIRCULAR	0.60	0.28	0.15	0.60	1	0.29
2223	CIRCULAR	0.60	0.28	0.15	0.60	1	0.85
2224	CIRCULAR	0.60	0.28	0.15	0.60	1	0.25
2225	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
2226	CIRCULAR	0.60	0.28	0.15	0.60	1	0.16

2264	CIRCULAR	0.60	0.28	0.15	0.60	1	0.25
2269	CIRCULAR	0.25	0.05	0.06	0.25	1	0.10
2270	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
2271	CIRCULAR	0.45	0.16	0.11	0.45	1	0.26
2272	CIRCULAR	0.45	0.16	0.11	0.45	1	0.35
2273	CIRCULAR	0.25	0.05	0.06	0.25	1	0.39
2274	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
2277	CIRCULAR	0.45	0.16	0.11	0.45	1	0.51
2278	CIRCULAR	0.45	0.16	0.11	0.45	1	0.40
2279	CIRCULAR	0.45	0.16	0.11	0.45	1	0.27
2280	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
2281	CIRCULAR	0.40	0.13	0.10	0.40	1	0.12
2282	CIRCULAR	0.40	0.13	0.10	0.40	1	0.12
2283	CIRCULAR	0.40	0.13	0.10	0.40	1	0.14
2284	CIRCULAR	0.40	0.13	0.10	0.40	1	0.09
2285	CIRCULAR	0.40	0.13	0.10	0.40	1	0.21
2286	CIRCULAR	0.40	0.13	0.10	0.40	1	0.15
2287	CIRCULAR	0.40	0.13	0.10	0.40	1	0.15
2288	CIRCULAR	0.40	0.13	0.10	0.40	1	0.16
2289	CIRCULAR	0.40	0.13	0.10	0.40	1	0.48
229	CIRCULAR	0.45	0.16	0.11	0.45	1	0.17
2291	CIRCULAR	0.90	0.64	0.23	0.90	1	1.03
2292	CIRCULAR	0.75	0.44	0.19	0.75	1	0.47
2339	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
2340	CIRCULAR	0.53	0.22	0.13	0.53	1	0.31
235	CIRCULAR	0.38	0.11	0.09	0.38	1	0.17
2390_1	FORCE_MAIN	0.45	0.16	0.11	0.45	1	0.90
2390_2	FORCE_MAIN	0.45	0.16	0.11	0.45	1	1.84
2390_3	FORCE_MAIN	0.45	0.16	0.11	0.45	1	0.10
2390_5	FORCE_MAIN	0.45	0.16	0.11	0.45	1	0.21
273	CIRCULAR	0.45	0.16	0.11	0.45	1	0.44
274	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
275	CIRCULAR	0.53	0.22	0.13	0.53	1	0.27
276	CIRCULAR	0.53	0.22	0.13	0.53	1	0.36
277	CIRCULAR	0.60	0.28	0.15	0.60	1	0.24
278	CIRCULAR	0.60	0.28	0.15	0.60	1	0.18
283	CIRCULAR	0.60	0.28	0.15	0.60	1	0.33
289	CIRCULAR	0.38	0.11	0.09	0.38	1	0.13
290	CIRCULAR	0.38	0.11	0.09	0.38	1	0.14
291	CIRCULAR	0.38	0.11	0.09	0.38	1	0.13
292	CIRCULAR	0.38	0.11	0.09	0.38	1	0.13
3300	CIRCULAR	0.68	0.36	0.17	0.68	1	0.58
3301	CIRCULAR	0.68	0.36	0.17	0.68	1	0.51
3302	CIRCULAR	0.68	0.36	0.17	0.68	1	0.59
3303	CIRCULAR	0.68	0.36	0.17	0.68	1	0.50
3304	CIRCULAR	0.68	0.36	0.17	0.68	1	0.45
3305	CIRCULAR	0.68	0.36	0.17	0.68	1	0.51
3306	CIRCULAR	0.68	0.36	0.17	0.68	1	0.52
3307	CIRCULAR	0.68	0.36	0.17	0.68	1	0.48
3309	CIRCULAR	0.68	0.36	0.17	0.68	1	0.48
3310	CIRCULAR	0.68	0.36	0.17	0.68	1	0.50
3311	CIRCULAR	0.68	0.36	0.17	0.68	1	0.53
3312	CIRCULAR	0.68	0.36	0.17	0.68	1	0.78
3313	CIRCULAR	0.45	0.16	0.11	0.45	1	0.20
3314	CIRCULAR	0.45	0.16	0.11	0.45	1	0.22
3315	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
3317	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
3318	CIRCULAR	0.45	0.16	0.11	0.45	1	0.39
3319	CIRCULAR	0.45	0.16	0.11	0.45	1	0.20
3320	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
3321	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
3339_10	CIRCULAR	0.25	0.05	0.06	0.25	1	0.24
3339_11	CIRCULAR	0.45	0.16	0.11	0.45	1	1.02
3339_12	CIRCULAR	0.25	0.05	0.06	0.25	1	0.20
3339_2	CIRCULAR	0.25	0.05	0.06	0.25	1	0.02
3339_3	CIRCULAR	0.25	0.05	0.06	0.25	1	0.24
3339_5	CIRCULAR	0.25	0.05	0.06	0.25	1	0.18
3339_6	CIRCULAR	0.45	0.16	0.11	0.45	1	1.14
3339_8	CIRCULAR	0.25	0.05	0.06	0.25	1	0.02
3339_9	CIRCULAR	0.45	0.16	0.11	0.45	1	0.08
3340	CIRCULAR	0.60	0.28	0.15	0.60	1	0.29
3341	CIRCULAR	0.60	0.28	0.15	0.60	1	0.29
3342	CIRCULAR	0.60	0.28	0.15	0.60	1	0.27
3343	CIRCULAR	0.60	0.28	0.15	0.60	1	0.27
3344	CIRCULAR	0.60	0.28	0.15	0.60	1	0.26
3345	CIRCULAR	0.60	0.28	0.15	0.60	1	0.30
3346	CIRCULAR	0.60	0.28	0.15	0.60	1	0.37
3347	CIRCULAR	0.60	0.28	0.15	0.60	1	0.30
3348	CIRCULAR	0.60	0.28	0.15	0.60	1	0.51
3364	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3365	CIRCULAR	0.53	0.22	0.13	0.53	1	0.29
3366	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3367	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3368	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3369	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3370	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3371	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3372	CIRCULAR	0.53	0.22	0.13	0.53	1	0.29
3373	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3374	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3375	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3376	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3377	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3378	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3379	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3380	CIRCULAR	0.53	0.22	0.13	0.53	1	0.22
3381	CIRCULAR	0.53	0.22	0.13	0.53	1	0.20
3382	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3383	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3384	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3385	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3386	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
3387	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14
3388	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14
3389	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14
3390	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14

3391	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14
3392	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14
3393	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
3394	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
3395	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
3396	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
3398	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
3399	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
3400	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
3401	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
3402	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
3403	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
3500	CIRCULAR	0.60	0.28	0.15	0.60	1	0.25
3502	CIRCULAR	0.53	0.22	0.13	0.53	1	0.25
3503	CIRCULAR	0.53	0.22	0.13	0.53	1	0.24
3504	CIRCULAR	0.53	0.22	0.13	0.53	1	0.23
3505	CIRCULAR	0.53	0.22	0.13	0.53	1	0.14
3690	CIRCULAR	0.60	0.28	0.15	0.60	1	0.24
39	CIRCULAR	0.60	0.28	0.15	0.60	1	0.20
391	CIRCULAR	0.60	0.28	0.15	0.60	1	0.26
392	CIRCULAR	0.60	0.28	0.15	0.60	1	0.33
393	CIRCULAR	0.60	0.28	0.15	0.60	1	0.32
394	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
395	CIRCULAR	0.60	0.28	0.15	0.60	1	0.37
396	CIRCULAR	0.60	0.28	0.15	0.60	1	0.37
400	CIRCULAR	0.90	0.64	0.23	0.90	1	1.46
401	CIRCULAR	0.90	0.64	0.23	0.90	1	1.21
403	CIRCULAR	0.45	0.16	0.11	0.45	1	0.23
4035	CIRCULAR	0.53	0.22	0.13	0.53	1	0.14
4036	CIRCULAR	0.53	0.22	0.13	0.53	1	0.13
4037	CIRCULAR	0.53	0.22	0.13	0.53	1	0.32
4038	CIRCULAR	0.38	0.11	0.09	0.38	1	0.13
408	CIRCULAR	0.90	0.64	0.23	0.90	1	1.39
412	CIRCULAR	0.50	0.20	0.12	0.50	1	0.35
413	CIRCULAR	0.50	0.20	0.12	0.50	1	0.29
414	CIRCULAR	0.50	0.20	0.12	0.50	1	0.08
415	CIRCULAR	0.50	0.20	0.12	0.50	1	0.41
417	CIRCULAR	0.50	0.20	0.12	0.50	1	0.21
418	CIRCULAR	0.53	0.22	0.13	0.53	1	0.34
419	CIRCULAR	0.53	0.22	0.13	0.53	1	0.31
420	CIRCULAR	0.53	0.22	0.13	0.53	1	0.42
421	CIRCULAR	0.53	0.22	0.13	0.53	1	0.46
422	CIRCULAR	0.25	0.05	0.06	0.25	1	0.05
423	CIRCULAR	0.38	0.11	0.09	0.38	1	0.32
424	CIRCULAR	0.38	0.11	0.09	0.38	1	0.30
425	CIRCULAR	0.38	0.11	0.09	0.38	1	0.26
426	CIRCULAR	0.45	0.16	0.11	0.45	1	0.49
427	CIRCULAR	0.90	0.64	0.23	0.90	1	0.61
428	CIRCULAR	0.90	0.64	0.23	0.90	1	1.26
429	CIRCULAR	0.45	0.16	0.11	0.45	1	0.27
436	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
437	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
438	CIRCULAR	0.90	0.64	0.23	0.90	1	1.00
439	CIRCULAR	0.90	0.64	0.23	0.90	1	0.90
442	CIRCULAR	0.23	0.04	0.06	0.23	1	0.06
443	CIRCULAR	0.53	0.22	0.13	0.53	1	0.30
444	CIRCULAR	0.53	0.22	0.13	0.53	1	0.14
445	CIRCULAR	0.23	0.04	0.06	0.23	1	0.01
446	CIRCULAR	0.50	0.20	0.12	0.50	1	0.25
447	CIRCULAR	0.50	0.20	0.12	0.50	1	0.29
448	CIRCULAR	0.25	0.05	0.06	0.25	1	0.08
449	CIRCULAR	0.23	0.04	0.06	0.23	1	0.02
45	CIRCULAR	0.75	0.44	0.19	0.75	1	0.35
450	CIRCULAR	0.23	0.04	0.06	0.23	1	0.04
451	CIRCULAR	0.25	0.05	0.06	0.25	1	0.12
452	CIRCULAR	0.75	0.44	0.19	0.75	1	0.84
453	CIRCULAR	0.40	0.13	0.10	0.40	1	0.09
454	CIRCULAR	0.90	0.64	0.23	0.90	1	1.89
455	CIRCULAR	0.25	0.05	0.06	0.25	1	0.03
456	CIRCULAR	0.25	0.05	0.06	0.25	1	0.04
457	CIRCULAR	0.35	0.10	0.09	0.35	1	0.09
458	CIRCULAR	0.45	0.16	0.11	0.45	1	0.19
459	CIRCULAR	0.53	0.22	0.13	0.53	1	0.24
460	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
461	CIRCULAR	0.45	0.16	0.11	0.45	1	0.17
465	CIRCULAR	0.75	0.44	0.19	0.75	1	1.11
468	CIRCULAR	0.75	0.44	0.19	0.75	1	0.62
469	CIRCULAR	0.75	0.44	0.19	0.75	1	0.42
474	CIRCULAR	0.75	0.44	0.19	0.75	1	0.70
475	CIRCULAR	0.75	0.44	0.19	0.75	1	1.20
476	CIRCULAR	0.60	0.28	0.15	0.60	1	0.54
477	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
478	CIRCULAR	0.75	0.44	0.19	0.75	1	0.71
499	CIRCULAR	0.45	0.16	0.11	0.45	1	0.12
500	CIRCULAR	0.45	0.16	0.11	0.45	1	0.14
502	CIRCULAR	0.45	0.16	0.11	0.45	1	0.33
505	CIRCULAR	0.38	0.11	0.09	0.38	1	0.10
5050	CIRCULAR	0.53	0.22	0.13	0.53	1	0.42
506	CIRCULAR	0.38	0.11	0.09	0.38	1	0.10
507	CIRCULAR	0.45	0.16	0.11	0.45	1	0.22
51	CIRCULAR	0.75	0.44	0.19	0.75	1	0.36
510	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
511	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
512	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
513	CIRCULAR	0.30	0.07	0.07	0.30	1	0.07
515	CIRCULAR	0.25	0.05	0.06	0.25	1	0.05
520	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
53_1	CIRCULAR	0.75	0.44	0.19	0.75	1	0.33
53_2	CIRCULAR	0.75	0.44	0.19	0.75	1	0.36
551	CIRCULAR	0.60	0.28	0.15	0.60	1	0.22
552	CIRCULAR	0.60	0.28	0.15	0.60	1	0.29
558	CIRCULAR	0.60	0.28	0.15	0.60	1	0.31
560	CIRCULAR	0.60	0.28	0.15	0.60	1	0.28
60	CIRCULAR	0.75	0.44	0.19	0.75	1	0.35
61	CIRCULAR	0.75	0.44	0.19	0.75	1	0.35
62	CIRCULAR	0.75	0.44	0.19	0.75	1	0.34

63	CIRCULAR	0.75	0.44	0.19	0.75	1	2.07
63_1	CIRCULAR	0.75	0.44	0.19	0.75	1	0.45
64	CIRCULAR	0.38	0.11	0.09	0.38	1	0.13
646	CIRCULAR	0.60	0.28	0.15	0.60	1	0.21
647	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
649	CIRCULAR	0.60	0.28	0.15	0.60	1	0.31
650	CIRCULAR	0.60	0.28	0.15	0.60	1	0.24
651	CIRCULAR	0.60	0.28	0.15	0.60	1	0.28
663	CIRCULAR	0.30	0.07	0.07	0.30	1	0.05
664	CIRCULAR	0.38	0.11	0.09	0.38	1	0.09
665	CIRCULAR	0.38	0.11	0.09	0.38	1	0.10
666	CIRCULAR	0.45	0.16	0.11	0.45	1	0.11
667	CIRCULAR	0.45	0.16	0.11	0.45	1	0.11
668	CIRCULAR	0.45	0.16	0.11	0.45	1	0.11
669	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
670	CIRCULAR	0.60	0.28	0.15	0.60	1	0.20
672	CIRCULAR	0.60	0.28	0.15	0.60	1	0.23
673	CIRCULAR	0.60	0.28	0.15	0.60	1	0.19
675	CIRCULAR	0.60	0.28	0.15	0.60	1	0.26
680	CIRCULAR	0.40	0.13	0.10	0.40	1	0.11
681	CIRCULAR	0.40	0.13	0.10	0.40	1	0.15
682	CIRCULAR	0.40	0.13	0.10	0.40	1	0.10
683	CIRCULAR	0.60	0.28	0.15	0.60	1	0.26
684	CIRCULAR	0.60	0.28	0.15	0.60	1	0.32
688	CIRCULAR	0.60	0.28	0.15	0.60	1	0.28
689	CIRCULAR	0.60	0.28	0.15	0.60	1	0.24
779	CIRCULAR	0.60	0.28	0.15	0.60	1	0.27
780	CIRCULAR	0.60	0.28	0.15	0.60	1	0.26
781	CIRCULAR	0.60	0.28	0.15	0.60	1	0.25
782	CIRCULAR	0.60	0.28	0.15	0.60	1	0.30
854	CIRCULAR	0.35	0.10	0.09	0.35	1	0.15
855	CIRCULAR	0.35	0.10	0.09	0.35	1	0.15
860	CIRCULAR	0.35	0.10	0.09	0.35	1	0.15
861	CIRCULAR	0.35	0.10	0.09	0.35	1	0.15
862	CIRCULAR	0.35	0.10	0.09	0.35	1	0.15
866	CIRCULAR	0.35	0.10	0.09	0.35	1	0.15
867	CIRCULAR	0.35	0.10	0.09	0.35	1	0.16
868	CIRCULAR	0.40	0.13	0.10	0.40	1	0.29
880	CIRCULAR	0.40	0.13	0.10	0.40	1	0.21
881	CIRCULAR	0.45	0.16	0.11	0.45	1	0.32
882	CIRCULAR	0.45	0.16	0.11	0.45	1	0.25
883	CIRCULAR	0.45	0.16	0.11	0.45	1	0.20
884	CIRCULAR	0.45	0.16	0.11	0.45	1	0.21
885	CIRCULAR	0.45	0.16	0.11	0.45	1	0.19
886	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
887	CIRCULAR	0.60	0.28	0.15	0.60	1	0.26
888	CIRCULAR	0.60	0.28	0.15	0.60	1	0.36
889	CIRCULAR	0.60	0.28	0.15	0.60	1	0.31
890	CIRCULAR	0.60	0.28	0.15	0.60	1	0.54
891	CIRCULAR	0.60	0.28	0.15	0.60	1	0.47
892	CIRCULAR	0.60	0.28	0.15	0.60	1	0.55
9011	FORCE_MAIN	0.45	0.16	0.11	0.45	1	0.40
9012	FORCE_MAIN	0.45	0.16	0.11	0.45	1	0.41
9013	CIRCULAR	1.00	0.79	0.25	1.00	1	0.44
9014	CIRCULAR	0.53	0.22	0.13	0.53	1	0.26
9015	CIRCULAR	0.53	0.22	0.13	0.53	1	0.33
9016	CIRCULAR	0.53	0.22	0.13	0.53	1	0.33
9017	CIRCULAR	0.53	0.22	0.13	0.53	1	0.33
9018	CIRCULAR	0.53	0.22	0.13	0.53	1	0.35
9019	CIRCULAR	0.53	0.22	0.13	0.53	1	0.58
9020	CIRCULAR	0.53	0.22	0.13	0.53	1	0.58
9021	CIRCULAR	0.53	0.22	0.13	0.53	1	0.57
9022	CIRCULAR	0.53	0.22	0.13	0.53	1	0.57
9023	CIRCULAR	0.60	0.28	0.15	0.60	1	0.51
9024	CIRCULAR	0.60	0.28	0.15	0.60	1	0.49
9025	CIRCULAR	0.60	0.28	0.15	0.60	1	0.51
9026	CIRCULAR	0.60	0.28	0.15	0.60	1	0.54
9027	CIRCULAR	1.05	0.87	0.26	1.05	1	0.77
9028	CIRCULAR	0.60	0.28	0.15	0.60	1	1.68
9029	CIRCULAR	0.60	0.28	0.15	0.60	1	0.64
932	CIRCULAR	0.45	0.16	0.11	0.45	1	0.30
946	CIRCULAR	0.30	0.07	0.07	0.30	1	0.11
947	CIRCULAR	0.30	0.07	0.07	0.30	1	0.19
948	CIRCULAR	0.30	0.07	0.07	0.30	1	0.17
949	CIRCULAR	0.30	0.07	0.07	0.30	1	0.06
952	CIRCULAR	0.25	0.05	0.06	0.25	1	0.03
953	CIRCULAR	0.25	0.05	0.06	0.25	1	0.03
955	CIRCULAR	0.25	0.05	0.06	0.25	1	0.07
957	CIRCULAR	1.05	0.87	0.26	1.05	1	2.11
958	CIRCULAR	1.05	0.87	0.26	1.05	1	1.73
959	CIRCULAR	1.05	0.87	0.26	1.05	1	1.37
960	CIRCULAR	1.05	0.87	0.26	1.05	1	1.23
961	CIRCULAR	1.05	0.87	0.26	1.05	1	1.63
962	CIRCULAR	1.05	0.87	0.26	1.05	1	1.64
963	CIRCULAR	1.05	0.87	0.26	1.05	1	1.41
964_1	CIRCULAR	1.05	0.87	0.26	1.05	1	1.22
964_2	CIRCULAR	1.05	0.87	0.26	1.05	1	1.68
965	CIRCULAR	1.05	0.87	0.26	1.05	1	1.37
966	CIRCULAR	1.05	0.87	0.26	1.05	1	1.38
967	CIRCULAR	1.05	0.87	0.26	1.05	1	1.33
968	CIRCULAR	1.05	0.87	0.26	1.05	1	1.46
969	CIRCULAR	1.05	0.87	0.26	1.05	1	1.47
970	CIRCULAR	1.05	0.87	0.26	1.05	1	1.13
971	CIRCULAR	1.05	0.87	0.26	1.05	1	1.39
988	CIRCULAR	0.45	0.16	0.11	0.45	1	0.18
989	CIRCULAR	0.45	0.16	0.11	0.45	1	0.13
990	CIRCULAR	0.45	0.16	0.11	0.45	1	0.10
990_1	CIRCULAR	0.53	0.22	0.13	0.53	1	0.21
9902	CIRCULAR	0.75	0.44	0.19	0.75	1	0.54
9904	FORCE_MAIN	0.60	0.28	0.15	0.60	1	0.08
9905	CIRCULAR	0.60	0.28	0.15	0.60	1	0.34
9906_1	FORCE_MAIN	0.45	0.16	0.11	0.45	1	0.04
9906_2	FORCE_MAIN	0.45	0.16	0.11	0.45	1	1.39
9907	CIRCULAR	0.45	0.16	0.11	0.45	1	0.09
9908	CIRCULAR	0.45	0.16	0.11	0.45	1	0.64
9909	FORCE_MAIN	0.60	0.28	0.15	0.60	1	0.22
9910	FORCE_MAIN	0.60	0.28	0.15	0.60	1	0.22
9911	CIRCULAR	0.35	0.10	0.09	0.35	1	0.77
9912	CIRCULAR	0.91	0.65	0.23	0.91	1	3.48
9914	FORCE_MAIN	0.30	0.07	0.07	0.30	1	0.08
9915	FORCE_MAIN	0.35	0.10	0.09	0.35	1	2.24
9916	FORCE_MAIN	0.35	0.10	0.09	0.35	1	2.01
992_1	CIRCULAR	0.53	0.22	0.13	0.53	1	0.20
992_2	CIRCULAR	0.53	0.22	0.13	0.53	1	0.12
998	CIRCULAR	0.50	0.20	0.12	0.50	1	0.24
999	CIRCULAR	0.50	0.20	0.12	0.50	1	0.23

```
****************
Analysis Options
****************
Flow Units ............... CMS
Process Models:
  Rainfall/Runoff ........ YES
  RDII ................... YES
  Snowmelt ............... NO
  Groundwater ............ NO
  Flow Routing ........... YES
  Ponding Allowed ........ NO
  Water Quality .......... NO
Flow Routing Method ...... DYNWAVE
Surcharge Method ......... EXTRAN
Starting Date ............ 03/13/2018 02:10:00
Ending Date .............. 03/17/2018 02:10:00
Antecedent Dry Days ...... 0.0
Report Time Step ......... 00:01:00
Routing Time Step ........ 1.00 sec
Variable Time Step ....... YES
Maximum Trials ........... 8
Number of Threads ........ 24
Head Tolerance ........... 0.001500 m


**********************         Volume        Volume
Rainfall Dependent I/I       hectare-m      10^6 ltr
**********************       ---------     ---------
Sewershed Rainfall ......      235.004      2350.068
RDII Produced ...........       26.820       268.204
RDII Ratio ..............        0.114


**************************        Volume        Volume
Flow Routing Continuity         hectare-m      10^6 ltr
**************************      ---------     ---------
Dry Weather Inflow .......         22.108       221.079
Wet Weather Inflow .......          0.000         0.000
Groundwater Inflow .......          0.000         0.000
RDII Inflow ..............         26.810       268.106
External Inflow ..........         26.937       269.369
External Outflow .........         72.619       726.202
Flooding Loss ............          3.016        30.162
Evaporation Loss .........          0.000         0.000
Exfiltration Loss ........          0.000         0.000
Initial Stored Volume ....          0.480         4.801
Final Stored Volume ......          0.818         8.176
Continuity Error (%) .....         -0.155


*************************
Highest Continuity Errors
*************************
Node 2340_2 (-59.92%)
Node 2340_1 (-53.75%)
Node 2340 (23.33%)
Node 2340_3 (1.86%)
Node 2271 (1.16%)


***************************
Time-Step Critical Elements
***************************
Link 2278 (75.47%)
Link 421 (1.55%)
Link 465 (1.37%)
Link 9029 (1.07%)


********************************
Highest Flow Instability Indexes
********************************
Link 964_1 (94)
Link 968 (94)
Link 1054_2 (93)
Link 964_2 (90)
Link 1050 (89)


*********************************
Most Frequent Nonconverging Nodes
*********************************
Node Dundas_Street_Outfall (39.79%)
Node Dundas_Street_PS_Overflow_1 (39.79%)
Node Front_St_PS_Overflow_1 (39.79%)
Node WWTP (39.79%)
Node 2340_2 (15.23%)


*************************
Routing Time Step Summary
*************************
Minimum Time Step           :     0.16 sec
Average Time Step           :     0.88 sec
```

```
Maximum Time Step            :     1.00 sec
% of Time in Steady State    :     0.00
Average Iterations per Step  :     7.03
% of Steps Not Converging    :    39.79
Time Step Frequencies        :
    1.000 -  0.871 sec       :    63.06 %
    0.871 -  0.758 sec       :    31.82 %
    0.758 -  0.660 sec       :     1.39 %
    0.660 -  0.574 sec       :     1.03 %
    0.574 -  0.500 sec       :     2.70 %
```

```
******************
Node Depth Summary
******************
```

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days	Time of Max Occurrence hr:min	Reported Max Depth Meters
1048	JUNCTION	8.84	9.66	80.36	0	00:00	9.39
1050	JUNCTION	18.28	26.12	95.62	0	17:54	26.12
1050_1	JUNCTION	13.33	21.18	95.62	0	18:00	21.17
1050_2	JUNCTION	13.33	21.18	95.62	0	17:54	21.17
1175	JUNCTION	1.13	2.78	83.67	0	17:40	2.77
1176	JUNCTION	1.30	2.95	83.63	0	17:49	2.95
1177	JUNCTION	1.36	3.01	83.54	0	17:51	3.00
1178	JUNCTION	2.04	3.70	83.43	0	17:49	3.70
1179	JUNCTION	2.23	3.87	83.36	0	17:53	3.87
1180	JUNCTION	2.89	4.50	83.23	0	17:39	4.49
1181	JUNCTION	3.16	4.74	83.13	0	17:45	4.73
1182	JUNCTION	3.39	4.94	83.03	0	17:42	4.93
2151	JUNCTION	7.74	8.18	79.74	0	15:36	8.18
2152	JUNCTION	7.96	8.43	79.82	0	15:40	8.43
2271	JUNCTION	1.38	2.54	81.82	0	17:29	2.53
2272	JUNCTION	3.24	4.39	81.81	0	17:23	4.38
2273	JUNCTION	3.66	8.15	86.94	0	00:02	5.83
2275	JUNCTION	5.51	9.01	86.59	0	00:00	7.49
2276	JUNCTION	6.23	12.82	90.19	0	00:00	8.05
2277	JUNCTION	7.88	16.60	92.76	0	00:00	9.55
2278	JUNCTION	9.22	11.71	84.41	0	00:00	10.46
2279	JUNCTION	3.55	4.68	81.80	0	17:54	4.67
2280	JUNCTION	6.59	7.72	81.79	0	17:21	7.71
2339	JUNCTION	0.65	2.64	95.03	0	15:04	2.63
2339_1	JUNCTION	2.31	4.54	95.14	0	15:04	4.53
2339_2	JUNCTION	2.58	4.52	95.12	0	15:04	4.52
2339_3	JUNCTION	2.52	4.55	95.15	0	15:04	4.55
2340	JUNCTION	0.56	2.66	96.17	0	15:04	2.63
2340_1	JUNCTION	0.27	2.58	96.09	0	12:59	2.48
2340_2	JUNCTION	0.40	2.57	96.09	0	12:59	2.47
2340_3	JUNCTION	2.31	5.39	96.09	0	15:04	5.30
2340_4	JUNCTION	3.17	5.18	95.88	0	15:04	5.16
2340_5	JUNCTION	2.91	5.30	96.00	0	15:04	5.29
430	JUNCTION	6.50	9.74	85.73	0	00:00	7.84
67	JUNCTION	2.81	83.23	162.93	0	12:47	36.43
902	JUNCTION	12.17	19.76	95.03	0	17:12	19.75
902a	JUNCTION	12.46	20.28	95.57	0	17:29	20.28
905	JUNCTION	8.96	26.06	101.51	0	02:16	24.28
950	JUNCTION	3.70	5.21	82.90	0	17:41	5.20
951	JUNCTION	4.44	5.89	82.72	0	17:43	5.88
952	JUNCTION	4.86	6.28	82.62	0	17:37	6.27
953	JUNCTION	5.27	6.61	82.41	0	17:24	6.59
954	JUNCTION	5.50	6.80	82.30	0	17:37	6.79
955	JUNCTION	5.87	7.13	82.17	0	17:44	7.12
956	JUNCTION	6.30	7.49	81.98	0	17:36	7.48
957	JUNCTION	6.55	7.70	81.84	0	17:37	7.69
958	JUNCTION	6.83	7.94	81.73	0	16:47	7.93
959	JUNCTION	7.12	8.17	81.58	0	16:57	8.16
960	JUNCTION	7.56	8.53	81.37	0	16:42	8.52
961	JUNCTION	7.86	8.78	81.23	0	16:57	8.76
962	JUNCTION	8.52	9.42	81.17	0	16:43	9.41
963	JUNCTION	8.72	9.50	80.81	0	16:36	9.49
964	JUNCTION	8.73	9.44	80.59	0	16:50	9.43
965	JUNCTION	8.85	9.60	80.33	0	00:00	9.42
9914	JUNCTION	8.81	9.65	80.36	0	00:00	9.34
9915	JUNCTION	5.33	11.94	86.44	0	11:11	7.20
9916	JUNCTION	4.70	5.10	79.60	0	15:39	5.10
DundasFM_1	JUNCTION	0.05	0.08	82.18	0	13:40	0.08
DundasFM_2	JUNCTION	0.96	1.88	81.83	0	15:50	1.87
DundasFM_3	JUNCTION	0.95	1.86	81.82	0	15:54	1.84
EastFM_1	JUNCTION	3.24	10.00	86.63	0	11:11	5.23
EastFM_2	JUNCTION	2.03	2.08	78.71	0	00:00	2.03
Dundas_Street_Outfall	OUTFALL	2.30	2.30	74.80	0	00:00	2.30
Dundas_Street_PS_Overflow_1	OUTFALL	0.00	0.00	77.00	0	00:00	0.00
Front_St_PS_Overflow_1	OUTFALL	0.80	0.80	74.80	0	00:00	0.80
WWTP	OUTFALL	5.29	5.29	78.71	0	00:00	5.29
1005	STORAGE	0.20	1.01	77.83	0	18:30	1.01
1007	STORAGE	0.23	1.18	77.82	0	18:30	1.18
1008	STORAGE	0.30	1.40	77.80	0	18:30	1.40
1020	STORAGE	0.41	1.91	77.69	0	18:30	1.91
1022	STORAGE	0.42	1.95	77.68	0	18:30	1.95
1023	STORAGE	0.47	2.22	77.58	0	18:30	2.22
1024	STORAGE	0.56	2.60	77.44	0	18:28	2.60
1025	STORAGE	0.60	2.79	77.36	0	18:22	2.79
1026	STORAGE	0.65	3.09	77.34	0	18:21	3.09
1029	STORAGE	0.33	1.83	77.35	0	18:21	1.83
1030	STORAGE	0.36	1.92	77.35	0	18:21	1.92
1031	STORAGE	0.46	2.38	77.34	0	18:21	2.38
1042	STORAGE	0.13	0.69	77.35	0	18:20	0.69
1044	STORAGE	0.04	0.06	81.02	0	17:10	0.06
1045	STORAGE	0.05	0.07	78.85	0	17:10	0.07
1049	STORAGE	3.05	7.79	77.29	0	18:20	7.79
1051	STORAGE	5.78	6.17	79.60	0	15:36	6.17
106	STORAGE	0.08	0.14	78.00	0	13:50	0.14
107	STORAGE	0.05	0.08	78.19	0	13:50	0.08
1085	STORAGE	0.12	0.15	82.43	0	13:25	0.15
1090	STORAGE	0.14	0.17	82.93	0	13:25	0.17
1091	STORAGE	0.18	0.22	82.70	0	13:25	0.22
1092	STORAGE	0.22	0.26	82.58	0	13:25	0.26
1093	STORAGE	0.23	0.28	83.08	0	13:25	0.28
1096	STORAGE	0.14	0.18	83.22	0	13:25	0.18
1101	STORAGE	0.20	0.24	83.35	0	13:23	0.24
1111	STORAGE	0.16	0.20	83.59	0	13:21	0.20
1114	STORAGE	0.29	0.33	83.59	0	13:21	0.33
1115	STORAGE	0.19	0.22	83.57	0	13:22	0.22
1116	STORAGE	0.10	0.12	83.34	0	13:23	0.12
1117	STORAGE	0.17	0.21	83.65	0	13:20	0.21
112	STORAGE	0.02	0.03	78.81	0	13:50	0.03
1131	STORAGE	0.00	0.00	82.10	0	00:00	0.00
1185	STORAGE	0.53	1.69	83.82	0	17:59	1.69
1186	STORAGE	0.53	1.73	83.82	0	17:59	1.73
1187	STORAGE	0.67	2.08	83.78	0	17:57	2.08
1190	STORAGE	0.82	2.37	83.74	0	17:57	2.37
1191	STORAGE	1.05	2.67	83.69	0	17:52	2.67
1192	STORAGE	0.27	0.29	85.43	1	12:50	0.29
1193	STORAGE	0.30	0.33	84.96	1	12:50	0.33
1195	STORAGE	0.29	0.31	84.65	1	12:51	0.31
1196	STORAGE	0.24	0.26	84.31	1	12:52	0.26
1199	STORAGE	0.29	0.82	83.90	0	17:59	0.82
1202	STORAGE	0.32	0.34	85.95	1	12:50	0.34
1203	STORAGE	0.27	0.30	86.27	1	12:50	0.30
1204	STORAGE	0.29	0.31	86.79	1	12:50	0.31
1205	STORAGE	0.29	0.31	87.31	1	12:50	0.31
1206	STORAGE	0.28	0.30	87.78	1	12:50	0.30
1208	STORAGE	0.26	0.28	89.96	1	12:50	0.28
1209	STORAGE	0.38	0.41	89.70	1	12:50	0.41
1210	STORAGE	0.29	0.31	89.21	1	12:50	0.31
1211	STORAGE	0.26	0.28	88.69	1	12:50	0.28
1212	STORAGE	0.31	0.33	88.27	1	12:50	0.33
1216	STORAGE	0.06	0.07	91.39	1	12:50	0.07
1217	STORAGE	0.08	0.10	90.76	1	12:50	0.10
1218	STORAGE	0.09	0.10	90.49	1	12:50	0.10
1219	STORAGE	0.09	0.10	90.19	1	12:50	0.10
1220	STORAGE	0.08	0.10	89.93	1	12:50	0.10
1221	STORAGE	0.09	0.11	89.63	1	12:50	0.11
1222	STORAGE	0.04	0.05	91.96	1	12:50	0.05
1241	STORAGE	0.05	0.06	92.98	1	12:50	0.06
1242	STORAGE	0.07	0.08	92.74	1	12:50	0.08
1243	STORAGE	0.35	0.37	92.52	1	12:50	0.37
1244	STORAGE	0.11	0.12	92.28	1	12:50	0.12
1245	STORAGE	0.12	0.14	91.98	1	12:50	0.14
1246	STORAGE	0.13	0.15	91.68	1	12:50	0.15
1247	STORAGE	0.14	0.16	91.34	1	12:50	0.16
1248	STORAGE	0.16	0.19	91.06	1	12:50	0.19
1249	STORAGE	0.18	0.22	90.74	1	12:50	0.22
1252	STORAGE	0.17	0.20	90.33	1	12:50	0.20
1253	STORAGE	0.16	0.19	89.95	1	12:50	0.19
1286	STORAGE	0.18	0.21	89.75	1	12:50	0.21
1287	STORAGE	0.16	0.19	89.51	1	12:50	0.19
1288	STORAGE	0.18	0.21	89.24	1	12:50	0.21
1289	STORAGE	0.18	0.21	88.99	1	12:50	0.21
1290	STORAGE	0.13	0.16	88.66	1	12:51	0.16
1291	STORAGE	0.48	0.57	88.35	0	15:53	0.57
1292	STORAGE	0.47	0.55	88.00	0	15:54	0.55
1293	STORAGE	0.44	0.52	87.64	0	15:54	0.52
1294	STORAGE	0.46	0.55	87.39	0	15:55	0.55
1295	STORAGE	0.48	0.57	86.96	0	15:56	0.57
1296	STORAGE	0.47	0.56	86.58	0	15:57	0.56
1297	STORAGE	0.44	0.52	86.18	0	15:57	0.52
1298	STORAGE	0.47	0.55	85.85	0	15:58	0.55
1299	STORAGE	0.47	0.56	85.51	0	15:58	0.56
1303	STORAGE	0.45	0.54	85.09	0	17:26	0.54
1306	STORAGE	0.48	0.62	84.79	0	17:44	0.62
1307	STORAGE	0.48	0.87	84.60	0	17:48	0.87
1308	STORAGE	0.41	1.05	84.39	0	17:50	1.05
1309	STORAGE	0.70	2.07	84.20	0	17:50	2.07
1310	STORAGE	0.81	2.34	83.92	0	17:49	2.34
1344	STORAGE	0.11	0.16	81.66	0	16:50	0.16
1345	STORAGE	0.11	0.17	81.51	0	17:00	0.17
1346	STORAGE	0.13	0.20	81.20	0	17:00	0.20
1347	STORAGE	0.12	0.18	81.00	0	17:00	0.18
1348	STORAGE	0.11	0.17	80.56	0	17:00	0.17
135	STORAGE	0.01	0.03	80.18	0	13:50	0.03
1352	STORAGE	0.15	0.22	80.12	0	17:01	0.22
136	STORAGE	0.02	0.03	80.51	0	13:50	0.03
137	STORAGE	0.01	0.02	81.16	0	13:50	0.02
138	STORAGE	0.12	0.28	82.67	0	13:55	0.28
1511	STORAGE	0.17	0.20	88.26	0	13:50	0.20
1514	STORAGE	0.15	0.17	88.07	0	13:50	0.17
157	STORAGE	0.15	0.95	81.84	0	15:44	0.94
158	STORAGE	0.00	0.36	81.86	0	15:44	0.35
159	STORAGE	0.16	1.08	81.77	0	15:44	1.08
1593	STORAGE	0.12	0.15	87.58	0	13:50	0.15
161	STORAGE	0.00	0.00	87.16	0	00:00	0.00
162	STORAGE	0.00	0.00	85.79	0	00:00	0.00
163	STORAGE	0.00	0.00	82.39	0	00:00	0.00
164	STORAGE	0.00	0.00	84.11	0	00:00	0.00
165	STORAGE	0.00	0.00	88.44	0	00:00	0.00
166	STORAGE	0.00	0.00	89.92	0	00:00	0.00
167	STORAGE	0.00	0.00	91.14	0	00:00	0.00
168	STORAGE	0.00	0.00	91.64	0	00:00	0.00
169	STORAGE	0.00	0.00	92.30	0	00:00	0.00
170	STORAGE	0.00	0.00	92.56	0	00:00	0.00
1705	STORAGE	0.00	0.00	82.31	0	00:00	0.00
171	STORAGE	0.00	0.00	93.24	0	00:00	0.00
1718	STORAGE	0.00	0.00	84.19	0	00:00	0.00
1719	STORAGE	0.00	0.00	83.65	0	00:00	0.00
172	STORAGE	0.00	0.00	93.22	0	00:00	0.00
1720	STORAGE	0.00	0.00	83.29	0	00:00	0.00
1721	STORAGE	0.00	0.00	82.82	0	00:00	0.00
1725	STORAGE	0.00	0.00	84.54	0	00:00	0.00

173	STORAGE	0.00	0.00	93.03	0	00:00	0.00
174	STORAGE	0.00	0.00	92.77	0	00:00	0.00
1742	STORAGE	0.00	0.00	84.57	0	00:00	0.00
1743	STORAGE	0.00	0.00	84.23	0	00:00	0.00
1745	STORAGE	0.22	0.27	82.40	0	13:25	0.27
1746	STORAGE	0.16	0.20	82.24	0	13:25	0.20
1747	STORAGE	0.18	0.23	81.96	0	13:25	0.23
1748	STORAGE	0.20	0.24	81.90	0	13:26	0.24
1749	STORAGE	0.17	0.21	81.61	0	13:28	0.21
175	STORAGE	0.00	0.00	92.71	0	00:00	0.00
1750	STORAGE	0.12	0.14	81.17	0	13:29	0.14
1754	STORAGE	0.00	0.00	81.97	0	00:00	0.00
1755	STORAGE	0.00	0.00	81.70	0	00:00	0.00
1756	STORAGE	0.00	0.00	81.45	0	00:00	0.00
1757	STORAGE	0.00	0.00	81.32	0	00:00	0.00
1758	STORAGE	0.00	0.00	81.11	0	00:00	0.00
1759	STORAGE	0.00	0.00	80.78	0	00:00	0.00
1763	STORAGE	0.00	0.00	80.10	0	00:00	0.00
1768	STORAGE	0.00	0.00	79.69	0	00:00	0.00
1769	STORAGE	0.00	0.00	79.43	0	00:00	0.00
1770	STORAGE	0.00	0.00	78.95	0	00:00	0.00
1771	STORAGE	0.11	0.13	77.94	0	13:40	0.13
1772	STORAGE	0.11	0.14	80.12	0	13:30	0.14
1773	STORAGE	0.12	0.14	79.04	0	13:31	0.14
1774	STORAGE	0.14	0.17	76.84	0	13:41	0.17
1794	STORAGE	0.22	0.27	75.39	0	13:42	0.27
1795	STORAGE	0.29	0.36	75.20	0	13:44	0.36
1796	STORAGE	0.33	0.40	75.16	0	13:45	0.40
1797	STORAGE	0.23	0.28	74.98	0	13:46	0.28
1798	STORAGE	0.24	0.30	74.86	0	13:48	0.30
1799	STORAGE	0.27	0.32	74.78	0	13:49	0.32
1800	STORAGE	0.25	0.31	74.66	0	13:51	0.31
1801	STORAGE	0.32	0.38	74.61	0	13:50	0.38
1812	STORAGE	0.32	0.39	74.56	0	13:50	0.39
1866	STORAGE	0.27	0.33	74.46	0	13:50	0.33
1867	STORAGE	0.33	0.39	74.39	0	13:51	0.39
1868	STORAGE	0.22	0.27	74.28	0	13:51	0.27
1869	STORAGE	0.28	0.35	74.11	0	13:53	0.35
1870	STORAGE	0.30	0.37	74.04	0	13:54	0.37
1871	STORAGE	0.29	0.35	73.96	0	13:55	0.35
1872	STORAGE	0.27	0.34	73.86	0	13:58	0.34
1873	STORAGE	0.38	0.45	73.80	0	13:58	0.45
1874	STORAGE	0.33	0.40	73.69	0	13:59	0.40
1875	STORAGE	0.28	0.34	73.59	0	14:00	0.34
1876	STORAGE	0.31	0.46	73.48	0	00:00	0.46
1877	STORAGE	0.12	0.15	87.31	0	13:50	0.15
1880	STORAGE	0.16	0.19	87.16	0	13:50	0.19
1881	STORAGE	0.15	0.18	86.96	0	13:51	0.18
1898	STORAGE	0.07	0.16	84.44	0	12:50	0.16
1899	STORAGE	0.07	0.17	84.42	0	12:49	0.17
1913	STORAGE	0.11	0.24	84.12	0	12:49	0.24
1914	STORAGE	0.10	0.25	84.06	0	12:42	0.25
1915	STORAGE	0.11	0.26	83.74	0	12:44	0.26
1916	STORAGE	0.11	0.28	83.18	0	12:50	0.28
1917	STORAGE	0.11	0.29	82.27	0	12:50	0.29
1918	STORAGE	0.11	0.21	81.93	0	12:50	0.21
1919	STORAGE	0.09	0.20	81.38	0	12:50	0.20
1920	STORAGE	0.13	0.16	81.59	0	17:00	0.16
1923	STORAGE	0.06	0.09	81.58	0	17:00	0.09
1927	STORAGE	0.06	0.09	81.32	0	17:10	0.09
1931	STORAGE	0.08	0.18	79.38	0	12:50	0.18
1932	STORAGE	0.09	0.21	77.46	0	12:55	0.21
1933	STORAGE	0.14	0.74	73.48	0	00:00	0.44
1938	STORAGE	0.34	0.83	73.48	0	00:00	0.69
1939	STORAGE	0.29	0.60	73.48	0	00:00	0.60
1940	STORAGE	0.33	0.75	73.48	0	00:00	0.71
1941	STORAGE	0.35	0.88	73.48	0	00:00	0.67
1942	STORAGE	1.23	1.55	73.18	0	00:01	1.55
1943	STORAGE	0.01	0.02	81.77	0	17:00	0.02
1968	STORAGE	0.17	0.20	87.71	0	13:50	0.20
1969	STORAGE	0.10	0.12	88.01	0	13:50	0.12
1970	STORAGE	0.10	0.12	88.12	0	13:50	0.12
2029	STORAGE	0.10	0.15	84.22	0	13:13	0.15
2030	STORAGE	0.11	0.15	84.29	0	13:12	0.15
2031	STORAGE	0.12	0.16	84.38	0	13:10	0.16
2032	STORAGE	0.20	0.23	84.13	0	13:15	0.23
2033	STORAGE	0.08	0.11	84.43	0	13:08	0.11
2034	STORAGE	0.09	0.13	84.52	0	13:05	0.13
2035	STORAGE	0.06	0.09	84.59	0	13:05	0.09
2036	STORAGE	0.09	0.12	84.79	0	13:05	0.12
2061	STORAGE	0.00	0.00	86.95	0	00:00	0.00
2062	STORAGE	0.77	2.99	84.49	0	16:05	2.99
2063	STORAGE	0.58	2.89	84.46	0	16:05	2.89
2096	STORAGE	0.16	0.24	79.79	0	17:04	0.24
2097	STORAGE	0.15	0.24	79.94	0	17:03	0.24
2105	STORAGE	0.76	4.02	91.34	0	20:55	4.02
211	STORAGE	0.14	0.31	92.01	0	13:18	0.31
212	STORAGE	0.00	0.00	92.16	0	00:00	0.00
213	STORAGE	0.14	0.30	91.77	0	13:23	0.30
2140	STORAGE	0.14	0.24	78.89	0	13:50	0.24
2140_1	STORAGE	0.10	0.19	78.96	0	13:50	0.19
2140_2	STORAGE	0.09	0.17	79.03	0	13:50	0.17
2140_3	STORAGE	0.07	0.14	79.10	0	13:50	0.14
2140_4	STORAGE	0.05	0.10	79.12	0	13:50	0.10
2141	STORAGE	1.28	5.64	79.06	0	20:49	5.64
2146	STORAGE	0.14	0.17	90.06	1	17:10	0.17
2147	STORAGE	0.11	0.13	90.54	1	12:50	0.13
2148	STORAGE	0.08	0.09	90.94	1	12:50	0.09
2154	STORAGE	0.32	2.29	80.19	0	16:05	2.29
2155	STORAGE	0.55	3.38	80.19	0	16:05	3.38
216	STORAGE	0.14	0.32	91.62	0	13:24	0.32
2176	STORAGE	0.14	0.17	83.72	0	13:19	0.17
2177	STORAGE	0.20	0.24	83.85	0	13:17	0.24
2178	STORAGE	0.19	0.23	83.91	0	13:16	0.23
2179	STORAGE	0.19	0.23	83.99	0	13:15	0.23
2180	STORAGE	0.17	0.21	84.00	0	13:15	0.21
2217	STORAGE	0.66	3.39	90.17	0	20:50	3.39
2218	STORAGE	0.73	3.31	89.93	0	20:50	3.31
2219	STORAGE	0.79	3.10	89.56	0	20:48	3.10
222	STORAGE	0.15	0.31	91.29	0	13:25	0.31
2220	STORAGE	0.56	2.50	88.45	0	20:35	2.50
2221	STORAGE	0.59	2.68	88.76	0	20:41	2.68
2222	STORAGE	0.44	1.89	87.46	0	20:18	1.89
2223	STORAGE	0.45	1.82	87.23	0	20:10	1.82
2224	STORAGE	0.38	1.47	86.63	0	19:56	1.47
2259	STORAGE	0.71	3.72	90.77	0	20:51	3.72
2264	STORAGE	0.00	0.05	84.94	0	18:01	0.05
2265	STORAGE	0.21	1.26	83.13	0	16:36	1.26
2266	STORAGE	0.46	1.86	83.04	0	17:44	1.86
2267	STORAGE	2.58	4.14	83.03	0	17:44	4.14
2268	STORAGE	0.07	0.16	85.62	0	13:05	0.16
2269	STORAGE	0.05	0.59	81.84	0	17:39	0.59
2270	STORAGE	0.68	1.82	81.83	0	17:38	1.82
2282	STORAGE	2.68	8.05	79.06	0	15:38	8.06
2282_1	STORAGE	2.49	7.79	78.79	0	18:20	7.79
2282_2	STORAGE	0.00	0.00	73.30	0	00:00	0.00
2286	STORAGE	0.12	0.15	86.77	0	13:52	0.15
2300	STORAGE	0.49	0.62	88.82	0	15:11	0.62
2301	STORAGE	0.57	0.92	89.72	0	15:10	0.92
2302	STORAGE	0.58	0.99	89.89	0	15:10	0.99
2303	STORAGE	0.66	1.27	90.44	0	15:10	1.27
2304	STORAGE	0.67	1.31	90.51	0	15:10	1.31
2305	STORAGE	0.66	1.55	91.15	0	15:08	1.55
2306	STORAGE	0.69	1.81	91.89	0	15:07	1.81
2307	STORAGE	0.76	2.11	92.56	0	15:06	2.11
2309	STORAGE	0.81	2.47	93.47	0	15:05	2.47
231	STORAGE	0.13	0.28	90.92	0	13:25	0.28
2310	STORAGE	0.84	2.68	94.04	0	15:04	2.68
2311	STORAGE	1.14	3.08	94.39	0	15:04	3.08
2312	STORAGE	0.75	2.84	94.83	0	15:04	2.84
2313	STORAGE	0.97	1.49	95.42	0	12:58	1.49
2314	STORAGE	1.44	1.96	96.51	0	14:10	1.96
2315	STORAGE	2.09	2.62	97.60	0	14:10	2.62
2317	STORAGE	2.99	3.51	98.71	0	14:10	3.51
2318	STORAGE	2.08	2.59	99.74	0	14:10	2.59
2319	STORAGE	2.65	3.13	100.77	0	14:10	3.13
2320	STORAGE	3.50	3.95	101.80	0	14:10	3.95
2321	STORAGE	4.34	4.75	102.82	0	06:31	4.75
2341	STORAGE	0.44	2.56	96.43	0	15:12	2.56
2342	STORAGE	0.37	2.52	96.67	0	15:12	2.52
2343	STORAGE	0.36	2.48	96.84	0	15:11	2.48
2344	STORAGE	0.35	2.44	96.94	0	15:10	2.44
2345	STORAGE	0.33	2.41	97.01	0	15:10	2.41
2346	STORAGE	0.29	2.30	97.09	0	15:10	2.30
2347	STORAGE	0.23	1.94	97.19	0	15:10	1.94
2348	STORAGE	0.22	1.69	97.25	0	14:55	1.69
2349	STORAGE	0.14	1.52	97.26	0	14:55	1.52
236	STORAGE	0.09	0.19	89.89	0	13:25	0.19
2363	STORAGE	0.60	3.70	92.87	0	21:10	3.70
2364	STORAGE	0.56	3.64	92.94	0	21:10	3.64
2365	STORAGE	0.55	3.51	93.14	0	21:11	3.51
2366	STORAGE	0.53	3.40	93.33	0	21:16	3.40
2367	STORAGE	0.51	3.27	93.56	0	21:19	3.27
2368	STORAGE	0.49	3.22	93.59	0	21:19	3.22
2369	STORAGE	0.49	3.14	93.67	0	21:19	3.14
2370	STORAGE	0.46	3.00	93.83	0	21:20	3.00
2371	STORAGE	0.46	2.98	93.87	0	21:20	2.98
2372	STORAGE	0.44	2.81	94.03	0	21:19	2.81
2373	STORAGE	0.40	2.64	94.17	0	21:17	2.64
2374	STORAGE	0.38	2.47	94.30	0	21:15	2.47
2375	STORAGE	0.36	2.28	94.42	0	21:13	2.28
2376	STORAGE	0.33	2.10	94.54	0	21:10	2.10
2377	STORAGE	0.31	1.91	94.65	0	21:10	1.91
2378	STORAGE	0.28	1.70	94.75	0	21:06	1.70
2379	STORAGE	0.26	1.48	94.85	0	21:04	1.48
2380	STORAGE	0.27	1.45	94.87	0	21:03	1.45
2381	STORAGE	0.23	1.19	94.97	0	20:59	1.19
2382	STORAGE	0.22	0.96	95.04	0	20:56	0.96
2383	STORAGE	0.19	0.78	95.10	0	20:55	0.78
2384	STORAGE	0.19	0.53	95.17	0	20:52	0.53
2385	STORAGE	0.16	0.31	95.22	0	20:51	0.31
2386	STORAGE	0.12	0.20	95.47	0	14:25	0.20
2387	STORAGE	0.11	0.18	95.76	0	14:25	0.18
2388	STORAGE	0.10	0.17	96.05	0	14:25	0.17
2389	STORAGE	0.10	0.16	96.35	0	14:25	0.16
2390	STORAGE	0.09	0.15	96.64	0	14:25	0.15
2391	STORAGE	0.08	0.13	96.99	0	14:25	0.13
2392	STORAGE	0.08	0.14	97.15	0	14:25	0.14
2393	STORAGE	0.08	0.13	98.26	0	14:25	0.13
2394	STORAGE	0.06	0.10	98.43	0	14:25	0.10
2395	STORAGE	0.04	0.07	98.60	0	14:25	0.07
2397	STORAGE	0.14	0.26	95.62	0	14:25	0.26
2398	STORAGE	0.11	0.20	95.87	0	14:25	0.20
2399	STORAGE	0.10	0.17	96.14	0	14:25	0.17
2400	STORAGE	0.09	0.15	96.42	0	14:25	0.15
2401	STORAGE	0.08	0.14	96.79	0	14:25	0.14
2402	STORAGE	0.05	0.09	97.04	0	14:25	0.09
2453	STORAGE	0.81	2.97	89.35	0	20:47	2.97
2474	STORAGE	0.95	4.90	80.44	0	17:35	4.90
2475	STORAGE	1.01	5.02	80.19	0	17:35	5.02
2476	STORAGE	1.07	5.10	79.87	0	17:35	5.10
2477	STORAGE	1.10	5.12	79.62	0	17:35	5.12
284	STORAGE	0.50	2.78	81.17	0	15:44	2.78
285	STORAGE	0.45	2.70	81.04	0	15:22	2.70
286	STORAGE	0.49	2.87	80.75	0	15:42	2.87
287	STORAGE	0.94	4.48	80.47	0	15:24	4.48
288	STORAGE	0.94	4.52	80.27	0	15:17	4.52
289	STORAGE	1.08	4.82	80.19	0	16:05	4.82
290	STORAGE	1.07	4.85	80.10	0	16:05	4.85
300	STORAGE	0.09	0.18	92.96	0	13:15	0.18
3000	STORAGE	0.14	0.21	78.04	0	18:23	0.21
3000A	STORAGE	0.16	0.24	78.00	0	18:27	0.24

301	STORAGE	0.09	0.19	92.45	0	13:15	0.19
302	STORAGE	0.06	0.12	93.55	0	13:15	0.12
303	STORAGE	0.08	0.16	93.31	0	13:15	0.16
360	STORAGE	0.14	0.57	81.86	0	17:50	0.57
401	STORAGE	1.08	4.94	80.02	0	16:15	4.94
402	STORAGE	1.18	5.26	79.96	0	16:15	5.26
403	STORAGE	1.24	5.43	79.80	0	16:35	5.43
404	STORAGE	1.40	6.01	79.65	0	17:00	6.01
405	STORAGE	1.52	6.13	79.58	0	17:10	6.13
406	STORAGE	1.80	6.37	79.53	0	17:26	6.37
409	STORAGE	1.46	5.88	79.99	0	17:37	5.88
411	STORAGE	1.51	6.11	79.79	0	17:36	6.11
413	STORAGE	1.10	5.17	79.59	0	17:25	5.17
414	STORAGE	1.13	5.08	79.06	0	14:55	5.08
418	STORAGE	1.05	4.65	80.36	0	17:38	4.65
419	STORAGE	0.96	4.73	80.58	0	17:35	4.73
421	STORAGE	1.32	5.43	80.22	0	17:37	5.43
424	STORAGE	0.93	4.61	79.93	0	17:43	4.61
425	STORAGE	1.17	5.39	79.56	0	17:44	5.39
426	STORAGE	1.39	5.77	79.22	0	17:44	5.77
427	STORAGE	1.33	5.61	79.06	0	15:07	5.61
428	STORAGE	0.65	3.62	80.61	0	17:39	3.62
429	STORAGE	0.90	4.54	80.33	0	17:41	4.54
431	STORAGE	0.87	4.66	80.61	0	17:35	4.66
432	STORAGE	0.74	4.16	80.74	0	17:35	4.16
433	STORAGE	0.95	3.69	80.85	0	17:36	3.69
434	STORAGE	0.94	3.68	80.86	0	17:39	3.68
435	STORAGE	0.07	0.15	87.54	0	12:56	0.15
436	STORAGE	0.92	3.66	82.89	0	16:25	3.66
437	STORAGE	1.09	4.04	80.89	0	17:45	4.04
438	STORAGE	0.46	3.05	80.89	0	17:45	3.05
439	STORAGE	0.98	3.95	80.67	0	17:39	3.95
44	STORAGE	0.15	0.24	78.79	0	13:50	0.24
446	STORAGE	0.08	0.89	81.28	0	17:45	0.89
447	STORAGE	0.11	1.10	81.28	0	17:45	1.10
448	STORAGE	0.18	1.61	81.23	0	17:45	1.61
449	STORAGE	0.93	3.95	81.04	0	17:48	3.95
45	STORAGE	0.15	0.27	78.60	0	13:50	0.27
451	STORAGE	0.46	2.94	80.98	0	17:37	2.94
452	STORAGE	0.86	3.62	80.88	0	17:36	3.62
453	STORAGE	0.52	2.98	80.98	0	17:36	2.98
454	STORAGE	0.58	3.26	80.78	0	17:37	3.26
455	STORAGE	0.23	1.48	81.58	0	18:06	1.48
456	STORAGE	0.02	0.41	81.33	0	17:47	0.41
457	STORAGE	1.48	3.51	81.54	0	18:10	3.51
458	STORAGE	1.71	3.57	81.30	0	17:58	3.57
459	STORAGE	0.32	2.45	81.30	0	17:58	2.45
460	STORAGE	0.81	3.68	81.17	0	17:55	3.68
461	STORAGE	0.33	2.54	81.22	0	17:45	2.54
462	STORAGE	0.43	2.67	81.18	0	17:35	2.67
463	STORAGE	0.37	2.58	81.09	0	17:38	2.58
464	STORAGE	0.41	2.74	81.06	0	17:38	2.74
465	STORAGE	0.57	3.01	81.36	0	17:35	3.01
468	STORAGE	1.23	3.65	82.09	0	18:30	3.65
469	STORAGE	1.09	3.54	82.13	0	18:35	3.54
473	STORAGE	1.44	3.70	81.86	0	18:24	3.70
477	STORAGE	0.58	2.80	82.53	0	18:50	2.80
478	STORAGE	0.56	2.95	82.29	0	18:40	2.95
479	STORAGE	0.39	1.68	83.77	0	19:20	1.68
480	STORAGE	0.46	1.68	83.19	0	19:05	1.68
481	STORAGE	0.53	2.56	82.87	0	18:58	2.56
501	STORAGE	1.13	3.25	82.15	0	17:25	3.25
502	STORAGE	1.17	3.14	81.97	0	17:25	3.14
503	STORAGE	1.37	2.88	81.42	0	17:35	2.88
506	STORAGE	0.75	3.05	82.37	0	17:25	3.05
507	STORAGE	0.54	3.71	83.63	0	17:28	3.71
508	STORAGE	0.59	3.35	82.92	0	17:25	3.35
51	STORAGE	0.16	0.28	78.49	0	13:50	0.28
511	STORAGE	0.81	5.46	86.36	0	13:12	5.47
512	STORAGE	0.59	4.09	84.42	0	17:35	4.09
513	STORAGE	0.42	3.65	84.46	0	17:35	3.65
514	STORAGE	0.38	3.44	84.47	0	17:35	3.44
516	STORAGE	0.60	5.00	86.16	0	15:35	5.00
521	STORAGE	0.37	3.37	84.48	0	17:35	3.37
54	STORAGE	0.17	0.29	78.37	0	13:50	0.29
55_1	STORAGE	0.16	0.28	78.29	0	13:50	0.28
553	STORAGE	0.61	3.85	92.63	0	21:05	3.85
554	STORAGE	0.74	4.30	92.49	0	21:05	4.30
555	STORAGE	0.71	4.27	92.36	0	21:05	4.27
556	STORAGE	0.77	4.33	92.21	0	21:05	4.33
56	STORAGE	0.16	0.29	78.21	0	13:50	0.29
563	STORAGE	0.65	3.98	92.53	0	21:05	3.98
63	STORAGE	0.16	0.29	78.13	0	13:51	0.29
64	STORAGE	0.19	0.33	78.05	0	13:53	0.33
649	STORAGE	0.81	4.28	92.05	0	21:03	4.28
65	STORAGE	0.14	0.23	77.79	0	13:53	0.23
65_1	STORAGE	0.09	0.19	77.70	0	13:53	0.19
650	STORAGE	0.84	4.22	91.88	0	20:59	4.22
652	STORAGE	0.73	4.08	91.66	0	20:57	4.08
653	STORAGE	0.71	4.06	91.61	0	20:57	4.06
654	STORAGE	0.75	4.05	91.42	0	20:56	4.05
66	STORAGE	1.54	2.04	74.19	0	16:51	2.03
666	STORAGE	0.29	2.56	92.01	0	20:55	2.56
667	STORAGE	0.35	2.90	92.00	0	20:55	2.90
668	STORAGE	0.41	3.17	91.99	0	20:55	3.17
669	STORAGE	0.48	3.50	91.97	0	21:03	3.50
670	STORAGE	0.51	3.64	91.95	0	21:02	3.64
671	STORAGE	0.54	3.78	91.93	0	20:58	3.78
672	STORAGE	0.55	3.90	91.91	0	20:58	3.90
673	STORAGE	0.74	3.88	91.10	0	20:54	3.88
675	STORAGE	0.74	3.85	91.02	0	20:54	3.85
676	STORAGE	0.70	3.74	90.84	0	20:52	3.74
678	STORAGE	0.70	3.58	90.50	0	20:50	3.58
68	STORAGE	0.06	0.12	77.90	0	13:50	0.12
682	STORAGE	0.25	1.79	90.70	0	20:45	1.79
684	STORAGE	0.32	2.02	90.61	0	20:45	2.02
685	STORAGE	0.68	3.42	90.21	0	20:50	3.42
686	STORAGE	0.73	3.27	89.88	0	20:50	3.27
689	STORAGE	0.78	3.18	89.68	0	20:50	3.18
690	STORAGE	0.84	2.87	89.17	0	20:45	2.87
708	STORAGE	0.26	1.62	90.86	0	20:35	1.62
780	STORAGE	0.89	2.72	88.90	0	20:43	2.72
781	STORAGE	0.56	2.42	88.30	0	20:35	2.42
782	STORAGE	0.50	2.17	87.89	0	20:25	2.17
783	STORAGE	0.54	2.04	87.60	0	20:20	2.04
796	STORAGE	0.09	0.14	92.13	0	14:25	0.14
852	STORAGE	0.09	0.15	91.47	0	14:22	0.15
853	STORAGE	0.09	0.15	90.80	0	14:24	0.15
859	STORAGE	0.10	0.16	89.44	0	14:24	0.16
860	STORAGE	0.10	0.16	90.12	0	14:25	0.16
861	STORAGE	0.10	0.16	89.93	0	14:25	0.16
864	STORAGE	0.11	0.18	88.00	0	14:25	0.18
865	STORAGE	0.10	0.16	88.62	0	14:25	0.16
866	STORAGE	0.13	0.21	87.87	0	14:25	0.21
877	STORAGE	0.13	0.22	86.77	0	14:25	0.22
878	STORAGE	0.11	0.18	87.53	0	14:25	0.18
879	STORAGE	0.16	0.53	86.59	0	19:25	0.53
880	STORAGE	0.18	0.81	86.46	0	19:40	0.81
881	STORAGE	0.21	1.08	86.35	0	19:41	1.08
882	STORAGE	0.37	1.31	86.19	0	19:51	1.31
883	STORAGE	0.47	1.76	87.06	0	20:07	1.76
884	STORAGE	0.45	1.58	86.76	0	19:58	1.58
885	STORAGE	0.40	1.39	86.35	0	19:52	1.39
886	STORAGE	0.36	1.30	85.42	0	19:47	1.30
887	STORAGE	0.33	1.13	84.65	0	19:40	1.13
9001	STORAGE	0.11	0.12	84.61	1	06:55	0.12
9002	STORAGE	0.25	0.26	84.53	1	06:55	0.26
9003	STORAGE	0.16	0.17	84.41	1	07:03	0.17
9004	STORAGE	0.15	0.16	84.36	1	07:01	0.16
9005	STORAGE	0.11	0.12	84.29	1	06:58	0.12
9006	STORAGE	0.13	0.14	84.19	1	07:05	0.14
9050	STORAGE	0.11	0.13	86.58	0	13:52	0.13
9051	STORAGE	0.11	0.13	86.46	0	13:53	0.13
9052	STORAGE	0.11	0.13	86.06	0	13:53	0.13
9053	STORAGE	0.11	0.13	85.65	0	13:54	0.13
9054	STORAGE	0.08	0.10	85.47	0	13:54	0.10
9055	STORAGE	0.08	0.10	82.61	0	13:54	0.10
9056	STORAGE	0.09	0.10	79.77	0	13:50	0.10
9057	STORAGE	0.09	0.10	77.36	0	13:50	0.10
9058	STORAGE	0.11	0.13	76.69	0	13:50	0.13
9059	STORAGE	0.11	0.13	76.38	0	13:50	0.13
9060	STORAGE	0.11	0.13	75.88	0	13:50	0.13
9061	STORAGE	0.11	0.13	75.77	0	13:50	0.13
924	STORAGE	0.06	0.12	87.62	0	13:05	0.12
940	STORAGE	0.06	0.93	84.49	0	17:35	0.93
941	STORAGE	0.00	0.00	86.78	0	00:00	0.00
942	STORAGE	0.31	2.99	84.49	0	17:35	2.99
945	STORAGE	0.48	3.94	85.53	0	15:37	3.94
946	STORAGE	0.54	4.43	85.81	0	15:36	4.43
948	STORAGE	0.24	2.13	85.16	0	15:19	2.13
978	STORAGE	0.13	0.20	79.52	0	17:07	0.20
984	STORAGE	0.14	0.21	78.94	0	17:08	0.21
985	STORAGE	0.17	0.24	78.74	0	17:09	0.24
986	STORAGE	0.17	0.26	78.51	0	17:10	0.26
987	STORAGE	0.18	0.27	78.21	0	17:11	0.27
988	STORAGE	0.20	0.42	77.95	0	18:30	0.42
9902	STORAGE	1.77	6.53	77.31	0	18:21	6.53
991	STORAGE	0.15	0.44	77.94	0	18:30	0.44
996	STORAGE	0.20	0.81	77.90	0	18:31	0.81
997	STORAGE	0.26	1.09	77.86	0	18:30	1.09
999	STORAGE	0.32	1.32	77.83	0	18:30	1.32

****
Node Inflow Summary
****

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days	Time of Max Occurrence hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
1048	JUNCTION	0.000	1.316	0	17:45	0	372	0.000
1050	JUNCTION	0.000	2.912	0	00:00	0	60.2	-0.367
1050_1	JUNCTION	0.000	0.946	0	09:03	0	219	0.041
1050_2	JUNCTION	0.000	0.385	0	11:50	0	84.5	0.062
1175	JUNCTION	0.000	0.899	0	21:03	0	260	0.005
1176	JUNCTION	0.002	0.901	0	21:06	0.339	260	0.015
1177	JUNCTION	0.000	0.901	0	21:02	0	260	0.014
1178	JUNCTION	0.000	0.901	0	21:03	0	260	0.011
1179	JUNCTION	0.000	0.901	0	21:01	0	260	0.034
1180	JUNCTION	0.000	0.901	0	21:03	0	260	0.029
1181	JUNCTION	0.000	0.901	0	21:03	0	260	0.023
1182	JUNCTION	0.000	0.957	0	18:18	0	265	0.015
2151	JUNCTION	0.012	1.340	0	17:54	1.96	376	-0.000
2152	JUNCTION	0.012	1.327	0	17:59	1.96	374	-0.000
2271	JUNCTION	0.000	0.033	0	00:47	0	1.35	1.176
2272	JUNCTION	0.000	0.102	0	00:00	0	1.36	0.603
2273	JUNCTION	0.000	0.237	0	00:00	0	62.4	0.048
2275	JUNCTION	0.000	0.237	0	00:00	0	62.4	0.000
2276	JUNCTION	0.000	0.237	0	00:00	0	62.4	-0.000
2277	JUNCTION	0.490	0.490	0	00:00	169	169	-0.000
2278	JUNCTION	0.000	0.340	0	16:02	0	107	0.000
2279	JUNCTION	0.000	0.101	0	00:00	0	1.37	0.004
2280	JUNCTION	0.000	0.981	0	18:23	0	266	0.000
2339	JUNCTION	0.000	0.326	0	15:04	0	42.4	-0.037
2339_1	JUNCTION	0.000	0.230	0	15:04	0	14.4	0.000
2339_2	JUNCTION	0.000	0.050	0	11:51	0	15.9	0.000
2339_3	JUNCTION	0.000	0.050	0	11:17	0	12.1	0.000
2340	JUNCTION	0.000	1.127	1	00:50	0	50.2	30.434
2340_1	JUNCTION	0.000	0.742	0	12:42	0	11.3	-34.961

2340_2	JUNCTION	0.000	0.679	1	03:17	0	11.3	-37.470	
2340_3	JUNCTION	0.000	0.239	0	15:38	0	14.7	1.898	
2340_4	JUNCTION	0.000	0.050	0	11:51	0	15.9	-0.139	
2340_5	JUNCTION	0.000	0.050	0	11:15	0	12.1	0.069	
430	JUNCTION	0.000	0.345	0	00:00	0	107	-0.000	
67	JUNCTION	0.000	0.301	0	12:58	0	21	0.000	
902	JUNCTION	0.000	0.346	0	22:18	0	84.4	0.000	
902a	JUNCTION	0.000	0.347	0	22:16	0	84.4	0.001	
905	JUNCTION	0.000	0.795	0	22:14	0	192	0.016	
950	JUNCTION	0.000	0.957	0	18:08	0	265	0.003	
951	JUNCTION	0.000	0.957	0	18:08	0	265	0.000	
952	JUNCTION	0.000	0.957	0	18:08	0	265	-0.000	
953	JUNCTION	0.000	0.957	0	18:08	0	265	0.000	
954	JUNCTION	0.000	0.956	0	18:04	0	265	-0.000	
955	JUNCTION	0.000	0.957	0	18:08	0	265	0.000	
956	JUNCTION	0.000	0.957	0	18:08	0	265	-0.000	
957	JUNCTION	0.000	0.956	0	18:06	0	265	-0.000	
958	JUNCTION	0.000	0.981	0	18:23	0	265	-0.000	
959	JUNCTION	0.000	0.981	0	18:17	0	265	-0.000	
960	JUNCTION	0.000	0.981	0	18:08	0	265	-0.000	
961	JUNCTION	0.000	0.981	0	18:09	0	265	0.000	
962	JUNCTION	0.000	1.315	0	17:54	0	372	-0.000	
963	JUNCTION	0.000	1.315	0	17:44	0	372	0.000	
964	JUNCTION	0.000	1.315	0	18:05	0	372	0.000	
965	JUNCTION	0.000	1.315	0	17:51	0	372	-0.000	
9914	JUNCTION	0.000	1.318	0	17:35	0	372	-0.000	
9915	JUNCTION	0.000	0.443	0	00:01	0	73.7	0.000	
9916	JUNCTION	0.000	0.001	0	00:00	0	0.00176	0.000	
DundasFM_1	JUNCTION	0.000	0.142	0	02:43	0	15.4	0.058	
DundasFM_2	JUNCTION	0.000	0.130	0	13:40	0	15.1	0.000	
DundasFM_3	JUNCTION	0.000	0.130	0	13:58	0	15.1	0.020	
EastFM_1	JUNCTION	0.000	0.400	0	00:00	0	73.6	-0.000	
EastFM_2	JUNCTION	0.000	0.000	0	00:00	0	0	-1.909	ltr
Dundas_Street_Outfall	OUTFALL	0.000	0.000	0	00:00	0	0	0.000	ltr
Dundas_Street_PS_Overflow_1	OUTFALL	0.000	0.000	0	00:00	0	0	0.000	ltr
Front_St_PS_Overflow_1	OUTFALL	0.000	0.000	0	00:00	0	0	0.000	ltr
WWTP	OUTFALL	0.000	2.854	0	15:36	0	726	0.000	
1005	STORAGE	0.047	0.047	0	16:50	7.66	7.66	0.005	
1007	STORAGE	0.001	0.048	0	16:51	0.21	7.87	0.022	
1008	STORAGE	0.000	0.134	0	18:30	0.0355	22.5	0.021	
1020	STORAGE	0.001	0.134	0	18:30	0.0839	22.5	-0.005	
1022	STORAGE	0.001	0.135	0	18:30	0.0996	22.6	0.020	
1023	STORAGE	0.001	0.136	0	18:37	0.142	22.8	0.016	
1024	STORAGE	0.001	0.136	0	18:39	0.142	22.9	-0.003	
1025	STORAGE	0.000	0.136	0	18:40	0	22.9	0.006	
1026	STORAGE	0.000	0.168	0	18:36	0	28	0.000	
1029	STORAGE	0.004	0.075	0	14:05	0.571	4.53	0.013	
1030	STORAGE	0.002	0.075	0	14:07	0.399	4.93	0.008	
1031	STORAGE	0.001	0.031	0	18:05	0.175	5.09	0.034	
1042	STORAGE	0.006	0.024	0	17:10	1.01	3.95	0.004	
1044	STORAGE	0.003	0.015	0	17:10	0.523	2.41	0.019	
1045	STORAGE	0.003	0.018	0	17:10	0.532	2.94	0.028	
1049	STORAGE	0.000	1.144	0	14:56	0	277	-0.017	
1051	STORAGE	0.000	2.856	0	15:36	0	726	0.013	
106	STORAGE	0.001	0.011	0	13:50	0.0672	1.23	0.071	
107	STORAGE	0.008	0.010	0	13:50	0.893	1.16	0.024	
1085	STORAGE	0.002	0.074	0	13:25	0.402	17.8	0.009	
1090	STORAGE	0.001	0.071	0	13:25	0.0888	17.2	0.022	
1091	STORAGE	0.001	0.071	0	13:25	0.0888	17.3	0.030	
1092	STORAGE	0.001	0.072	0	13:25	0.0888	17.4	0.039	
1093	STORAGE	0.011	0.070	0	13:25	3.07	17.1	0.043	
1096	STORAGE	0.001	0.061	0	13:23	0.224	14.1	0.028	
1101	STORAGE	0.002	0.059	0	13:23	0.274	13.8	0.021	
1111	STORAGE	0.001	0.056	0	13:20	0.0924	13.4	0.013	
1114	STORAGE	0.001	0.057	0	13:20	0.126	13.5	0.017	
1115	STORAGE	0.000	0.057	0	13:21	0.0404	13.5	0.032	
1116	STORAGE	0.000	0.057	0	13:22	0.0404	13.6	0.014	
1117	STORAGE	0.000	0.055	0	13:19	0.0322	13.3	0.017	
112	STORAGE	0.001	0.002	0	13:50	0.0672	0.268	0.038	
1131	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1185	STORAGE	0.001	0.238	1	12:50	0.176	71.6	0.003	
1186	STORAGE	0.000	0.240	1	14:46	0.101	71.7	0.014	
1187	STORAGE	0.001	0.243	1	14:46	0.155	71.9	0.043	
1190	STORAGE	0.001	0.246	1	14:46	0.155	72	0.016	
1191	STORAGE	0.001	0.248	1	14:45	0.155	72.2	0.028	
1192	STORAGE	0.002	0.236	1	12:50	0.483	71	0.022	
1193	STORAGE	0.000	0.236	1	12:50	0.0993	71	0.025	
1195	STORAGE	0.000	0.236	1	12:51	0.0935	71.1	0.006	
1196	STORAGE	0.001	0.237	1	12:50	0.17	71.3	0.014	
1199	STORAGE	0.001	0.238	1	12:50	0.225	71.5	0.029	
1202	STORAGE	0.002	0.234	1	12:50	0.483	70.5	0.025	
1203	STORAGE	0.002	0.232	1	12:50	0.483	70	0.018	
1204	STORAGE	0.002	0.230	1	12:50	0.483	69.6	0.025	
1205	STORAGE	0.002	0.228	1	12:50	0.483	69.1	0.024	
1206	STORAGE	0.002	0.226	1	12:50	0.483	68.6	0.024	
1208	STORAGE	0.139	0.201	1	12:50	45.9	62.1	0.009	
1209	STORAGE	0.001	0.202	1	12:50	0.204	62.3	0.044	
1210	STORAGE	0.001	0.220	1	12:50	0.204	67.1	0.013	
1211	STORAGE	0.001	0.221	1	12:50	0.204	67.3	0.020	
1212	STORAGE	0.003	0.225	1	12:50	0.911	68.2	0.025	
1216	STORAGE	0.005	0.009	1	12:50	1.18	2.37	0.051	
1217	STORAGE	0.005	0.014	1	12:50	1.18	3.55	0.019	
1218	STORAGE	0.001	0.015	1	12:50	0.261	3.81	0.042	
1219	STORAGE	0.001	0.016	1	12:50	0.261	4.07	0.036	
1220	STORAGE	0.001	0.017	1	12:50	0.261	4.33	0.028	
1221	STORAGE	0.001	0.018	1	12:50	0.261	4.59	0.049	
1222	STORAGE	0.005	0.005	1	12:40	1.18	1.18	0.025	
1241	STORAGE	0.006	0.006	1	12:40	1.6	1.6	0.014	
1242	STORAGE	0.006	0.012	1	12:50	1.59	3.19	0.030	
1243	STORAGE	0.006	0.018	1	12:50	1.59	4.77	0.115	
1244	STORAGE	0.006	0.024	1	12:50	1.59	6.35	0.027	
1245	STORAGE	0.006	0.030	1	12:50	1.59	7.93	0.024	
1246	STORAGE	0.006	0.036	1	12:50	1.59	9.52	0.022	
1247	STORAGE	0.006	0.042	1	12:50	1.59	11.1	0.021	
1248	STORAGE	0.006	0.049	1	12:50	1.59	12.7	0.025	
1249	STORAGE	0.006	0.055	1	12:50	1.59	14.3	0.030	
1252	STORAGE	0.006	0.061	1	12:50	1.59	15.8	0.014	
1253	STORAGE	0.000	0.061	1	12:50	0.126	16	0.016	
1286	STORAGE	0.000	0.062	1	12:50	0.126	16.1	0.018	
1287	STORAGE	0.000	0.062	1	12:50	0.126	16.2	0.018	
1288	STORAGE	0.000	0.063	1	12:50	0.126	16.3	0.021	
1289	STORAGE	0.000	0.063	1	12:50	0.126	16.5	0.023	
1290	STORAGE	0.000	0.064	1	12:50	0.126	16.6	0.018	
1291	STORAGE	0.000	0.679	0	15:53	0.0442	181	0.015	
1292	STORAGE	0.001	0.679	0	15:53	0.178	181	0.011	
1293	STORAGE	0.001	0.679	0	15:55	0.178	182	0.007	
1294	STORAGE	0.001	0.680	0	15:55	0.178	182	0.013	
1295	STORAGE	0.001	0.680	0	15:56	0.178	182	0.014	
1296	STORAGE	0.001	0.681	0	15:56	0.178	182	0.013	
1297	STORAGE	0.001	0.681	0	15:57	0.178	182	0.009	
1298	STORAGE	0.001	0.682	0	15:57	0.178	182	0.012	
1299	STORAGE	0.009	0.687	0	15:58	2.33	185	0.014	
1303	STORAGE	0.000	0.687	0	15:59	0.0637	185	0.011	
1306	STORAGE	0.000	0.687	0	15:58	0.105	185	0.012	
1307	STORAGE	0.000	0.687	0	15:47	0.105	185	0.012	
1308	STORAGE	0.000	0.687	0	16:56	0.105	185	0.008	
1309	STORAGE	0.011	0.694	0	17:05	2.88	188	0.017	
1310	STORAGE	0.001	0.695	0	16:58	0.215	188	0.012	
1344	STORAGE	0.049	0.049	0	16:50	8.37	8.37	0.003	
1345	STORAGE	0.001	0.050	0	16:50	0.123	8.49	0.012	
1346	STORAGE	0.002	0.052	0	17:00	0.284	8.77	0.026	
1347	STORAGE	0.009	0.060	0	17:00	1.41	10.2	0.022	
1348	STORAGE	0.002	0.063	0	17:00	0.381	10.6	0.016	
135	STORAGE	0.001	0.002	0	13:50	0.0672	0.201	0.048	
1352	STORAGE	0.003	0.065	0	17:00	0.405	11	0.011	
136	STORAGE	0.001	0.001	0	13:50	0.0672	0.134	0.072	
137	STORAGE	0.001	0.001	0	13:40	0.0672	0.0672	0.138	
138	STORAGE	0.000	0.077	0	16:52	0	6.02	-0.032	
1511	STORAGE	0.028	0.028	0	13:40	7.06	7.06	0.032	
1514	STORAGE	0.000	0.029	0	13:50	0.107	7.28	0.014	
157	STORAGE	0.094	0.154	0	15:44	14.1	16	-0.020	
158	STORAGE	0.000	0.023	0	15:19	0	0.0682	-0.152	
159	STORAGE	0.000	0.261	0	14:57	0	31.1	0.046	
1593	STORAGE	0.004	0.035	0	13:50	1.12	8.68	0.042	
161	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
162	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
163	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
164	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
165	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
166	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
167	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
168	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
169	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
170	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1705	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
171	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1718	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1719	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
172	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1720	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1721	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1725	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
173	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
174	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1742	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1743	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1745	STORAGE	0.003	0.077	0	13:25	0.525	18.3	0.025	
1746	STORAGE	0.003	0.080	0	13:25	0.379	18.7	0.027	
1747	STORAGE	0.000	0.080	0	13:25	0	18.7	0.017	
1748	STORAGE	0.000	0.080	0	13:25	0	18.7	0.029	
1749	STORAGE	0.002	0.082	0	13:27	0.59	19.2	0.038	
175	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1750	STORAGE	0.002	0.084	0	13:28	0.59	19.8	0.018	
1754	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1755	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1756	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1757	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1758	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1759	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1763	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1768	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1769	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1770	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
1771	STORAGE	0.020	0.109	0	13:40	5	26	0.005	
1772	STORAGE	0.002	0.087	0	13:29	0.59	20.4	0.013	
1773	STORAGE	0.002	0.089	0	13:30	0.59	21	0.016	
1774	STORAGE	0.002	0.112	0	13:40	0.59	26.6	0.014	
1794	STORAGE	0.002	0.114	0	13:41	0.59	27.2	0.041	
1795	STORAGE	0.002	0.116	0	13:42	0.59	27.8	0.044	
1796	STORAGE	0.033	0.149	0	13:43	8.22	36	0.031	
1797	STORAGE	0.001	0.150	0	13:45	0.14	36.1	0.026	
1798	STORAGE	0.001	0.150	0	13:46	0.14	36.2	0.027	
1799	STORAGE	0.001	0.151	0	13:47	0.14	36.3	0.036	
1800	STORAGE	0.001	0.152	0	13:49	0.14	36.5	0.037	
1801	STORAGE	0.001	0.152	0	13:50	0.14	36.6	0.046	
1812	STORAGE	0.020	0.172	0	13:50	4.93	41.5	0.045	
1866	STORAGE	0.001	0.173	0	13:50	0.162	41.7	0.037	
1867	STORAGE	0.001	0.173	0	13:50	0.162	41.8	0.035	
1868	STORAGE	0.001	0.174	0	13:51	0.162	41.9	0.022	
1869	STORAGE	0.001	0.174	0	13:51	0.162	42.1	0.035	
1870	STORAGE	0.001	0.175	0	13:53	0.162	42.2	0.036	
1871	STORAGE	0.001	0.176	0	13:54	0.162	42.4	0.037	
1872	STORAGE	0.001	0.176	0	13:55	0.162	42.5	0.039	
1873	STORAGE	0.001	0.227	0	13:57	0.162	55.2	0.030	
1874	STORAGE	0.001	0.227	0	13:58	0.127	55.3	0.015	
1875	STORAGE	0.001	0.228	0	14:00	0.127	55.4	0.011	
1876	STORAGE	0.001	0.228	0	14:00	0.127	55.5	-0.034	
1877	STORAGE	0.001	0.035	0	13:50	0.171	8.84	0.041	
1880	STORAGE	0.005	0.040	0	13:50	1.3	10.1	0.057	
1881	STORAGE	0.000	0.041	0	13:50	0.0827	10.2	0.063	
1898	STORAGE	0.026	0.026	0	12:40	2.02	2.02	0.003	

1899	STORAGE	0.026	0.053	0	12:40	2.02	4.05	0.005	
1913	STORAGE	0.026	0.079	0	12:49	2.02	6.07	0.007	
1914	STORAGE	0.003	0.083	0	12:49	0.334	6.4	0.023	
1915	STORAGE	0.031	0.114	0	12:43	2.39	8.79	0.021	
1916	STORAGE	0.024	0.137	0	12:44	1.8	10.6	0.020	
1917	STORAGE	0.022	0.159	0	12:50	1.68	12.3	0.001	
1918	STORAGE	0.001	0.160	0	12:50	0.0795	12.3	0.002	
1919	STORAGE	0.000	0.160	0	12:50	0	12.3	0.012	
1920	STORAGE	0.002	0.003	0	17:00	0.393	0.522	0.263	
1923	STORAGE	0.005	0.008	0	17:00	0.739	1.26	0.050	
1927	STORAGE	0.004	0.012	0	17:00	0.628	1.89	0.060	
1931	STORAGE	0.000	0.160	0	12:50	0	12.3	0.004	
1932	STORAGE	0.005	0.165	0	12:55	0.795	13.1	0.018	
1933	STORAGE	0.013	0.176	0	12:56	2.04	15.2	-0.178	
1938	STORAGE	0.003	0.341	0	00:02	0.923	56.8	-0.049	
1939	STORAGE	0.001	0.229	0	14:01	0.127	55.7	-0.049	
1940	STORAGE	0.001	0.268	0	00:02	0.127	55.8	-0.055	
1941	STORAGE	0.005	0.390	0	00:01	0.785	57.6	-0.082	
1942	STORAGE	0.005	0.907	0	00:00	0.785	73.7	-0.006	
1943	STORAGE	0.001	0.001	0	16:50	0.129	0.129	0.031	
1968	STORAGE	0.001	0.030	0	13:50	0.143	7.56	0.062	
1969	STORAGE	0.001	0.029	0	13:50	0.143	7.42	0.020	
1970	STORAGE	0.000	0.028	0	13:45	0.118	7.18	0.022	
2029	STORAGE	0.002	0.022	0	13:12	0.33	3.52	0.034	
2030	STORAGE	0.001	0.020	0	13:10	0.0869	3.19	0.045	
2031	STORAGE	0.005	0.020	0	13:05	0.743	3.11	0.083	
2032	STORAGE	0.001	0.053	0	13:13	0.166	13	0.047	
2033	STORAGE	0.000	0.015	0	13:06	0.0653	2.37	0.070	
2034	STORAGE	0.000	0.014	0	13:05	0.0653	2.31	0.065	
2035	STORAGE	0.000	0.014	0	13:05	0.0653	2.24	0.011	
2036	STORAGE	0.013	0.013	0	12:55	2.18	2.18	0.068	
2061	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
2062	STORAGE	0.000	0.197	1	09:30	0	62.4	0.007	
2063	STORAGE	0.000	0.343	0	13:43	0.0377	80.7	0.004	
2096	STORAGE	0.002	0.069	0	17:03	0.461	11.6	0.028	
2097	STORAGE	0.001	0.066	0	17:01	0.196	11.2	0.025	
2105	STORAGE	0.001	0.302	0	23:44	0.144	50.5	0.018	
211	STORAGE	0.015	0.087	0	13:15	1.66	9.39	0.008	
212	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
213	STORAGE	0.010	0.096	0	13:18	1.05	10.4	0.008	
2140	STORAGE	0.021	0.065	0	13:50	4.09	8.44	0.046	
2140_1	STORAGE	0.011	0.044	0	13:50	1.09	4.35	0.060	
2140_2	STORAGE	0.011	0.033	0	13:50	1.09	3.26	0.058	
2140_3	STORAGE	0.011	0.022	0	13:50	1.09	2.18	0.054	
2140_4	STORAGE	0.011	0.011	0	13:40	1.09	1.09	0.024	
2141	STORAGE	0.000	0.270	0	14:55	0	28.9	0.002	
2146	STORAGE	0.021	0.062	1	12:50	5.41	16.2	0.006	
2147	STORAGE	0.021	0.041	1	12:50	5.41	10.8	0.053	
2148	STORAGE	0.021	0.021	1	12:40	5.41	5.41	0.021	
2154	STORAGE	0.001	0.009	0	13:55	0.135	0.194	0.009	
2155	STORAGE	0.001	0.016	0	13:21	0.135	0.42	0.030	
216	STORAGE	0.021	0.117	0	13:22	2.24	12.7	0.007	
2176	STORAGE	0.000	0.055	0	13:18	0	13.2	0.030	
2177	STORAGE	0.000	0.055	0	13:16	0	13.2	0.042	
2178	STORAGE	0.000	0.055	0	13:15	0	13.3	0.042	
2179	STORAGE	0.001	0.055	0	13:15	0.149	13.3	0.031	
2180	STORAGE	0.001	0.054	0	13:15	0.149	13.1	0.031	
2217	STORAGE	0.001	0.383	0	21:51	0.187	64.4	0.006	
2218	STORAGE	0.001	0.384	0	21:51	0.0704	64.4	0.009	
2219	STORAGE	0.002	0.390	0	22:42	0.259	65.4	0.014	
222	STORAGE	0.018	0.135	0	13:24	1.99	14.7	0.008	
2220	STORAGE	0.007	0.403	0	22:50	1	67.3	0.011	
2221	STORAGE	0.001	0.397	0	22:53	0.137	66.4	0.011	
2222	STORAGE	0.001	0.413	1	00:54	0.203	68.6	0.007	
2223	STORAGE	0.001	0.416	1	00:53	0.203	68.8	0.008	
2224	STORAGE	0.001	0.425	1	00:52	0.203	69.4	0.007	
2259	STORAGE	0.001	0.312	1	01:19	0.102	51.5	0.014	
2264	STORAGE	0.000	0.038	0	18:01	0	1.11	-0.000	
2265	STORAGE	0.000	0.082	0	13:25	0	4.77	0.016	
2266	STORAGE	0.000	0.079	0	13:55	0	4.77	-0.003	
2267	STORAGE	0.000	0.078	0	14:02	0	4.77	0.044	
2268	STORAGE	0.000	0.044	0	13:05	0	3.66	0.022	
2269	STORAGE	0.000	0.024	0	18:26	0	0.59	0.005	
2270	STORAGE	0.000	0.024	0	18:24	0	0.965	0.089	
2282	STORAGE	0.000	1.071	0	14:55	0	249	-0.001	
2282_1	STORAGE	0.000	1.062	0	14:55	0.0582	248	-0.029	
2282_2	STORAGE	0.000	0.000	0	00:00	0	0	0.000	ltr
2286	STORAGE	0.000	0.041	0	13:51	0.0827	10.3	0.029	
2300	STORAGE	0.000	0.640	0	15:10	0.0442	165	0.015	
2301	STORAGE	0.000	0.640	0	15:10	0.0442	165	0.013	
2302	STORAGE	0.000	0.640	0	15:08	0.0442	165	0.008	
2303	STORAGE	0.000	0.639	0	15:08	0.0442	165	0.007	
2304	STORAGE	0.002	0.639	0	15:07	0.179	165	0.010	
2305	STORAGE	0.002	0.638	0	15:05	0.179	164	0.017	
2306	STORAGE	0.002	0.636	0	15:05	0.179	164	0.018	
2307	STORAGE	0.016	0.634	0	14:55	1.54	164	0.012	
2309	STORAGE	0.003	0.619	0	14:30	0.263	163	0.028	
231	STORAGE	0.013	0.148	0	13:25	1.41	16.1	0.006	
2310	STORAGE	0.003	0.617	0	14:25	0.263	162	0.012	
2311	STORAGE	0.003	0.615	0	14:25	0.263	162	0.014	
2312	STORAGE	0.076	0.661	0	12:59	21.3	162	0.004	
2313	STORAGE	0.002	0.304	1	04:08	0.218	99.6	0.036	
2314	STORAGE	0.002	0.300	1	04:11	0.145	99.4	0.028	
2315	STORAGE	0.002	0.298	0	12:24	0.145	99.3	0.038	
2317	STORAGE	0.002	0.297	2	06:16	0.145	99.2	0.058	
2318	STORAGE	0.002	0.301	2	06:09	0.145	99.1	0.030	
2319	STORAGE	0.002	0.307	2	06:07	0.145	99	0.039	
2320	STORAGE	0.002	0.313	2	06:06	0.145	98.9	0.052	
2321	STORAGE	0.417	0.417	0	12:40	110	110	0.030	
2341	STORAGE	0.058	0.327	0	14:55	13.6	41.6	0.017	
2342	STORAGE	0.021	0.272	0	14:45	2	27.9	-0.002	
2343	STORAGE	0.021	0.252	0	14:45	2	25.9	0.011	
2344	STORAGE	0.021	0.232	0	14:35	2	24	0.011	
2345	STORAGE	0.021	0.212	0	14:35	2	22	0.010	
2346	STORAGE	0.021	0.193	0	14:35	2	20	0.012	
2347	STORAGE	0.021	0.175	0	12:46	2	18	-0.004	
2348	STORAGE	0.081	0.156	0	13:40	8.75	16	0.031	
2349	STORAGE	0.076	0.076	0	13:35	7.22	7.22	0.002	
236	STORAGE	0.011	0.159	0	13:25	1.14	17.2	0.004	
2363	STORAGE	0.000	0.185	0	12:49	0.0388	28.8	0.043	
2364	STORAGE	0.000	0.191	0	12:53	0.0388	28.8	-0.010	
2365	STORAGE	0.000	0.196	0	12:59	0	28.8	0.040	
2366	STORAGE	0.000	0.200	0	13:06	0.0388	28.8	0.025	
2367	STORAGE	0.007	0.201	0	13:07	1.01	28.7	0.015	
2368	STORAGE	0.005	0.194	0	13:08	0.706	27.7	0.000	
2369	STORAGE	0.005	0.192	0	13:18	0.706	27	0.005	
2370	STORAGE	0.005	0.187	0	13:18	0.706	26.3	0.016	
2371	STORAGE	0.005	0.184	0	13:26	0.706	25.6	-0.010	
2372	STORAGE	0.005	0.180	0	13:38	0.706	24.9	0.038	
2373	STORAGE	0.005	0.176	0	13:51	0.706	24.2	0.026	
2374	STORAGE	0.005	0.172	0	13:54	0.706	23.5	0.004	
2375	STORAGE	0.005	0.167	0	14:21	0.706	22.8	0.030	
2376	STORAGE	0.005	0.162	0	14:35	0.706	22.1	0.027	
2377	STORAGE	0.005	0.158	0	14:42	0.706	21.4	0.006	
2378	STORAGE	0.005	0.152	0	14:35	0.706	20.7	0.031	
2379	STORAGE	0.005	0.147	0	14:34	0.706	20	0.016	
2380	STORAGE	0.005	0.142	0	14:33	0.706	19.3	0.005	
2381	STORAGE	0.005	0.136	0	14:31	0.706	18.6	0.020	
2382	STORAGE	0.005	0.131	0	14:30	0.706	17.9	0.052	
2383	STORAGE	0.005	0.126	0	14:29	0.706	17.2	0.005	
2384	STORAGE	0.005	0.121	0	14:25	0.706	16.5	0.050	
2385	STORAGE	0.005	0.116	0	14:25	0.706	15.8	0.016	
2386	STORAGE	0.005	0.054	0	14:25	0.735	7.34	0.056	
2387	STORAGE	0.005	0.048	0	14:25	0.735	6.61	0.041	
2388	STORAGE	0.005	0.043	0	14:25	0.735	5.87	0.026	
2389	STORAGE	0.005	0.038	0	14:25	0.735	5.14	0.048	
2390	STORAGE	0.005	0.032	0	14:25	0.735	4.41	0.026	
2391	STORAGE	0.005	0.027	0	14:25	0.735	3.67	0.036	
2392	STORAGE	0.005	0.022	0	14:25	0.735	2.94	0.012	
2393	STORAGE	0.005	0.016	0	14:25	0.735	2.2	0.064	
2394	STORAGE	0.005	0.011	0	14:25	0.735	1.47	0.028	
2395	STORAGE	0.005	0.005	0	14:20	0.735	0.735	0.025	
2397	STORAGE	0.009	0.057	0	14:25	1.3	7.76	0.058	
2398	STORAGE	0.009	0.047	0	14:25	1.3	6.47	0.041	
2399	STORAGE	0.009	0.038	0	14:25	1.3	5.18	0.042	
2400	STORAGE	0.009	0.028	0	14:25	1.3	3.88	0.023	
2401	STORAGE	0.009	0.019	0	14:25	1.3	2.59	0.081	
2402	STORAGE	0.009	0.009	0	14:20	1.3	1.3	0.030	
2453	STORAGE	0.001	0.391	0	22:43	0.149	65.6	0.019	
2474	STORAGE	0.004	0.208	0	17:25	0.425	19.6	0.012	
2475	STORAGE	0.004	0.211	0	17:35	0.533	20.2	0.014	
2476	STORAGE	0.004	0.215	0	17:35	0.367	20.5	0.010	
2477	STORAGE	0.004	0.218	0	17:35	0.367	20.9	-0.011	
284	STORAGE	0.001	0.251	0	14:35	0.135	31.2	1.094	
285	STORAGE	0.001	0.241	0	15:44	0.135	31	-0.345	
286	STORAGE	0.001	0.232	0	13:48	0.135	31.2	0.061	
287	STORAGE	0.001	0.220	0	13:38	0.135	31.3	-0.000	
288	STORAGE	0.001	0.219	0	15:53	0.135	31.4	0.028	
289	STORAGE	0.001	0.187	0	15:17	0.135	31.3	0.037	
290	STORAGE	0.024	0.198	0	15:18	3.45	34.6	0.025	
300	STORAGE	0.010	0.061	0	13:15	1.03	6.62	0.007	
3000	STORAGE	0.002	0.080	0	17:11	0.406	13.5	0.002	
3000A	STORAGE	0.001	0.080	0	17:12	0.122	13.7	0.018	
301	STORAGE	0.010	0.071	0	13:15	1.1	7.72	0.011	
302	STORAGE	0.028	0.028	0	13:05	2.99	2.99	0.003	
303	STORAGE	0.024	0.052	0	13:14	2.6	5.59	0.005	
360	STORAGE	0.066	0.066	0	16:50	10.7	10.7	0.014	
401	STORAGE	0.024	0.214	0	15:19	3.45	38	0.018	
402	STORAGE	0.032	0.241	0	15:20	4.63	42.7	0.007	
403	STORAGE	0.003	0.241	0	15:21	0.471	43.1	0.025	
404	STORAGE	0.000	0.239	0	15:23	0	43.1	0.001	
405	STORAGE	0.000	0.238	0	15:24	0	43.1	0.013	
406	STORAGE	0.000	1.030	0	17:25	0.0582	220	0.028	
409	STORAGE	0.003	0.840	0	12:56	0.44	177	0.013	
411	STORAGE	0.001	0.811	0	13:05	0.112	177	0.010	
413	STORAGE	0.004	0.222	0	17:25	0.367	21.3	0.002	
414	STORAGE	0.000	0.222	0	17:35	0	21.3	0.003	
418	STORAGE	0.001	0.895	0	13:02	0.0838	176	-0.004	
419	STORAGE	0.065	0.204	0	17:35	7.07	19.2	0.010	
421	STORAGE	0.001	0.863	0	12:56	0.0838	176	0.009	
424	STORAGE	0.000	0.198	0	17:36	0.0737	22.6	-0.025	
425	STORAGE	0.000	0.198	0	17:41	0.0575	22.6	0.009	
426	STORAGE	0.000	0.198	0	17:44	0.0575	22.7	0.022	
427	STORAGE	0.000	0.274	0	14:55	0	34.6	0.006	
428	STORAGE	0.002	0.196	0	17:25	0.183	22.2	0.006	
429	STORAGE	0.002	0.197	0	17:35	0.266	22.5	0.055	
431	STORAGE	0.004	0.148	0	13:34	0.425	12.1	0.008	
432	STORAGE	0.002	0.201	0	13:33	0.229	11.7	0.001	
433	STORAGE	0.000	0.205	0	13:33	0	13.6	0.005	
434	STORAGE	0.002	0.210	0	13:33	0.229	13.6	0.062	
435	STORAGE	0.011	0.170	0	13:25	1.14	18.4	0.003	
436	STORAGE	0.000	0.343	0	13:44	0.0377	80.8	0.009	
437	STORAGE	0.000	0.905	0	13:35	0	183	0.018	
438	STORAGE	0.000	0.204	1	09:57	0	6.24	-0.005	
439	STORAGE	0.001	0.889	0	13:04	0.0838	176	0.030	
44	STORAGE	0.003	0.068	0	13:50	0.337	8.77	0.057	
446	STORAGE	0.003	0.004	0	15:14	0.271	0.271	0.004	
447	STORAGE	0.003	0.022	0	22:15	0.271	1.14	0.031	
448	STORAGE	0.003	0.024	0	22:22	0.271	1.42	0.016	
449	STORAGE	0.002	0.571	0	20:10	0.239	102	0.022	
45	STORAGE	0.027	0.095	0	13:50	2.99	11.8	0.024	
451	STORAGE	0.003	0.112	0	17:45	0.271	7.63	0.022	
452	STORAGE	0.002	0.110	0	17:35	0.229	7.18	0.191	
453	STORAGE	0.002	0.191	0	13:45	0.149	20.3	0.010	
454	STORAGE	0.002	0.178	0	13:37	0.183	19.9	0.010	
455	STORAGE	0.000	0.065	0	14:53	0	10.1	-0.001	
456	STORAGE	0.000	0.018	0	16:04	0	0.603	-0.017	
457	STORAGE	0.002	0.595	0	21:18	0.244	103	0.040	
458	STORAGE	0.001	0.596	0	21:18	0.11	103	0.024	
459	STORAGE	0.001	0.038	1	01:19	0.11	1.73	0.002	
460	STORAGE	0.001	0.595	0	14:02	0.11	102	0.019	
461	STORAGE	0.000	0.038	1	01:20	0	1.73	0.003	

462	STORAGE	0.017	0.084	0	14:51	1.78	5.33	0.018
463	STORAGE	0.002	0.083	0	17:25	0.222	5.19	-0.007
464	STORAGE	0.002	0.085	0	17:35	0.207	5.4	0.009
465	STORAGE	0.002	0.219	0	14:22	0.149	21.3	0.024
468	STORAGE	0.010	0.562	0	20:35	1.3	93.3	0.012
469	STORAGE	0.003	0.554	0	20:45	0.466	92	0.016
473	STORAGE	0.002	0.564	0	20:35	0.244	93.3	0.054
477	STORAGE	0.003	0.548	0	20:45	0.466	90.9	0.015
478	STORAGE	0.003	0.551	0	20:46	0.466	91.4	0.007
479	STORAGE	0.003	0.538	0	20:42	0.464	89.5	0.003
480	STORAGE	0.003	0.541	0	20:45	0.466	90	0.012
481	STORAGE	0.003	0.544	0	20:45	0.466	90.4	0.010
501	STORAGE	0.036	0.210	0	14:23	2.83	20.3	0.072
502	STORAGE	0.004	0.213	0	14:23	0.296	20.5	0.088
503	STORAGE	0.004	0.217	0	14:22	0.296	20.8	0.087
506	STORAGE	0.015	0.174	0	14:24	1.15	17.4	0.065
507	STORAGE	0.003	0.157	0	14:28	0.269	16	0.008
508	STORAGE	0.003	0.160	0	14:26	0.269	16.3	0.037
51	STORAGE	0.007	0.102	0	13:50	0.827	12.6	0.050
511	STORAGE	0.194	0.194	0	14:50	15.4	15.5	0.015
512	STORAGE	0.003	0.156	0	13:12	0.269	15.8	0.041
513	STORAGE	0.002	0.020	0	17:20	0.145	1.71	0.026
514	STORAGE	0.001	0.019	0	17:20	0.109	1.57	0.004
516	STORAGE	0.000	0.042	0	13:12	0	1.3	-0.001
521	STORAGE	0.006	0.017	0	14:37	0.476	1.46	-0.012
54	STORAGE	0.002	0.104	0	13:50	0.232	12.8	0.045
55_1	STORAGE	0.002	0.106	0	13:50	0.19	13	0.032
553	STORAGE	0.035	0.213	0	12:45	4.76	33.6	-0.002
554	STORAGE	0.002	0.248	0	16:15	0.256	41.2	0.010
555	STORAGE	0.003	0.250	0	16:15	0.472	41.6	0.018
556	STORAGE	0.001	0.248	0	16:15	0.103	41.7	0.026
56	STORAGE	0.002	0.107	0	13:50	0.19	13.2	0.034
563	STORAGE	0.051	0.248	0	12:42	7.34	40.9	0.009
63	STORAGE	0.002	0.109	0	13:50	0.19	13.4	0.040
64	STORAGE	0.002	0.111	0	13:50	0.19	13.5	0.077
649	STORAGE	0.002	0.249	0	21:50	0.333	42.1	0.036
65	STORAGE	0.002	0.112	0	13:53	0.19	13.7	0.002
65_1	STORAGE	0.000	0.112	0	13:53	0	13.7	0.001
650	STORAGE	0.001	0.295	0	22:50	0.131	49.7	0.035
652	STORAGE	0.001	0.297	0	23:22	0.114	49.8	0.013
653	STORAGE	0.002	0.299	0	23:36	0.318	50.2	0.011
654	STORAGE	0.001	0.301	0	23:37	0.201	50.4	0.014
66	STORAGE	0.000	0.137	0	13:50	0	16.5	0.003
666	STORAGE	0.011	0.011	0	14:20	1.45	1.45	0.064
667	STORAGE	0.011	0.021	0	13:18	1.44	2.89	0.008
668	STORAGE	0.011	0.031	0	13:13	1.44	4.32	0.070
669	STORAGE	0.014	0.046	0	12:45	1.87	6.19	0.007
670	STORAGE	0.004	0.046	0	12:41	0.556	6.75	0.036
671	STORAGE	0.003	0.048	0	12:34	0.417	7.16	0.042
672	STORAGE	0.003	0.048	0	12:25	0.417	7.58	0.040
673	STORAGE	0.003	0.305	1	00:00	0.396	50.9	0.017
675	STORAGE	0.001	0.307	1	01:19	0.151	51	0.014
676	STORAGE	0.003	0.310	1	01:19	0.35	51.4	0.012
678	STORAGE	0.001	0.381	0	21:50	0.113	64.1	0.014
68	STORAGE	0.014	0.025	0	13:50	1.5	2.73	0.013
682	STORAGE	0.001	0.091	0	14:31	0.0844	12.3	0.014
684	STORAGE	0.002	0.092	0	14:19	0.24	12.5	0.043
685	STORAGE	0.001	0.382	0	21:51	0.0836	64.2	0.008
686	STORAGE	0.004	0.387	0	21:51	0.528	64.9	0.008
689	STORAGE	0.002	0.388	0	21:52	0.236	65.2	0.013
690	STORAGE	0.004	0.395	0	22:50	0.574	66.1	0.022
708	STORAGE	0.089	0.089	0	14:20	12.2	12.2	0.019
780	STORAGE	0.001	0.396	0	22:50	0.121	66.2	0.016
781	STORAGE	0.001	0.405	0	22:50	0.16	67.5	0.013
782	STORAGE	0.003	0.407	0	22:50	0.367	67.9	0.015
783	STORAGE	0.004	0.411	0	22:50	0.554	68.4	0.011
796	STORAGE	0.054	0.054	0	14:20	7.5	7.5	0.005
852	STORAGE	0.004	0.057	0	14:25	0.678	8.18	0.012
853	STORAGE	0.003	0.060	0	14:23	0.381	8.56	0.011
859	STORAGE	0.003	0.069	0	14:25	0.381	9.7	0.004
860	STORAGE	0.003	0.063	0	14:24	0.381	8.94	0.007
861	STORAGE	0.003	0.066	0	14:25	0.381	9.32	0.011
864	STORAGE	0.039	0.110	0	14:25	5.28	15.4	0.003
865	STORAGE	0.003	0.071	0	14:25	0.381	10.1	0.010
866	STORAGE	0.003	0.113	0	14:25	0.381	15.7	0.003
877	STORAGE	0.009	0.123	0	14:25	1.3	17.2	0.010
878	STORAGE	0.001	0.114	0	14:25	0.117	15.9	0.007
879	STORAGE	0.002	0.125	0	14:25	0.265	17.4	0.015
880	STORAGE	0.001	0.127	0	14:25	0.188	17.6	0.014
881	STORAGE	0.001	0.128	0	14:25	0.188	17.8	0.018
882	STORAGE	0.006	0.529	0	20:25	0.886	88.2	0.010
883	STORAGE	0.001	0.418	1	00:53	0.203	69	0.011
884	STORAGE	0.001	0.421	1	00:52	0.203	69.2	0.010
885	STORAGE	0.001	0.428	1	00:51	0.203	69.6	0.008
886	STORAGE	0.003	0.534	1	00:50	0.464	88.7	0.013
887	STORAGE	0.003	0.535	0	20:40	0.4	89.1	0.019
9001	STORAGE	0.029	0.029	1	06:50	8.74	8.74	0.005
9002	STORAGE	0.000	0.029	1	06:55	0.0497	8.79	0.022
9003	STORAGE	0.000	0.029	1	06:55	0.0497	8.83	0.021
9004	STORAGE	0.000	0.030	1	07:04	0.0497	8.88	0.020
9005	STORAGE	0.000	0.030	1	07:03	0.0497	8.93	0.009
9006	STORAGE	0.002	0.031	1	07:02	0.359	9.29	0.016
9050	STORAGE	0.000	0.041	0	13:52	0.0827	10.4	0.003
9051	STORAGE	0.000	0.042	0	13:52	0.0827	10.5	0.017
9052	STORAGE	0.000	0.042	0	13:53	0.0827	10.5	0.017
9053	STORAGE	0.000	0.042	0	13:54	0.0827	10.6	0.004
9054	STORAGE	0.000	0.043	0	13:54	0.0827	10.7	0.007
9055	STORAGE	0.000	0.043	0	13:54	0.0827	10.8	0.011
9056	STORAGE	0.005	0.048	0	13:50	1.32	12.1	0.004
9057	STORAGE	0.000	0.049	0	13:50	0.0827	12.2	0.006
9058	STORAGE	0.000	0.049	0	13:50	0.0827	12.3	0.010
9059	STORAGE	0.000	0.049	0	13:50	0.0827	12.3	0.019
9060	STORAGE	0.000	0.050	0	13:50	0.0827	12.4	0.003
9061	STORAGE	0.000	0.050	0	13:50	0.0827	12.5	0.004
924	STORAGE	0.044	0.044	0	12:55	3.66	3.66	0.026
940	STORAGE	0.005	0.005	0	14:50	0.38	0.38	0.012
941	STORAGE	0.000	0.000	0	00:00	0	0	0.000 ltr
942	STORAGE	0.008	0.015	0	12:23	0.603	0.983	0.071
945	STORAGE	0.000	0.038	0	13:18	0	1.17	0.011
946	STORAGE	0.000	0.040	0	13:13	0	1.24	0.003
948	STORAGE	0.000	0.038	0	15:37	0	1.12	-0.000
978	STORAGE	0.005	0.074	0	17:05	0.821	12.4	0.027
984	STORAGE	0.002	0.076	0	17:07	0.347	12.8	0.021
985	STORAGE	0.001	0.077	0	17:08	0.122	12.9	0.020
986	STORAGE	0.001	0.077	0	17:09	0.122	13	0.027
987	STORAGE	0.001	0.078	0	17:11	0.122	13.1	0.015
988	STORAGE	0.001	0.081	0	17:13	0.122	13.8	0.007
9902	STORAGE	0.000	0.168	0	18:36	0	28.1	-0.001
991	STORAGE	0.000	0.081	0	18:13	0.0713	13.9	0.028
996	STORAGE	0.003	0.084	0	18:23	0.445	14.3	0.005
997	STORAGE	0.000	0.084	0	18:22	0.0334	14.3	0.020
999	STORAGE	0.001	0.086	0	18:52	0.229	14.6	0.024

****
Node Surcharge Summary
****

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
1048	JUNCTION	96.00	8.165	0.000
1050	JUNCTION	96.00	20.069	0.000
1050_1	JUNCTION	94.69	19.472	0.000
1050_2	JUNCTION	96.00	20.496	0.000
1175	JUNCTION	41.00	1.728	0.000
1176	JUNCTION	50.29	1.870	0.000
1177	JUNCTION	52.99	1.909	0.000
1178	JUNCTION	67.73	2.115	0.000
1179	JUNCTION	90.77	2.824	0.000
1180	JUNCTION	95.01	3.223	0.000
1181	JUNCTION	95.27	3.577	0.000
1182	JUNCTION	95.32	3.783	0.000
2151	JUNCTION	96.00	6.681	0.000
2152	JUNCTION	96.00	6.932	0.000
2271	JUNCTION	94.74	2.137	0.000
2272	JUNCTION	95.33	2.764	0.000
2273	JUNCTION	95.96	6.452	0.000
2275	JUNCTION	96.00	8.541	0.000
2276	JUNCTION	96.00	12.277	0.000
2277	JUNCTION	96.00	15.533	0.000
2278	JUNCTION	96.00	8.097	0.000
2279	JUNCTION	96.00	4.273	0.000
2280	JUNCTION	96.00	6.670	0.000
2339	JUNCTION	20.23	1.825	0.000
2339_1	JUNCTION	87.87	4.089	0.000
2339_2	JUNCTION	95.86	4.274	0.000
2339_3	JUNCTION	95.44	4.304	0.000
2340	JUNCTION	15.00	1.543	0.000
2340_1	JUNCTION	14.71	1.461	0.000
2340_2	JUNCTION	14.99	1.458	0.000
2340_3	JUNCTION	87.82	4.937	0.000
2340_4	JUNCTION	95.86	4.925	0.000
2340_5	JUNCTION	95.39	5.050	0.000
430	JUNCTION	96.00	9.338	0.000
67	JUNCTION	76.00	82.783	0.000
902	JUNCTION	96.00	19.308	0.000
902a	JUNCTION	96.00	19.834	0.000
905	JUNCTION	95.86	25.450	0.000
950	JUNCTION	95.86	4.068	0.000
951	JUNCTION	96.00	4.841	0.000
952	JUNCTION	96.00	5.071	0.000
953	JUNCTION	96.00	5.407	0.000
954	JUNCTION	96.00	5.623	0.000
955	JUNCTION	96.00	5.942	0.000
956	JUNCTION	96.00	6.393	0.000
957	JUNCTION	96.00	6.556	0.000
958	JUNCTION	96.00	6.756	0.000
959	JUNCTION	96.00	7.019	0.000
960	JUNCTION	96.00	7.323	0.000
961	JUNCTION	96.00	7.596	0.000
962	JUNCTION	96.00	7.786	0.000
963	JUNCTION	96.00	8.448	0.000
964	JUNCTION	96.00	8.386	0.000
965	JUNCTION	96.00	8.533	0.000
9914	JUNCTION	96.00	8.154	0.000
9915	JUNCTION	96.00	11.407	0.000
9916	JUNCTION	96.00	4.569	0.000
DundasFM_2	JUNCTION	93.36	1.435	0.000
DundasFM_3	JUNCTION	93.36	1.405	0.000
EastFM_1	JUNCTION	96.00	9.652	0.000
EastFM_2	JUNCTION	96.00	1.729	0.000

****
Node Flooding Summary
****

Flooding refers to all water that overflows a node, whether it ponds or not.

Node	Hours Flooded	Maximum Rate CMS	Time of Max Occurrence days hr:min	Total Flood Volume 10^6 ltr	Maximum Ponded Depth Meters
2273	0.01	0.155	0 00:02	0.000	6.451
2275	0.01	0.025	0 00:02	0.000	8.540
2277	0.01	0.342	0 00:00	0.001	15.532
2278	0.01	0.023	0 00:00	0.000	8.097

430	0.01	0.138	0	00:00	0.000	9.338
2282	5.18	0.058	0	17:26	0.748	0.000
2313	7.92	0.079	0	15:04	1.518	0.000
2321	69.23	0.130	0	13:40	11.598	0.000
285	1.34	0.025	0	15:44	0.057	0.000
288	3.93	0.069	0	16:05	0.659	0.000
414	14.97	0.221	0	17:35	9.376	0.000
427	11.16	0.198	0	17:45	5.664	0.000
511	5.87	0.039	0	16:25	0.539	0.000

****
Storage Volume Summary
****

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days	hr:min	Maximum Outflow CMS
1005	0.000	3.2	0.0	0.0	0.001	16.2	0	18:30	0.047
1007	0.000	3.2	0.0	0.0	0.001	16.0	0	18:30	0.048
1008	0.000	3.9	0.0	0.0	0.002	17.9	0	18:30	0.134
1020	0.000	5.5	0.0	0.0	0.002	25.5	0	18:30	0.134
1022	0.000	5.6	0.0	0.0	0.002	26.1	0	18:30	0.135
1023	0.001	7.3	0.0	0.0	0.003	34.5	0	18:30	0.136
1024	0.001	7.6	0.0	0.0	0.003	35.5	0	18:28	0.136
1025	0.001	10.7	0.0	0.0	0.003	49.8	0	18:22	0.136
1026	0.001	11.0	0.0	0.0	0.003	52.1	0	18:21	0.168
1029	0.000	4.9	0.0	0.0	0.002	27.2	0	18:21	0.073
1030	0.000	5.3	0.0	0.0	0.002	28.2	0	18:21	0.056
1031	0.001	8.4	0.0	0.0	0.003	43.8	0	18:21	0.032
1042	0.000	2.4	0.0	0.0	0.001	12.4	0	18:20	0.024
1044	0.000	1.2	0.0	0.0	0.000	1.8	0	17:10	0.015
1045	0.000	1.1	0.0	0.0	0.000	1.7	0	17:10	0.018
1049	0.064	28.6	0.0	0.0	0.164	73.0	0	18:20	1.223
1051	0.007	22.6	0.0	0.0	0.007	24.2	0	15:36	2.854
106	0.000	1.4	0.0	0.0	0.000	2.3	0	13:50	0.011
107	0.000	0.8	0.0	0.0	0.000	1.5	0	13:50	0.010
1085	0.000	3.6	0.0	0.0	0.000	4.3	0	13:25	0.074
1090	0.000	3.6	0.0	0.0	0.000	4.4	0	13:25	0.071
1091	0.000	4.6	0.0	0.0	0.000	5.6	0	13:25	0.071
1092	0.000	5.5	0.0	0.0	0.000	6.4	0	13:25	0.072
1093	0.000	6.2	0.0	0.0	0.000	7.3	0	13:25	0.070
1096	0.000	4.2	0.0	0.0	0.000	5.2	0	13:25	0.061
1101	0.000	5.0	0.0	0.0	0.000	6.0	0	13:23	0.059
1111	0.000	3.7	0.0	0.0	0.000	4.6	0	13:21	0.056
1114	0.000	6.5	0.0	0.0	0.000	7.4	0	13:21	0.057
1115	0.000	4.8	0.0	0.0	0.000	5.6	0	13:22	0.057
1116	0.000	3.3	0.0	0.0	0.000	4.0	0	13:23	0.057
1117	0.000	4.7	0.0	0.0	0.000	5.7	0	13:20	0.055
112	0.000	0.4	0.0	0.0	0.000	0.7	0	13:50	0.002
1131	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1185	0.001	13.3	0.0	0.0	0.002	42.0	0	17:59	0.239
1186	0.001	13.0	0.0	0.0	0.002	42.4	0	17:59	0.242
1187	0.001	9.3	0.0	0.0	0.002	28.5	0	17:57	0.245
1190	0.001	12.3	0.0	0.0	0.003	35.7	0	17:57	0.248
1191	0.001	14.2	0.0	0.0	0.003	36.2	0	17:52	0.250
1192	0.000	4.4	0.0	0.0	0.000	4.8	1	12:50	0.236
1193	0.000	5.8	0.0	0.0	0.000	6.3	1	12:50	0.236
1195	0.000	4.6	0.0	0.0	0.000	5.0	1	12:51	0.236
1196	0.000	3.7	0.0	0.0	0.000	4.0	1	12:52	0.237
1199	0.000	5.1	0.0	0.0	0.001	14.4	0	17:59	0.238
1202	0.000	6.0	0.0	0.0	0.000	6.5	1	12:50	0.234
1203	0.000	5.2	0.0	0.0	0.000	5.6	1	12:50	0.232
1204	0.000	3.6	0.0	0.0	0.000	3.9	1	12:50	0.230
1205	0.000	3.3	0.0	0.0	0.000	3.6	1	12:50	0.228
1206	0.000	3.9	0.0	0.0	0.000	4.2	1	12:50	0.226
1208	0.000	7.8	0.0	0.0	0.000	8.3	1	12:50	0.201
1209	0.000	7.8	0.0	0.0	0.000	8.3	1	12:50	0.202
1210	0.000	5.6	0.0	0.0	0.000	6.1	1	12:50	0.220
1211	0.000	5.1	0.0	0.0	0.000	5.5	1	12:50	0.221
1212	0.000	5.5	0.0	0.0	0.000	5.9	1	12:50	0.225
1216	0.000	1.5	0.0	0.0	0.000	1.8	1	12:50	0.009
1217	0.000	1.6	0.0	0.0	0.000	1.8	1	12:50	0.014
1218	0.000	1.2	0.0	0.0	0.000	1.4	1	12:50	0.015
1219	0.000	1.0	0.0	0.0	0.000	1.2	1	12:50	0.016
1220	0.000	1.1	0.0	0.0	0.000	1.3	1	12:50	0.017
1221	0.000	1.8	0.0	0.0	0.000	2.1	1	12:50	0.018
1222	0.000	0.9	0.0	0.0	0.000	1.0	1	12:50	0.005
1241	0.000	1.4	0.0	0.0	0.000	1.6	1	12:50	0.006
1242	0.000	1.6	0.0	0.0	0.000	1.9	1	12:50	0.012
1243	0.000	7.2	0.0	0.0	0.000	7.6	1	12:50	0.018
1244	0.000	2.9	0.0	0.0	0.000	3.3	1	12:50	0.024
1245	0.000	3.4	0.0	0.0	0.000	3.9	1	12:50	0.030
1246	0.000	3.5	0.0	0.0	0.000	4.1	1	12:50	0.036
1247	0.000	4.2	0.0	0.0	0.000	5.0	1	12:50	0.042
1248	0.000	3.9	0.0	0.0	0.000	4.7	1	12:50	0.049
1249	0.000	4.9	0.0	0.0	0.000	5.8	1	12:50	0.055
1252	0.000	3.5	0.0	0.0	0.000	4.2	1	12:50	0.061
1253	0.000	3.3	0.0	0.0	0.000	3.9	1	12:50	0.061
1286	0.000	3.9	0.0	0.0	0.000	4.5	1	12:50	0.062
1287	0.000	2.9	0.0	0.0	0.000	3.4	1	12:50	0.062
1288	0.000	4.6	0.0	0.0	0.000	5.5	1	12:50	0.063
1289	0.000	3.3	0.0	0.0	0.000	3.9	1	12:50	0.063
1290	0.000	2.5	0.0	0.0	0.000	2.9	1	12:51	0.064
1291	0.001	8.4	0.0	0.0	0.001	10.0	0	15:53	0.679
1292	0.001	7.0	0.0	0.0	0.001	8.3	0	15:54	0.679
1293	0.000	6.7	0.0	0.0	0.001	7.9	0	15:54	0.679
1294	0.001	6.6	0.0	0.0	0.001	7.8	0	15:55	0.680
1295	0.001	8.4	0.0	0.0	0.001	10.0	0	15:56	0.680
1296	0.001	8.3	0.0	0.0	0.001	9.8	0	15:57	0.681
1297	0.000	12.9	0.0	0.0	0.001	15.2	0	15:57	0.681
1298	0.001	8.6	0.0	0.0	0.001	10.2	0	15:58	0.682
1299	0.001	8.0	0.0	0.0	0.001	9.4	0	15:58	0.687
1303	0.001	6.2	0.0	0.0	0.001	7.4	0	17:26	0.687
1306	0.001	8.2	0.0	0.0	0.001	10.5	0	17:44	0.687
1307	0.001	8.9	0.0	0.0	0.001	16.2	0	17:48	0.687
1308	0.000	7.2	0.0	0.0	0.001	18.7	0	17:50	0.687
1309	0.001	10.3	0.0	0.0	0.002	30.5	0	17:50	0.694
1310	0.001	12.8	0.0	0.0	0.003	37.3	0	17:49	0.695
1344	0.000	1.8	0.0	0.0	0.000	2.7	0	16:50	0.049
1345	0.000	1.8	0.0	0.0	0.000	2.8	0	17:00	0.050
1346	0.000	2.1	0.0	0.0	0.000	3.1	0	17:00	0.052
1347	0.000	1.8	0.0	0.0	0.000	2.7	0	17:00	0.060
1348	0.000	1.5	0.0	0.0	0.000	2.3	0	17:00	0.063
135	0.000	0.4	0.0	0.0	0.000	0.6	0	13:50	0.002
1352	0.000	2.0	0.0	0.0	0.000	3.1	0	17:01	0.065
136	0.000	0.6	0.0	0.0	0.000	0.9	0	13:50	0.001
137	0.000	0.3	0.0	0.0	0.000	0.5	0	13:50	0.001
138	0.000	3.6	0.0	0.0	0.000	8.9	0	13:55	0.110
1511	0.000	4.8	0.0	0.0	0.000	5.6	0	13:50	0.028
1514	0.000	4.4	0.0	0.0	0.000	5.0	0	13:50	0.029
157	0.000	4.6	0.0	0.0	0.001	29.3	0	15:44	0.160
158	0.000	0.2	0.0	0.0	0.000	13.6	0	15:44	0.033
159	0.000	4.3	0.0	0.0	0.001	29.3	0	15:44	0.250
1593	0.000	2.4	0.0	0.0	0.000	2.8	0	13:50	0.035
161	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
162	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
163	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
164	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
165	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
166	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
167	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
168	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
169	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
170	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1705	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
171	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1718	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1719	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
172	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1720	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1721	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1725	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
173	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
174	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1742	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1743	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1745	0.000	6.1	0.0	0.0	0.000	7.4	0	13:25	0.077
1746	0.000	4.6	0.0	0.0	0.000	5.6	0	13:25	0.080
1747	0.000	6.7	0.0	0.0	0.000	8.6	0	13:25	0.080
1748	0.000	7.2	0.0	0.0	0.000	8.8	0	13:26	0.080
1749	0.000	5.1	0.0	0.0	0.000	6.2	0	13:28	0.082
175	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1750	0.000	3.8	0.0	0.0	0.000	4.7	0	13:29	0.084
1754	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1755	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1756	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1757	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1758	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1759	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1763	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1768	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1769	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1770	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
1771	0.000	2.6	0.0	0.0	0.000	3.2	0	13:40	0.109
1772	0.000	3.3	0.0	0.0	0.000	4.0	0	13:30	0.087
1773	0.000	2.9	0.0	0.0	0.000	3.6	0	13:31	0.089
1774	0.000	2.7	0.0	0.0	0.000	3.3	0	13:41	0.112
1794	0.000	5.4	0.0	0.0	0.000	6.7	0	13:42	0.114
1795	0.000	8.8	0.0	0.0	0.000	11.1	0	13:44	0.116
1796	0.000	8.8	0.0	0.0	0.000	10.6	0	13:45	0.149
1797	0.000	14.6	0.0	0.0	0.000	17.7	0	13:46	0.150
1798	0.000	4.2	0.0	0.0	0.000	5.2	0	13:48	0.150
1799	0.000	6.6	0.0	0.0	0.000	8.0	0	13:49	0.151
1800	0.000	5.9	0.0	0.0	0.000	7.4	0	13:51	0.152
1801	0.000	8.8	0.0	0.0	0.000	10.7	0	13:50	0.152
1812	0.000	5.0	0.0	0.0	0.000	6.0	0	13:50	0.172
1866	0.000	4.5	0.0	0.0	0.000	5.6	0	13:50	0.173
1867	0.000	6.0	0.0	0.0	0.000	7.1	0	13:51	0.173
1868	0.000	3.8	0.0	0.0	0.000	4.6	0	13:51	0.174
1869	0.000	5.3	0.0	0.0	0.000	6.5	0	13:53	0.174
1870	0.000	4.0	0.0	0.0	0.000	4.9	0	13:54	0.175
1871	0.000	3.6	0.0	0.0	0.000	4.4	0	13:55	0.176
1872	0.000	3.4	0.0	0.0	0.000	4.3	0	13:58	0.176
1873	0.000	5.4	0.0	0.0	0.001	6.4	0	13:58	0.227
1874	0.000	3.9	0.0	0.0	0.000	4.6	0	13:59	0.227
1875	0.000	2.9	0.0	0.0	0.000	3.5	0	14:00	0.228
1876	0.000	3.0	0.0	0.0	0.001	4.6	0	00:00	0.228
1877	0.000	3.6	0.0	0.0	0.000	4.3	0	13:50	0.035
1880	0.000	6.9	0.0	0.0	0.000	8.2	0	13:50	0.040
1881	0.000	8.7	0.0	0.0	0.000	10.2	0	13:51	0.041
1898	0.000	3.5	0.0	0.0	0.000	8.2	0	12:50	0.027
1899	0.000	3.6	0.0	0.0	0.000	8.4	0	12:49	0.053
1913	0.000	5.4	0.0	0.0	0.000	12.2	0	12:49	0.079
1914	0.000	5.0	0.0	0.0	0.000	11.9	0	12:42	0.083
1915	0.000	6.3	0.0	0.0	0.000	15.6	0	12:44	0.114
1916	0.000	4.9	0.0	0.0	0.000	12.5	0	12:50	0.137
1917	0.000	3.1	0.0	0.0	0.000	8.4	0	12:50	0.159
1918	0.000	2.8	0.0	0.0	0.000	5.7	0	12:50	0.160
1919	0.000	2.5	0.0	0.0	0.000	5.7	0	12:50	0.160
1920	0.000	3.5	0.0	0.0	0.000	4.2	0	17:00	0.003
1923	0.000	2.0	0.0	0.0	0.000	2.8	0	17:00	0.008
1927	0.000	1.4	0.0	0.0	0.000	2.1	0	17:10	0.012
1931	0.000	2.2	0.0	0.0	0.000	4.8	0	12:50	0.160
1932	0.000	2.1	0.0	0.0	0.000	4.6	0	12:55	0.165
1933	0.000	1.9	0.0	0.0	0.001	9.7	0	00:00	0.358
1938	0.000	3.0	0.0	0.0	0.001	7.3	0	00:00	0.390
1939	0.000	3.6	0.0	0.0	0.001	7.6	0	00:00	0.268
1940	0.000	2.8	0.0	0.0	0.001	6.3	0	00:00	0.339
1941	0.000	4.2	0.0	0.0	0.001	10.7	0	00:00	0.571

1942	0.026	21.0	0.0	0.0	0.032	26.4	0	00:01	0.547
1943	0.000	0.4	0.0	0.0	0.000	0.6	0	17:00	0.001
1968	0.000	3.5	0.0	0.0	0.000	4.1	0	13:50	0.030
1969	0.000	2.9	0.0	0.0	0.000	3.4	0	13:50	0.029
1970	0.000	3.2	0.0	0.0	0.000	3.8	0	13:50	0.028
2029	0.000	2.8	0.0	0.0	0.000	4.2	0	13:13	0.022
2030	0.000	2.4	0.0	0.0	0.000	3.4	0	13:12	0.020
2031	0.000	2.6	0.0	0.0	0.000	3.6	0	13:10	0.020
2032	0.000	6.4	0.0	0.0	0.000	7.7	0	13:15	0.053
2033	0.000	2.0	0.0	0.0	0.000	2.9	0	13:08	0.015
2034	0.000	2.1	0.0	0.0	0.000	3.0	0	13:05	0.014
2035	0.000	1.6	0.0	0.0	0.000	2.3	0	13:05	0.014
2036	0.000	2.0	0.0	0.0	0.000	2.8	0	13:05	0.013
2061	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
2062	0.001	21.2	0.0	0.0	0.003	82.5	0	16:05	0.216
2063	0.001	16.4	0.0	0.0	0.003	81.2	0	16:05	0.343
2096	0.000	4.5	0.0	0.0	0.000	6.8	0	17:04	0.069
2097	0.000	2.6	0.0	0.0	0.000	4.0	0	17:03	0.066
2105	0.001	13.5	0.0	0.0	0.005	71.7	0	20:55	0.303
211	0.000	5.8	0.0	0.0	0.000	13.2	0	13:18	0.087
212	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
213	0.000	20.9	0.0	0.0	0.000	46.4	0	13:23	0.096
2140	0.000	3.5	0.0	0.0	0.000	6.0	0	13:50	0.065
2140_1	0.000	2.2	0.0	0.0	0.000	4.3	0	13:50	0.044
2140_2	0.000	1.7	0.0	0.0	0.000	3.3	0	13:50	0.033
2140_3	0.000	1.5	0.0	0.0	0.000	2.9	0	13:50	0.022
2140_4	0.000	1.0	0.0	0.0	0.000	2.0	0	13:50	0.011
2141	0.001	22.7	0.0	0.0	0.006	100.0	0	20:49	0.269
2146	0.000	4.5	0.0	0.0	0.000	5.3	1	17:10	0.062
2147	0.000	3.7	0.0	0.0	0.000	4.3	1	12:50	0.041
2148	0.000	3.8	0.0	0.0	0.000	4.3	1	12:50	0.021
2154	0.000	10.3	0.0	0.0	0.003	73.6	0	16:05	0.007
2155	0.001	9.3	0.0	0.0	0.004	56.7	0	16:05	0.009
216	0.000	16.2	0.0	0.0	0.000	36.6	0	13:24	0.117
2176	0.000	3.5	0.0	0.0	0.000	4.3	0	13:19	0.055
2177	0.000	5.9	0.0	0.0	0.000	7.0	0	13:17	0.055
2178	0.000	4.7	0.0	0.0	0.000	5.7	0	13:16	0.055
2179	0.000	6.1	0.0	0.0	0.000	7.4	0	13:15	0.055
2180	0.000	7.2	0.0	0.0	0.000	9.0	0	13:15	0.054
2217	0.001	9.7	0.0	0.0	0.004	49.6	0	20:50	0.383
2218	0.001	12.6	0.0	0.0	0.004	57.1	0	20:50	0.384
2219	0.001	13.8	0.0	0.0	0.004	54.4	0	20:48	0.390
222	0.000	12.2	0.0	0.0	0.000	26.0	0	13:25	0.135
2220	0.001	7.5	0.0	0.0	0.003	33.5	0	20:35	0.404
2221	0.001	7.9	0.0	0.0	0.003	35.9	0	20:41	0.398
2222	0.001	6.1	0.0	0.0	0.002	25.9	0	20:18	0.415
2223	0.001	7.7	0.0	0.0	0.002	31.3	0	20:10	0.417
2224	0.000	6.6	0.0	0.0	0.002	25.3	0	19:56	0.427
2259	0.001	9.2	0.0	0.0	0.004	48.2	0	20:51	0.313
2264	0.000	0.1	0.0	0.0	0.000	1.7	0	18:01	0.038
2265	0.000	3.4	0.0	0.0	0.001	20.2	0	16:36	0.079
2266	0.001	9.2	0.0	0.0	0.002	37.4	0	17:44	0.078
2267	0.003	36.0	0.0	0.0	0.005	57.6	0	17:44	0.078
2268	0.000	1.7	0.0	0.0	0.000	3.7	0	13:05	0.044
2269	0.000	1.0	0.0	0.0	0.001	13.1	0	17:39	0.024
2270	0.001	11.2	0.0	0.0	0.002	30.1	0	17:38	0.025
2282	0.006	33.2	0.0	0.0	0.018	100.0	0	15:38	1.062
2282_1	0.006	30.9	0.0	0.0	0.018	96.7	0	18:20	1.054
2282_2	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
2286	0.000	4.4	0.0	0.0	0.000	5.2	0	13:52	0.041
2300	0.001	9.4	0.0	0.0	0.001	11.8	0	15:11	0.640
2301	0.001	10.8	0.0	0.0	0.001	17.5	0	15:10	0.640
2302	0.001	11.3	0.0	0.0	0.001	19.2	0	15:10	0.639
2303	0.001	15.3	0.0	0.0	0.001	29.5	0	15:10	0.639
2304	0.001	15.7	0.0	0.0	0.001	30.6	0	15:10	0.639
2305	0.001	9.9	0.0	0.0	0.002	23.3	0	15:08	0.638
2306	0.001	9.0	0.0	0.0	0.002	23.6	0	15:07	0.636
2307	0.001	12.1	0.0	0.0	0.002	33.6	0	15:06	0.634
2309	0.001	11.7	0.0	0.0	0.003	35.6	0	15:05	0.619
231	0.000	25.7	0.0	0.0	0.000	55.7	0	13:25	0.148
2310	0.001	17.4	0.0	0.0	0.003	55.7	0	15:04	0.616
2311	0.001	22.9	0.0	0.0	0.003	62.2	0	15:04	0.614
2312	0.001	16.7	0.0	0.0	0.003	63.5	0	15:04	0.612
2313	0.001	65.5	0.0	0.0	0.002	100.0	0	12:58	0.310
2314	0.002	38.8	0.0	0.0	0.002	53.0	0	14:10	0.303
2315	0.002	53.6	0.0	0.0	0.003	67.2	0	14:10	0.299
2317	0.003	65.5	0.0	0.0	0.004	77.0	0	14:10	0.296
2318	0.002	49.1	0.0	0.0	0.003	61.0	0	14:10	0.297
2319	0.003	71.0	0.0	0.0	0.004	84.0	0	14:10	0.301
2320	0.004	55.5	0.0	0.0	0.004	62.6	0	14:10	0.306
2321	0.005	91.3	0.0	0.0	0.005	100.0	0	06:31	0.313
2341	0.000	14.8	0.0	0.0	0.003	85.6	0	15:12	0.390
2342	0.000	10.2	0.0	0.0	0.003	69.2	0	15:12	0.271
2343	0.000	8.9	0.0	0.0	0.003	62.0	0	15:11	0.252
2344	0.000	9.9	0.0	0.0	0.003	69.8	0	15:10	0.232
2345	0.000	9.6	0.0	0.0	0.003	70.8	0	15:10	0.212
2346	0.000	8.1	0.0	0.0	0.003	64.9	0	15:10	0.192
2347	0.000	6.4	0.0	0.0	0.002	53.7	0	15:10	0.172
2348	0.000	4.6	0.0	0.0	0.002	35.6	0	14:55	0.155
2349	0.000	3.0	0.0	0.0	0.002	33.2	0	14:55	0.075
236	0.000	6.0	0.0	0.0	0.000	12.1	0	13:25	0.159
2363	0.001	11.8	0.0	0.0	0.004	73.3	0	21:10	0.180
2364	0.001	11.5	0.0	0.0	0.004	74.0	0	21:10	0.185
2365	0.001	11.3	0.0	0.0	0.004	71.7	0	21:11	0.191
2366	0.001	11.4	0.0	0.0	0.004	73.2	0	21:16	0.196
2367	0.001	13.1	0.0	0.0	0.004	84.7	0	21:19	0.200
2368	0.001	13.1	0.0	0.0	0.004	85.3	0	21:19	0.193
2369	0.001	11.9	0.0	0.0	0.004	76.6	0	21:19	0.189
2370	0.001	14.0	0.0	0.0	0.003	91.1	0	21:20	0.187
2371	0.001	14.2	0.0	0.0	0.003	92.1	0	21:20	0.182
2372	0.000	12.9	0.0	0.0	0.003	82.3	0	21:19	0.179
2373	0.000	6.5	0.0	0.0	0.003	42.6	0	21:17	0.175
2374	0.000	6.8	0.0	0.0	0.003	44.4	0	21:15	0.171
2375	0.000	8.2	0.0	0.0	0.003	52.5	0	21:13	0.167
2376	0.000	8.5	0.0	0.0	0.002	54.1	0	21:10	0.162
2377	0.000	5.7	0.0	0.0	0.002	35.5	0	21:10	0.157
2378	0.000	8.1	0.0	0.0	0.002	48.3	0	21:06	0.153
2379	0.000	6.8	0.0	0.0	0.002	39.1	0	21:04	0.147
2380	0.000	7.2	0.0	0.0	0.002	38.8	0	21:03	0.142
2381	0.000	5.5	0.0	0.0	0.001	28.6	0	20:59	0.136
2382	0.000	4.7	0.0	0.0	0.001	20.5	0	20:56	0.131
2383	0.000	5.5	0.0	0.0	0.001	22.9	0	20:55	0.126
2384	0.000	4.9	0.0	0.0	0.001	14.1	0	20:52	0.121
2385	0.000	3.7	0.0	0.0	0.000	7.1	0	20:51	0.116
2386	0.000	3.3	0.0	0.0	0.000	5.4	0	14:25	0.054
2387	0.000	2.8	0.0	0.0	0.000	4.7	0	14:25	0.048
2388	0.000	2.0	0.0	0.0	0.000	3.3	0	14:25	0.043
2389	0.000	2.0	0.0	0.0	0.000	3.2	0	14:25	0.038
2390	0.000	2.4	0.0	0.0	0.000	3.9	0	14:25	0.032
2391	0.000	1.9	0.0	0.0	0.000	3.2	0	14:25	0.027
2392	0.000	2.0	0.0	0.0	0.000	3.3	0	14:25	0.022
2393	0.000	1.9	0.0	0.0	0.000	3.1	0	14:25	0.016
2394	0.000	1.7	0.0	0.0	0.000	2.9	0	14:25	0.011
2395	0.000	1.2	0.0	0.0	0.000	2.0	0	14:25	0.005
2397	0.000	2.7	0.0	0.0	0.000	4.9	0	14:25	0.057
2398	0.000	2.6	0.0	0.0	0.000	4.4	0	14:25	0.047
2399	0.000	1.5	0.0	0.0	0.000	2.6	0	14:25	0.038
2400	0.000	1.4	0.0	0.0	0.000	2.3	0	14:25	0.028
2401	0.000	1.8	0.0	0.0	0.000	3.1	0	14:25	0.019
2402	0.000	1.4	0.0	0.0	0.000	2.4	0	14:25	0.009
2453	0.001	13.6	0.0	0.0	0.003	49.8	0	20:47	0.392
2474	0.001	15.4	0.0	0.0	0.006	79.4	0	17:35	0.207
2475	0.001	14.6	0.0	0.0	0.006	72.5	0	17:35	0.211
2476	0.001	13.0	0.0	0.0	0.006	61.8	0	17:35	0.215
2477	0.001	17.3	0.0	0.0	0.006	80.4	0	17:35	0.218
284	0.001	15.8	0.0	0.0	0.003	87.3	0	15:44	0.240
285	0.001	16.7	0.0	0.0	0.003	100.0	0	15:22	0.231
286	0.001	13.4	0.0	0.0	0.003	77.8	0	15:42	0.219
287	0.001	13.6	0.0	0.0	0.005	65.0	0	15:24	0.218
288	0.001	20.8	0.0	0.0	0.005	100.0	0	15:17	0.186
289	0.001	14.6	0.0	0.0	0.005	65.1	0	16:05	0.178
290	0.001	17.1	0.0	0.0	0.005	77.5	0	16:05	0.191
300	0.000	15.3	0.0	0.0	0.000	31.0	0	13:15	0.061
3000	0.000	2.1	0.0	0.0	0.000	3.1	0	18:23	0.080
3000A	0.000	2.4	0.0	0.0	0.000	3.6	0	18:27	0.080
301	0.000	7.4	0.0	0.0	0.000	14.9	0	13:15	0.071
302	0.000	12.0	0.0	0.0	0.000	23.5	0	13:15	0.028
303	0.000	16.0	0.0	0.0	0.000	32.1	0	13:15	0.052
360	0.000	3.2	0.0	0.0	0.001	12.7	0	17:50	0.066
401	0.001	17.8	0.0	0.0	0.006	81.2	0	16:15	0.210
402	0.001	21.2	0.0	0.0	0.006	94.1	0	16:15	0.238
403	0.001	15.3	0.0	0.0	0.006	67.0	0	16:35	0.239
404	0.002	14.5	0.0	0.0	0.007	62.4	0	17:00	0.238
405	0.002	15.8	0.0	0.0	0.007	63.7	0	17:10	0.237
406	0.002	23.2	0.0	0.0	0.007	82.1	0	17:26	1.030
409	0.002	18.0	0.0	0.0	0.007	72.0	0	17:37	0.810
411	0.002	16.1	0.0	0.0	0.007	65.4	0	17:36	0.805
413	0.001	18.2	0.0	0.0	0.006	85.1	0	17:25	0.222
414	0.001	22.2	0.0	0.0	0.006	100.0	0	14:55	0.149
418	0.001	15.3	0.0	0.0	0.005	67.8	0	17:38	0.862
419	0.001	17.4	0.0	0.0	0.005	85.5	0	17:35	0.204
421	0.001	19.0	0.0	0.0	0.006	78.4	0	17:37	0.837
424	0.001	11.3	0.0	0.0	0.005	56.2	0	17:43	0.198
425	0.001	15.4	0.0	0.0	0.006	71.2	0	17:44	0.198
426	0.002	19.7	0.0	0.0	0.007	81.8	0	17:44	0.198
427	0.002	23.6	0.0	0.0	0.006	100.0	0	15:07	0.270
428	0.001	12.8	0.0	0.0	0.004	71.6	0	17:39	0.195
429	0.001	16.3	0.0	0.0	0.005	82.2	0	17:41	0.197
431	0.001	16.0	0.0	0.0	0.005	85.7	0	17:35	0.145
432	0.001	12.7	0.0	0.0	0.005	71.4	0	17:35	0.143
433	0.001	12.8	0.0	0.0	0.004	49.8	0	17:36	0.198
434	0.001	12.6	0.0	0.0	0.004	49.8	0	17:39	0.205
435	0.000	14.8	0.0	0.0	0.000	29.8	0	12:56	0.170
436	0.001	20.5	0.0	0.0	0.004	81.9	0	16:25	0.343
437	0.001	13.9	0.0	0.0	0.005	51.6	0	17:45	0.899
438	0.001	6.7	0.0	0.0	0.003	44.6	0	17:45	0.150
439	0.001	16.7	0.0	0.0	0.004	67.5	0	17:39	0.895
44	0.000	3.4	0.0	0.0	0.000	5.3	0	13:50	0.068
446	0.000	1.5	0.0	0.0	0.001	16.9	0	17:45	0.003
447	0.000	2.0	0.0	0.0	0.001	20.1	0	17:45	0.022
448	0.000	4.3	0.0	0.0	0.002	38.9	0	17:45	0.024
449	0.001	12.0	0.0	0.0	0.004	50.7	0	17:48	0.572
45	0.000	3.2	0.0	0.0	0.000	5.6	0	13:50	0.095
451	0.001	7.6	0.0	0.0	0.003	47.8	0	17:37	0.112
452	0.001	11.7	0.0	0.0	0.004	49.5	0	17:36	0.110
453	0.001	8.1	0.0	0.0	0.003	47.1	0	17:36	0.188
454	0.001	8.6	0.0	0.0	0.004	48.7	0	17:37	0.176
455	0.000	3.9	0.0	0.0	0.002	24.9	0	18:06	0.064
456	0.000	0.4	0.0	0.0	0.000	7.4	0	17:47	0.018
457	0.002	18.5	0.0	0.0	0.004	43.8	0	18:10	0.596
458	0.002	27.4	0.0	0.0	0.004	57.1	0	17:58	0.597
459	0.000	4.6	0.0	0.0	0.003	34.4	0	17:58	0.038
460	0.001	10.0	0.0	0.0	0.004	45.4	0	17:55	0.570
461	0.000	4.3	0.0	0.0	0.003	33.0	0	17:45	0.038
462	0.000	5.5	0.0	0.0	0.003	34.0	0	17:35	0.082
463	0.000	8.8	0.0	0.0	0.003	61.8	0	17:38	0.083
464	0.000	7.8	0.0	0.0	0.003	51.9	0	17:38	0.085
465	0.001	7.8	0.0	0.0	0.003	40.8	0	17:35	0.216
468	0.001	21.4	0.0	0.0	0.004	63.5	0	18:30	0.563
469	0.001	18.0	0.0	0.0	0.004	58.5	0	18:35	0.554
473	0.002	18.6	0.0	0.0	0.004	47.7	0	18:24	0.564
477	0.001	10.8	0.0	0.0	0.003	51.7	0	18:50	0.548
478	0.001	8.6	0.0	0.0	0.003	45.0	0	18:40	0.551
479	0.000	6.8	0.0	0.0	0.002	29.5	0	19:20	0.539
480	0.001	8.0	0.0	0.0	0.002	29.3	0	19:05	0.542
481	0.001	9.1	0.0	0.0	0.003	43.6	0	18:58	0.545
501	0.001	21.8	0.0	0.0	0.004	62.7	0	17:25	0.210
502	0.001	20.9	0.0	0.0	0.004	56.2	0	17:25	0.213
503	0.002	19.0	0.0	0.0	0.003	40.1	0	17:35	0.217
506	0.001	13.3	0.0	0.0	0.003	54.3	0	17:25	0.174
507	0.001	12.0	0.0	0.0	0.004	81.8	0	17:28	0.157
508	0.001	11.6	0.0	0.0	0.004	65.4	0	17:25	0.160

51	0.000	3.6	0.0	0.0	0.000	6.2	0	13:50	0.102
511	0.001	14.9	0.0	0.0	0.006	100.0	0	13:12	0.185
512	0.001	10.9	0.0	0.0	0.005	74.9	0	17:35	0.154
513	0.000	8.5	0.0	0.0	0.004	74.1	0	17:35	0.020
514	0.000	5.7	0.0	0.0	0.004	51.9	0	17:35	0.019
516	0.001	10.1	0.0	0.0	0.006	83.6	0	15:35	0.040
521	0.000	5.7	0.0	0.0	0.004	51.4	0	17:35	0.017
54	0.000	3.3	0.0	0.0	0.000	5.6	0	13:50	0.104
55_1	0.000	3.0	0.0	0.0	0.000	5.4	0	13:50	0.106
553	0.001	13.1	0.0	0.0	0.004	82.4	0	21:05	0.203
554	0.001	12.3	0.0	0.0	0.005	71.0	0	21:05	0.247
555	0.001	9.9	0.0	0.0	0.005	59.8	0	21:05	0.247
556	0.001	9.8	0.0	0.0	0.005	54.9	0	21:05	0.247
56	0.000	3.4	0.0	0.0	0.000	6.0	0	13:50	0.107
563	0.001	11.8	0.0	0.0	0.005	71.7	0	21:05	0.246
63	0.000	3.6	0.0	0.0	0.000	6.4	0	13:51	0.109
64	0.000	4.2	0.0	0.0	0.000	7.2	0	13:53	0.111
649	0.001	9.8	0.0	0.0	0.005	52.2	0	21:03	0.249
65	0.000	2.9	0.0	0.0	0.000	4.8	0	13:53	0.112
65_1	0.000	2.0	0.0	0.0	0.000	3.9	0	13:53	0.112
650	0.001	12.7	0.0	0.0	0.005	63.4	0	20:59	0.296
652	0.001	9.8	0.0	0.0	0.005	55.2	0	20:57	0.297
653	0.001	11.7	0.0	0.0	0.005	67.0	0	20:57	0.300
654	0.001	13.5	0.0	0.0	0.005	72.8	0	20:56	0.302
66	0.017	15.4	0.0	0.0	0.022	20.4	0	16:51	0.245
666	0.000	6.5	0.0	0.0	0.003	57.4	0	20:55	0.011
667	0.000	7.1	0.0	0.0	0.003	58.6	0	20:55	0.021
668	0.000	5.7	0.0	0.0	0.004	44.2	0	20:55	0.033
669	0.001	6.3	0.0	0.0	0.004	46.5	0	21:03	0.043
670	0.001	8.7	0.0	0.0	0.004	62.4	0	21:02	0.045
671	0.001	11.2	0.0	0.0	0.004	78.6	0	20:58	0.045
672	0.001	9.6	0.0	0.0	0.004	67.9	0	20:58	0.050
673	0.001	10.0	0.0	0.0	0.004	52.6	0	20:54	0.307
675	0.001	12.1	0.0	0.0	0.004	63.0	0	20:54	0.309
676	0.001	9.2	0.0	0.0	0.004	48.8	0	20:52	0.312
678	0.001	9.0	0.0	0.0	0.004	45.9	0	20:50	0.381
68	0.000	1.1	0.0	0.0	0.000	2.0	0	13:50	0.025
682	0.000	5.3	0.0	0.0	0.002	37.4	0	20:45	0.090
684	0.000	5.0	0.0	0.0	0.002	31.2	0	20:45	0.092
685	0.001	9.9	0.0	0.0	0.004	50.1	0	20:50	0.382
686	0.001	12.5	0.0	0.0	0.004	56.5	0	20:50	0.387
689	0.001	12.8	0.0	0.0	0.004	52.5	0	20:50	0.389
690	0.001	20.3	0.0	0.0	0.003	69.1	0	20:45	0.395
708	0.000	4.8	0.0	0.0	0.002	29.9	0	20:35	0.090
780	0.001	14.6	0.0	0.0	0.003	44.7	0	20:43	0.397
781	0.001	9.4	0.0	0.0	0.003	40.6	0	20:35	0.406
782	0.001	9.4	0.0	0.0	0.002	40.7	0	20:25	0.409
783	0.001	8.2	0.0	0.0	0.002	30.7	0	20:20	0.413
796	0.000	2.9	0.0	0.0	0.000	4.8	0	14:25	0.054
852	0.000	3.3	0.0	0.0	0.000	5.4	0	14:22	0.057
853	0.000	2.7	0.0	0.0	0.000	4.4	0	14:24	0.060
859	0.000	2.8	0.0	0.0	0.000	4.6	0	14:24	0.069
860	0.000	2.5	0.0	0.0	0.000	4.2	0	14:25	0.063
861	0.000	2.4	0.0	0.0	0.000	4.0	0	14:25	0.066
864	0.000	2.8	0.0	0.0	0.000	4.9	0	14:25	0.110
865	0.000	3.1	0.0	0.0	0.000	5.1	0	14:25	0.071
866	0.000	5.0	0.0	0.0	0.000	8.5	0	14:25	0.113
877	0.000	3.1	0.0	0.0	0.000	5.3	0	14:25	0.123
878	0.000	3.9	0.0	0.0	0.000	6.5	0	14:25	0.114
879	0.000	3.4	0.0	0.0	0.001	11.3	0	19:25	0.125
880	0.000	5.5	0.0	0.0	0.001	25.3	0	19:40	0.127
881	0.000	4.1	0.0	0.0	0.001	21.4	0	19:41	0.128
882	0.000	7.7	0.0	0.0	0.001	27.3	0	19:51	0.532
883	0.001	9.1	0.0	0.0	0.002	33.9	0	20:07	0.420
884	0.001	7.8	0.0	0.0	0.002	27.3	0	19:58	0.424
885	0.000	8.4	0.0	0.0	0.002	29.5	0	19:52	0.431
886	0.000	6.0	0.0	0.0	0.001	21.4	0	19:47	0.533
887	0.000	6.1	0.0	0.0	0.001	21.2	0	19:40	0.535
9001	0.000	4.5	0.0	0.0	0.000	4.9	1	06:55	0.029
9002	0.000	13.3	0.0	0.0	0.000	13.6	1	06:55	0.029
9003	0.000	4.9	0.0	0.0	0.000	5.3	1	07:03	0.029
9004	0.000	4.4	0.0	0.0	0.000	4.7	1	07:01	0.030
9005	0.000	3.2	0.0	0.0	0.000	3.5	1	06:58	0.030
9006	0.000	4.2	0.0	0.0	0.000	4.5	1	07:05	0.031
9050	0.000	3.3	0.0	0.0	0.000	3.9	0	13:52	0.041
9051	0.000	3.1	0.0	0.0	0.000	3.6	0	13:53	0.042
9052	0.000	2.7	0.0	0.0	0.000	3.2	0	13:53	0.042
9053	0.000	2.4	0.0	0.0	0.000	2.8	0	13:54	0.042
9054	0.000	1.8	0.0	0.0	0.000	2.1	0	13:54	0.043
9055	0.000	1.7	0.0	0.0	0.000	2.0	0	13:54	0.043
9056	0.000	2.3	0.0	0.0	0.000	2.7	0	13:50	0.048
9057	0.000	1.8	0.0	0.0	0.000	2.2	0	13:50	0.049
9058	0.000	2.1	0.0	0.0	0.000	2.4	0	13:50	0.049
9059	0.000	2.1	0.0	0.0	0.000	2.5	0	13:50	0.049
9060	0.000	2.5	0.0	0.0	0.000	2.9	0	13:50	0.050
9061	0.000	2.4	0.0	0.0	0.000	2.9	0	13:50	0.050
924	0.000	1.6	0.0	0.0	0.000	3.5	0	13:05	0.044
940	0.000	1.6	0.0	0.0	0.001	26.4	0	17:35	0.006
941	0.000	0.0	0.0	0.0	0.000	0.0	0	00:00	0.000
942	0.000	6.1	0.0	0.0	0.003	58.8	0	17:35	0.012
945	0.001	7.6	0.0	0.0	0.004	62.5	0	15:37	0.038
946	0.001	8.1	0.0	0.0	0.005	66.7	0	15:36	0.038
948	0.000	4.8	0.0	0.0	0.002	42.9	0	15:19	0.038
978	0.000	3.4	0.0	0.0	0.000	5.1	0	17:07	0.074
984	0.000	3.2	0.0	0.0	0.000	4.8	0	17:08	0.076
985	0.000	3.8	0.0	0.0	0.000	5.3	0	17:09	0.077
986	0.000	2.8	0.0	0.0	0.000	4.3	0	17:10	0.077
987	0.000	2.8	0.0	0.0	0.000	4.1	0	17:11	0.078
988	0.000	2.9	0.0	0.0	0.000	6.0	0	18:30	0.081
9902	0.002	18.7	0.0	0.0	0.007	68.8	0	18:21	0.168
991	0.000	2.1	0.0	0.0	0.000	6.2	0	18:30	0.081
996	0.000	4.0	0.0	0.0	0.001	16.3	0	18:31	0.084
997	0.000	3.6	0.0	0.0	0.001	14.9	0	18:30	0.084
999	0.000	3.9	0.0	0.0	0.001	16.5	0	18:30	0.086

****
Outfall Loading Summary
****

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
Dundas_Street_Outfall	0.00	0.000	0.000	0.000
Dundas_Street_PS_Overflow_1	0.00	0.000	0.000	0.000
Front_St_PS_Overflow_1	0.00	0.000	0.000	0.000
WWTP	100.00	2.094	2.854	726.198
System	25.00	2.094	2.854	726.198

****
Link Flow Summary
****

Link	Type	Maximum |Flow| CMS	Time of Max Occurrence days	hr:min	Maximum |Veloc| m/sec	Max/ Full Flow	Max/ Full Depth
1001	CONDUIT	0.084	0	18:52	0.93	0.31	1.00
1009	CONDUIT	0.047	0	16:51	0.85	0.20	1.00
1010	CONDUIT	0.048	0	17:55	0.71	0.24	1.00
1011	CONDUIT	0.086	0	18:51	0.86	0.56	1.00
1023	CONDUIT	0.134	0	18:30	1.48	0.44	1.00
1025	CONDUIT	0.134	0	18:30	1.31	0.73	1.00
1026	CONDUIT	0.135	0	18:37	1.29	0.57	1.00
1027	CONDUIT	0.136	0	18:39	1.33	0.51	1.00
1028	CONDUIT	0.136	0	18:40	1.26	0.52	1.00
1029	CONDUIT	0.136	0	18:42	1.35	0.22	1.00
103	CONDUIT	0.011	0	13:50	0.43	0.26	0.28
1030	CONDUIT	0.168	0	18:36	1.86	0.19	1.00
1032	CONDUIT	0.073	0	14:07	1.13	0.16	1.00
1033	CONDUIT	0.030	0	18:19	0.85	0.10	1.00
104	CONDUIT	0.010	0	13:50	0.48	0.10	0.25
1045	CONDUIT	0.024	0	18:06	1.00	0.06	1.00
1046	CONDUIT	0.015	0	17:10	1.06	0.04	0.14
1048	CONDUIT	0.018	0	17:10	1.15	0.05	0.58
1050	CONDUIT	1.316	0	17:45	1.52	1.15	1.00
1052	CONDUIT	0.032	0	13:26	0.78	0.08	1.00
1054_1	CONDUIT	1.315	0	17:59	0.74	0.59	1.00
1054_2	CONDUIT	1.318	0	17:35	0.75	0.58	1.00
109	CONDUIT	0.002	0	13:50	0.39	0.02	0.11
1090	CONDUIT	0.071	0	13:25	0.87	0.18	0.33
1091	CONDUIT	0.071	0	13:25	0.68	0.29	0.40
1092	CONDUIT	0.072	0	13:26	0.85	0.46	0.34
1093	CONDUIT	0.070	0	13:25	0.73	0.48	0.37
1096	CONDUIT	0.061	0	13:25	0.62	0.19	0.38
1103	CONDUIT	0.059	0	13:23	0.69	0.33	0.34
1116	CONDUIT	0.056	0	13:20	0.46	0.11	0.44
1117	CONDUIT	0.057	0	13:21	0.45	0.14	0.46
1118	CONDUIT	0.057	0	13:22	0.85	0.27	0.29
1119	CONDUIT	0.057	0	13:23	0.82	0.09	0.30
1120	CONDUIT	0.055	0	13:20	0.65	0.26	0.34
1179	CONDUIT	0.899	0	21:06	1.61	0.42	1.00
1180	CONDUIT	0.901	0	21:02	1.55	0.93	1.00
1181	CONDUIT	0.901	0	21:03	1.69	0.63	1.00
1182	CONDUIT	0.901	0	21:01	1.78	0.54	1.00
1183	CONDUIT	0.901	0	21:03	1.78	0.47	1.00
1184	CONDUIT	0.901	0	21:03	1.04	0.61	1.00
1185	CONDUIT	0.901	0	21:03	1.04	0.64	1.00
1186	CONDUIT	0.957	0	18:08	1.10	0.65	1.00
1189	CONDUIT	0.239	1	14:46	1.24	0.38	1.00
1190	CONDUIT	0.242	1	14:46	1.38	0.39	1.00
1193	CONDUIT	0.245	1	14:46	1.26	0.45	1.00
1194	CONDUIT	0.248	1	14:45	1.01	0.41	1.00
1195	CONDUIT	0.250	1	14:45	1.12	0.46	1.00
1196	CONDUIT	0.236	1	12:50	1.48	0.39	0.46
1198	CONDUIT	0.236	1	12:51	1.44	0.47	0.47
1199	CONDUIT	0.236	1	12:51	1.63	0.42	0.42
1202	CONDUIT	0.237	1	12:52	1.81	0.32	0.68
1203	CONDUIT	0.238	1	12:52	1.74	0.34	1.00
1206	CONDUIT	0.234	1	12:50	1.41	0.50	0.47
1207	CONDUIT	0.232	1	12:50	1.39	0.40	0.47
1208	CONDUIT	0.230	1	12:50	1.49	0.42	0.45
1209	CONDUIT	0.228	1	12:50	1.42	0.44	0.46
1210	CONDUIT	0.226	1	12:50	1.43	0.40	0.45
1212	CONDUIT	0.201	1	12:50	1.79	0.35	0.51
1213	CONDUIT	0.202	1	12:50	1.10	0.77	0.51
1214	CONDUIT	0.220	1	12:50	1.46	0.43	0.44
1215	CONDUIT	0.221	1	12:50	1.40	0.36	0.45
1216	CONDUIT	0.225	1	12:50	1.36	0.48	0.47
1220	CONDUIT	0.009	1	12:50	0.74	0.12	0.23
1221	CONDUIT	0.014	1	12:50	0.59	0.14	0.26
1222	CONDUIT	0.015	1	12:50	0.62	0.16	0.27
1223	CONDUIT	0.016	1	12:50	0.67	0.15	0.26
1224	CONDUIT	0.017	1	12:50	0.67	0.15	0.28
1225	CONDUIT	0.018	1	12:50	0.73	0.16	0.27
1226	CONDUIT	0.005	1	12:50	0.45	0.06	0.20
1245	CONDUIT	0.006	1	12:50	0.45	0.06	0.20
1246	CONDUIT	0.012	1	12:50	0.29	0.11	0.61
1247	CONDUIT	0.018	1	12:50	0.63	0.23	0.34
1248	CONDUIT	0.024	1	12:50	0.74	0.27	0.37
1249	CONDUIT	0.030	1	12:50	0.82	0.32	0.41
1250	CONDUIT	0.036	1	12:50	0.87	0.38	0.45
1251	CONDUIT	0.042	1	12:50	0.86	0.45	0.51
1252	CONDUIT	0.049	1	12:50	0.83	0.57	0.59
1255	CONDUIT	0.055	1	12:50	0.96	0.61	0.57
1256	CONDUIT	0.061	1	12:50	1.11	0.59	0.55
1290	CONDUIT	0.061	1	12:50	0.96	0.47	0.51

1291	CONDUIT	0.062	1	12:50	0.97	0.54	0.51
1292	CONDUIT	0.062	1	12:50	0.98	0.47	0.50
1293	CONDUIT	0.063	1	12:50	0.94	0.54	0.53
1294	CONDUIT	0.063	1	12:51	1.13	0.53	0.46
1295	CONDUIT	0.064	1	12:51	0.82	0.32	0.69
1296	CONDUIT	0.679	0	15:53	1.85	0.84	0.65
1297	CONDUIT	0.679	0	15:54	1.89	0.81	0.64
1298	CONDUIT	0.679	0	15:54	1.97	0.73	0.62
1299	CONDUIT	0.680	0	15:56	1.90	0.78	0.63
1300	CONDUIT	0.680	0	15:56	1.86	0.84	0.65
1301	CONDUIT	0.681	0	15:57	1.88	0.83	0.64
1302	CONDUIT	0.681	0	15:57	1.97	0.73	0.62
1303	CONDUIT	0.682	0	15:58	1.90	0.81	0.64
1308	CONDUIT	0.687	0	15:59	1.90	0.81	0.64
1311	CONDUIT	0.687	0	15:58	1.93	0.75	0.67
1312	CONDUIT	0.687	0	15:47	1.88	0.78	0.84
1313	CONDUIT	0.687	0	16:56	1.92	0.79	1.00
1314	CONDUIT	0.687	0	16:58	2.44	0.50	1.00
1315	CONDUIT	0.694	0	16:58	1.84	0.78	1.00
1316	CONDUIT	0.695	0	16:57	1.85	0.69	1.00
132	CONDUIT	0.002	0	13:50	0.55	0.01	0.07
133	CONDUIT	0.001	0	13:50	0.33	0.01	0.07
134	CONDUIT	0.001	0	13:50	0.30	0.01	0.05
1348	CONDUIT	0.049	0	16:50	1.01	0.33	0.41
1349	CONDUIT	0.050	0	17:00	0.88	0.37	0.46
1350	CONDUIT	0.052	0	17:00	0.94	0.48	0.45
1351	CONDUIT	0.060	0	17:00	1.04	0.34	0.39
154	CONDUIT	0.051	0	13:55	0.83	0.41	0.42
155	CONDUIT	0.033	0	17:16	0.65	0.25	1.00
156	CONDUIT	0.160	0	15:44	1.58	0.47	1.00
158	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
159	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
160	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
161	CONDUIT	0.000	0	00:00	0.00	0.00	0.50
162	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
163	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
164	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
165	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
166	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
167	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
168	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
169	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
170	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1703	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
171	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1716	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1717	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1718	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1719	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
172	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1742	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1743	CONDUIT	0.000	0	00:00	0.00	0.00	0.34
1745	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1746	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1747	CONDUIT	0.074	0	13:25	0.85	0.14	0.35
1748	CONDUIT	0.077	0	13:25	0.76	0.40	0.39
1749	CONDUIT	0.080	0	13:25	0.89	0.24	0.35
1750	CONDUIT	0.080	0	13:25	0.78	0.19	0.39
1751	CONDUIT	0.080	0	13:27	0.83	0.31	0.37
1752	CONDUIT	0.082	0	13:28	1.20	0.24	0.29
1755	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1756	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1757	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1759	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1760	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1761	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1766	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1772	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1773	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1774	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
1775	CONDUIT	0.000	0	00:00	0.00	0.00	0.32
1776	CONDUIT	0.084	0	13:29	1.65	0.13	0.24
1777	CONDUIT	0.087	0	13:30	1.73	0.12	0.23
1778	CONDUIT	0.089	0	13:31	1.77	0.12	0.23
1779	CONDUIT	0.109	0	13:40	2.03	0.09	0.25
1802	CONDUIT	0.112	0	13:41	1.19	0.17	0.37
1803	CONDUIT	0.114	0	13:42	0.76	0.42	0.53
1804	CONDUIT	0.116	0	13:51	0.62	0.55	0.63
1805	CONDUIT	0.149	0	13:45	0.90	0.97	0.57
1806	CONDUIT	0.150	0	13:46	0.85	0.21	0.32
1807	CONDUIT	0.150	0	13:47	0.78	0.23	0.34
1808	CONDUIT	0.151	0	13:49	0.75	0.27	0.35
1809	CONDUIT	0.152	0	13:50	0.66	0.23	0.39
1821	CONDUIT	0.152	0	13:52	0.58	0.36	0.43
1877	CONDUIT	0.172	0	13:50	0.72	0.47	0.40
1878	CONDUIT	0.173	0	13:50	0.73	0.27	0.40
1879	CONDUIT	0.173	0	13:51	0.83	0.59	0.36
1880	CONDUIT	0.174	0	13:51	0.90	0.19	0.34
1881	CONDUIT	0.174	0	13:53	0.74	0.30	0.40
1882	CONDUIT	0.175	0	13:54	0.74	0.36	0.40
1883	CONDUIT	0.176	0	13:55	0.77	0.33	0.39
1884	CONDUIT	0.176	0	13:57	0.65	0.26	0.44
1885	CONDUIT	0.227	0	13:58	0.90	0.31	0.42
1886	CONDUIT	0.227	0	13:59	0.92	0.44	0.41
1887	CONDUIT	0.228	0	14:00	1.08	0.30	0.37
1888	CONDUIT	0.035	0	13:50	0.70	0.17	0.28
1891	CONDUIT	0.035	0	13:50	0.60	0.17	0.32
1893	CONDUIT	0.040	0	13:50	0.59	0.27	0.35
1905	CONDUIT	0.041	0	13:51	0.70	0.24	0.31
1912	CONDUIT	0.027	0	12:40	0.75	0.71	0.52
1925	CONDUIT	0.053	0	12:49	1.04	0.62	0.68
1926	CONDUIT	0.079	0	12:49	1.15	1.01	0.60
1927	CONDUIT	0.083	0	12:43	1.08	0.76	0.65
1929	CONDUIT	0.114	0	12:44	1.41	0.83	0.69
1931	CONDUIT	0.137	0	12:50	1.58	0.89	0.73
1933	CONDUIT	0.160	0	12:50	2.49	0.31	0.43
1934	CONDUIT	0.159	0	12:50	2.00	0.79	0.68
1935	CONDUIT	0.001	0	17:00	0.20	0.00	0.14
1946	CONDUIT	0.003	0	17:02	0.11	0.06	0.32
1947	CONDUIT	0.008	0	17:00	0.43	0.09	0.22
1948	CONDUIT	0.012	0	17:10	0.59	0.08	0.18
1949	CONDUIT	0.160	0	12:50	2.43	0.39	0.43
1950	CONDUIT	0.160	0	12:50	2.44	0.35	0.43
1951	CONDUIT	0.165	0	12:56	2.33	0.43	0.46
1956	CONDUIT	0.228	0	14:01	0.94	0.35	0.59
1957	CONDUIT	0.268	0	00:02	0.90	0.38	0.77
1958	CONDUIT	0.339	0	00:02	0.83	0.59	0.87
1959	CONDUIT	0.390	0	00:01	0.88	0.63	0.95
1960	CONDUIT	0.571	0	00:00	1.12	0.89	0.76
1977	CONDUIT	0.029	0	13:50	0.64	0.47	0.33
1978	CONDUIT	0.029	0	13:50	0.65	0.16	0.36
1979	CONDUIT	0.030	0	13:50	0.54	0.38	0.38
1980	CONDUIT	0.028	0	13:50	0.64	0.15	0.32
2015	CONDUIT	0.020	0	13:10	0.45	0.16	0.26
2016	CONDUIT	0.022	0	13:13	0.48	0.16	0.27
2017	CONDUIT	0.020	0	13:12	0.43	0.18	0.27
2018	CONDUIT	0.015	0	13:08	0.32	0.10	0.26
2019	CONDUIT	0.014	0	13:06	0.37	0.13	0.23
2020	CONDUIT	0.014	0	13:05	0.40	0.07	0.21
2021	CONDUIT	0.013	0	13:05	0.51	0.13	0.22
2029	CONDUIT	0.028	0	13:45	0.55	0.38	0.36
2048	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
2049	CONDUIT	0.170	0	13:25	4.20	0.32	0.69
2056	CONDUIT	0.862	0	12:56	2.65	0.31	1.00
208	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
2082	CONDUIT	0.065	0	17:01	0.79	0.50	0.51
2083	CONDUIT	0.066	0	17:03	0.77	0.55	0.53
2084	CONDUIT	0.069	0	17:05	0.88	0.53	0.49
2085	CONDUIT	0.063	0	17:00	1.04	0.30	0.40
2086	CONDUIT	0.074	0	17:07	1.05	0.41	0.45
2087	CONDUIT	0.076	0	17:08	0.96	0.43	0.50
209	CONDUIT	0.000	0	00:00	0.00	0.00	0.50
2099	CONDUIT	0.302	0	23:44	1.07	1.28	1.00
210	CONDUIT	0.087	0	13:18	0.90	1.02	0.82
2135	CONDUIT	0.065	0	13:50	0.62	0.34	0.40
2135_1	CONDUIT	0.044	0	13:50	0.48	0.22	0.36
2135_2	CONDUIT	0.033	0	13:50	0.46	0.18	0.30
2135_3	CONDUIT	0.022	0	13:50	0.39	0.12	0.26
2135_4	CONDUIT	0.011	0	13:50	0.28	0.06	0.20
2136	CONDUIT	0.269	0	14:55	2.45	0.48	1.00
2137	CONDUIT	0.149	0	14:55	1.05	0.35	1.00
2138	CONDUIT	0.270	0	14:55	1.91	0.85	1.00
2140	CONDUIT	0.237	0	00:00	1.49	0.94	1.00
2144	CONDUIT	0.062	1	12:50	0.84	0.13	0.26
2145	CONDUIT	0.021	1	12:50	0.55	0.04	0.16
2146	CONDUIT	0.041	1	12:50	0.90	0.08	0.19
2147	CONDUIT	1.340	0	17:59	0.76	0.27	1.00
2149	CONDUIT	1.327	0	17:59	0.75	0.60	1.00
2152	CONDUIT	0.009	0	13:55	0.25	0.09	1.00
2153	CONDUIT	0.015	0	13:21	0.40	0.12	1.00
216	CONDUIT	0.096	0	13:22	0.92	0.90	0.78
2175	CONDUIT	0.055	0	13:16	0.55	0.29	0.39
2176	CONDUIT	0.055	0	13:19	0.72	0.18	0.31
2177	CONDUIT	0.055	0	13:18	0.65	0.34	0.34
2178	CONDUIT	0.053	0	13:15	0.60	0.40	0.43
2179	CONDUIT	0.026	0	13:15	0.40	0.39	0.60
2180	CONDUIT	0.028	0	13:15	0.41	0.42	0.60
2181	CONDUIT	0.055	0	13:15	0.55	0.32	0.38
219	CONDUIT	0.117	0	13:24	1.10	0.97	0.79
2219	CONDUIT	0.382	0	21:51	1.35	1.91	1.00
2220	CONDUIT	0.384	0	22:51	1.36	1.82	1.00
2221	CONDUIT	0.389	0	22:52	1.37	1.61	1.00
2222	CONDUIT	0.404	0	22:50	1.43	1.39	1.00
2223	CONDUIT	0.397	0	22:53	1.46	0.47	1.00
2224	CONDUIT	0.413	1	00:54	1.46	1.66	1.00
2225	CONDUIT	0.417	1	00:53	1.48	1.24	1.00
2226	CONDUIT	0.424	1	00:52	1.50	2.61	1.00
2264	CONDUIT	0.312	1	01:19	1.10	1.23	1.00
2269	CONDUIT	0.038	0	18:01	1.23	0.37	0.61
2270	CONDUIT	0.079	0	13:55	0.86	0.44	1.00
2271	CONDUIT	0.078	0	14:02	0.65	0.30	1.00
2272	CONDUIT	0.078	0	14:02	1.05	0.22	1.00
2273	CONDUIT	0.038	0	15:14	1.23	0.10	0.61
2274	CONDUIT	0.044	0	13:05	0.92	0.25	0.34
2277	CONDUIT	0.197	1	09:30	1.86	0.39	1.00
2278	CONDUIT	0.216	0	12:05	1.80	0.54	1.00
2279	CONDUIT	0.237	0	00:00	2.26	0.89	1.00
2280	CONDUIT	0.237	0	00:00	1.49	1.79	1.00
2281	CONDUIT	0.345	0	00:00	2.74	2.92	1.00
2282	CONDUIT	0.340	0	16:02	2.71	2.79	1.00
2283	CONDUIT	0.340	0	15:58	2.71	2.38	1.00
2284	CONDUIT	0.024	0	18:26	0.74	0.28	0.39
2285	CONDUIT	0.024	0	18:24	0.19	0.12	1.00
2286	CONDUIT	0.025	0	18:23	0.20	0.16	1.00
2287	CONDUIT	0.033	0	00:47	0.36	0.21	1.00
2288	CONDUIT	0.102	0	00:00	0.81	0.63	1.00
2289	CONDUIT	0.101	0	00:00	0.80	0.21	1.00
229	CONDUIT	0.135	0	13:25	1.22	0.81	0.66
2291	CONDUIT	1.030	0	17:26	1.89	1.00	1.00
2292	CONDUIT	1.054	0	14:56	2.39	2.24	1.00
2339	CONDUIT	0.031	1	07:05	0.71	0.15	0.35
2340	CONDUIT	0.030	1	07:02	0.76	0.10	0.24
235	CONDUIT	0.148	0	13:25	2.06	0.85	0.62
2390_1	CONDUIT	0.130	0	13:40	1.22	0.14	1.00
2390_2	CONDUIT	0.130	0	13:40	2.37	0.07	0.59
2390_3	CONDUIT	0.130	0	13:58	0.82	1.30	1.00
2390_5	CONDUIT	0.142	0	02:43	1.59	0.68	0.59
273	CONDUIT	0.250	0	14:35	2.78	0.56	1.00
274	CONDUIT	0.240	0	15:44	1.23	1.07	1.00
275	CONDUIT	0.231	0	13:48	1.60	0.85	1.00
276	CONDUIT	0.219	0	13:38	1.73	0.61	1.00
277	CONDUIT	0.218	0	15:53	1.05	0.91	1.00

278	CONDUIT	0.176	0	12:49	0.85	0.98	1.00
283	CONDUIT	0.186	0	15:17	0.95	0.56	1.00
289	CONDUIT	0.061	0	13:15	1.13	0.46	0.49
290	CONDUIT	0.071	0	13:15	1.02	0.52	0.62
291	CONDUIT	0.028	0	13:14	0.73	0.21	0.38
292	CONDUIT	0.052	0	13:15	1.05	0.40	0.46
3300	CONDUIT	0.640	0	15:11	2.00	1.09	0.84
3301	CONDUIT	0.640	0	15:10	1.81	1.26	0.96
3302	CONDUIT	0.639	0	15:09	1.79	1.08	1.00
3303	CONDUIT	0.639	0	15:08	1.79	1.29	1.00
3304	CONDUIT	0.639	0	15:08	1.79	1.43	1.00
3305	CONDUIT	0.638	0	15:07	1.78	1.26	1.00
3306	CONDUIT	0.636	0	15:06	1.78	1.21	1.00
3307	CONDUIT	0.634	0	15:05	1.77	1.33	1.00
3309	CONDUIT	0.619	0	15:01	1.73	1.28	1.00
3310	CONDUIT	0.616	0	14:53	1.72	1.24	1.00
3311	CONDUIT	0.614	0	14:25	1.72	1.16	1.00
3312	CONDUIT	0.612	0	14:25	1.71	0.78	1.00
3313	CONDUIT	0.310	1	04:06	1.97	1.51	1.00
3314	CONDUIT	0.303	1	04:08	1.91	1.39	1.00
3315	CONDUIT	0.299	1	04:11	1.88	1.64	1.00
3317	CONDUIT	0.296	1	04:15	1.86	2.31	1.00
3318	CONDUIT	0.297	2	06:16	2.31	0.75	1.00
3319	CONDUIT	0.301	2	06:09	1.89	1.53	1.00
3320	CONDUIT	0.306	2	06:07	1.93	2.39	1.00
3321	CONDUIT	0.313	2	06:06	1.97	2.40	1.00
3339_10	CONDUIT	0.050	0	11:51	1.43	0.21	1.00
3339_11	CONDUIT	0.230	0	15:04	1.44	0.23	1.00
3339_12	CONDUIT	0.050	0	11:22	1.31	0.25	1.00
3339_2	CONDUIT	0.050	0	11:51	1.01	2.81	1.00
3339_3	CONDUIT	0.050	0	11:15	1.10	0.21	1.00
3339_5	CONDUIT	0.050	0	11:51	1.80	0.27	1.00
3339_6	CONDUIT	0.239	0	15:38	1.50	0.21	1.00
3339_8	CONDUIT	0.050	0	11:17	1.01	2.92	1.00
3339_9	CONDUIT	0.230	0	15:04	1.44	2.75	1.00
3340	CONDUIT	0.390	0	12:59	1.38	1.34	1.00
3341	CONDUIT	0.271	0	14:57	1.03	0.93	1.00
3342	CONDUIT	0.252	0	14:47	1.09	0.92	1.00
3343	CONDUIT	0.232	0	14:46	1.05	0.85	1.00
3344	CONDUIT	0.212	0	14:46	0.96	0.82	1.00
3345	CONDUIT	0.192	0	14:35	0.98	0.64	1.00
3346	CONDUIT	0.172	0	14:35	1.12	0.47	1.00
3347	CONDUIT	0.155	0	12:46	1.18	0.52	1.00
3348	CONDUIT	0.075	0	13:50	0.91	0.15	1.00
3364	CONDUIT	0.180	0	12:45	1.10	0.84	1.00
3365	CONDUIT	0.185	0	12:49	1.07	0.63	1.00
3366	CONDUIT	0.191	0	12:53	1.11	0.89	1.00
3367	CONDUIT	0.196	0	12:59	1.12	0.91	1.00
3368	CONDUIT	0.200	0	13:06	1.13	0.92	1.00
3369	CONDUIT	0.193	0	13:07	1.17	0.90	1.00
3370	CONDUIT	0.189	0	13:08	1.16	0.90	1.00
3371	CONDUIT	0.187	0	13:18	1.11	0.87	1.00
3372	CONDUIT	0.182	0	13:18	1.05	0.63	1.00
3373	CONDUIT	0.179	0	13:26	1.05	0.83	1.00
3374	CONDUIT	0.175	0	13:38	1.07	0.81	1.00
3375	CONDUIT	0.171	0	13:51	1.09	0.80	1.00
3376	CONDUIT	0.167	0	13:54	1.10	0.78	1.00
3377	CONDUIT	0.162	0	14:21	1.08	0.75	1.00
3378	CONDUIT	0.157	0	14:35	1.07	0.73	1.00
3379	CONDUIT	0.153	0	14:42	1.08	0.71	1.00
3380	CONDUIT	0.147	0	14:35	1.06	0.68	1.00
3381	CONDUIT	0.142	0	14:34	1.02	0.71	1.00
3382	CONDUIT	0.136	0	14:33	1.00	0.64	1.00
3383	CONDUIT	0.131	0	14:31	1.06	0.61	1.00
3384	CONDUIT	0.126	0	14:30	0.97	0.59	1.00
3385	CONDUIT	0.121	0	14:29	1.04	0.56	1.00
3386	CONDUIT	0.116	0	14:27	0.99	0.54	0.79
3387	CONDUIT	0.054	0	14:26	0.78	0.38	0.46
3388	CONDUIT	0.048	0	14:25	0.79	0.34	0.41
3389	CONDUIT	0.043	0	14:25	0.75	0.30	0.39
3390	CONDUIT	0.038	0	14:25	0.75	0.26	0.35
3391	CONDUIT	0.032	0	14:25	0.68	0.23	0.34
3392	CONDUIT	0.027	0	14:25	0.68	0.19	0.30
3393	CONDUIT	0.022	0	14:25	0.69	0.23	0.33
3394	CONDUIT	0.016	0	14:25	0.67	0.33	0.37
3395	CONDUIT	0.011	0	14:25	0.45	0.22	0.37
3396	CONDUIT	0.005	0	14:25	0.38	0.11	0.26
3398	CONDUIT	0.057	0	14:25	0.87	0.65	0.57
3399	CONDUIT	0.047	0	14:25	0.70	0.54	0.59
3400	CONDUIT	0.038	0	14:25	0.70	0.43	0.49
3401	CONDUIT	0.028	0	14:25	0.63	0.32	0.43
3402	CONDUIT	0.019	0	14:25	0.70	0.39	0.41
3403	CONDUIT	0.009	0	14:25	0.38	0.20	0.38
3500	CONDUIT	0.327	0	15:04	1.16	1.31	1.00
3502	CONDUIT	0.207	0	17:35	1.22	0.84	1.00
3503	CONDUIT	0.211	0	17:35	1.11	0.87	1.00
3504	CONDUIT	0.215	0	17:35	1.10	0.94	1.00
3505	CONDUIT	0.218	0	17:35	1.26	1.52	1.00
3690	CONDUIT	0.390	0	22:52	1.38	1.63	1.00
39	CONDUIT	0.068	0	13:50	0.82	0.34	0.33
391	CONDUIT	0.191	0	15:19	1.05	0.75	1.00
392	CONDUIT	0.210	0	15:19	1.32	0.64	1.00
393	CONDUIT	0.238	0	15:21	1.18	0.73	1.00
394	CONDUIT	0.239	0	15:23	1.29	0.70	1.00
395	CONDUIT	0.238	0	15:24	1.02	0.64	1.00
396	CONDUIT	0.237	0	15:26	0.84	0.64	1.00
400	CONDUIT	0.805	0	17:49	1.47	0.55	1.00
401	CONDUIT	0.810	0	13:05	2.00	0.67	1.00
403	CONDUIT	0.222	0	17:35	1.54	0.95	1.00
4035	CONDUIT	0.030	1	07:03	0.65	0.22	0.26
4036	CONDUIT	0.029	1	07:04	0.62	0.23	0.31
4037	CONDUIT	0.029	1	06:55	0.97	0.09	0.26
4038	CONDUIT	0.029	1	06:55	1.03	0.23	0.51
408	CONDUIT	0.837	0	12:56	2.09	0.60	1.00
412	CONDUIT	0.198	0	17:41	1.56	0.57	1.00
413	CONDUIT	0.198	0	17:44	1.01	0.68	1.00

414	CONDUIT	0.198	0	17:44	1.01	2.60	1.00
415	CONDUIT	0.195	0	17:35	1.48	0.48	1.00
417	CONDUIT	0.197	0	17:36	1.28	0.92	1.00
418	CONDUIT	0.145	0	20:55	0.74	0.42	1.00
419	CONDUIT	0.143	0	13:34	0.97	0.47	1.00
420	CONDUIT	0.198	0	13:33	1.19	0.47	1.00
421	CONDUIT	0.205	0	13:33	0.94	0.45	1.00
422	CONDUIT	0.035	0	13:40	0.76	0.67	1.00
423	CONDUIT	0.159	0	13:25	2.91	0.49	0.50
424	CONDUIT	0.343	0	13:44	3.11	1.15	1.00
425	CONDUIT	0.343	0	13:44	3.11	1.33	1.00
426	CONDUIT	0.204	1	09:57	2.65	0.42	1.00
427	CONDUIT	0.889	0	13:04	1.66	1.45	1.00
428	CONDUIT	0.895	0	13:02	2.01	0.71	1.00
429	CONDUIT	0.150	0	13:35	1.05	0.56	1.00
436	CONDUIT	0.003	0	14:55	0.39	0.05	1.00
437	CONDUIT	0.022	0	22:22	0.65	0.31	1.00
438	CONDUIT	0.570	0	20:10	1.23	0.57	1.00
439	CONDUIT	0.572	0	20:07	0.95	0.63	1.00
442	CONDUIT	0.024	0	22:23	0.61	0.38	1.00
443	CONDUIT	0.108	0	17:35	0.51	0.37	1.00
444	CONDUIT	0.110	0	17:37	0.51	0.78	1.00
445	CONDUIT	0.014	1	09:54	0.37	1.22	1.00
446	CONDUIT	0.175	0	13:37	1.44	0.70	1.00
447	CONDUIT	0.176	0	13:34	1.70	0.61	1.00
448	CONDUIT	0.065	0	14:53	1.74	0.85	1.00
449	CONDUIT	0.018	0	16:04	0.50	0.84	1.00
45	CONDUIT	0.095	0	13:50	0.66	0.27	0.36
450	CONDUIT	0.018	0	22:22	0.86	0.43	1.00
451	CONDUIT	0.064	0	14:27	2.38	0.55	1.00
452	CONDUIT	0.596	0	21:18	1.35	0.71	1.00
453	CONDUIT	0.037	1	01:19	0.83	0.43	1.00
454	CONDUIT	0.594	0	14:02	1.99	0.31	1.00
455	CONDUIT	0.038	1	01:20	0.77	1.12	1.00
456	CONDUIT	0.038	1	01:20	0.77	0.95	1.00
457	CONDUIT	0.082	0	17:35	0.85	0.88	1.00
458	CONDUIT	0.085	0	17:45	0.86	0.45	1.00
459	CONDUIT	0.083	0	17:35	0.86	0.35	1.00
460	CONDUIT	0.054	0	14:04	0.77	1.04	1.00
461	CONDUIT	0.189	0	13:45	1.32	1.14	1.00
465	CONDUIT	0.554	0	20:50	1.25	0.50	1.00
468	CONDUIT	0.563	0	20:35	1.27	0.91	1.00
469	CONDUIT	0.564	0	20:35	1.28	1.34	1.00
474	CONDUIT	0.548	0	20:51	1.91	0.79	1.00
475	CONDUIT	0.551	0	20:50	1.25	0.46	1.00
476	CONDUIT	0.539	0	20:50	1.90	1.00	1.00
477	CONDUIT	0.542	0	20:45	1.99	1.57	1.00
478	CONDUIT	0.545	0	20:47	1.69	0.77	1.00
499	CONDUIT	0.210	0	14:23	1.32	1.70	1.00
500	CONDUIT	0.213	0	14:22	1.34	1.47	1.00
502	CONDUIT	0.217	0	14:22	2.20	0.65	1.00
505	CONDUIT	0.157	0	14:26	1.42	1.62	1.00
5050	CONDUIT	0.204	0	17:35	1.49	0.48	1.00
506	CONDUIT	0.160	0	14:24	1.44	1.66	1.00
507	CONDUIT	0.174	0	14:23	1.09	0.81	1.00
51	CONDUIT	0.102	0	13:50	0.67	0.29	0.37
510	CONDUIT	0.144	0	13:09	2.03	2.28	1.00
511	CONDUIT	0.154	0	14:28	1.39	1.65	1.00
512	CONDUIT	0.020	0	17:25	0.45	0.29	1.00
513	CONDUIT	0.019	0	17:25	0.66	0.27	1.00
515	CONDUIT	0.042	0	13:12	0.85	0.83	1.00
520	CONDUIT	0.017	0	17:20	0.64	0.29	1.00
53_1	CONDUIT	0.104	0	13:50	0.68	0.31	0.38
53_2	CONDUIT	0.106	0	13:50	0.69	0.29	0.38
551	CONDUIT	0.247	0	16:15	0.98	1.14	1.00
552	CONDUIT	0.247	0	16:15	0.90	0.85	1.00
558	CONDUIT	0.203	0	23:50	1.07	0.66	1.00
560	CONDUIT	0.246	0	16:15	1.36	0.88	1.00
60	CONDUIT	0.107	0	13:50	0.68	0.31	0.39
61	CONDUIT	0.109	0	13:51	0.64	0.31	0.41
62	CONDUIT	0.111	0	13:53	0.80	0.32	0.35
63	CONDUIT	0.112	0	13:53	1.75	0.05	0.20
63_1	CONDUIT	0.112	0	13:53	1.13	0.25	0.28
64	CONDUIT	0.025	0	13:50	0.88	0.19	0.30
646	CONDUIT	0.247	0	21:50	0.87	1.15	1.00
647	CONDUIT	0.249	0	22:51	0.88	1.29	1.00
649	CONDUIT	0.296	0	23:26	1.07	0.97	1.00
650	CONDUIT	0.297	0	23:36	1.05	1.26	1.00
651	CONDUIT	0.300	0	23:37	1.06	1.06	1.00
663	CONDUIT	0.011	0	13:18	0.63	0.20	1.00
664	CONDUIT	0.021	0	13:13	0.59	0.23	1.00
665	CONDUIT	0.033	0	12:45	0.79	0.33	1.00
666	CONDUIT	0.043	0	12:41	0.64	0.38	1.00
667	CONDUIT	0.045	0	12:34	0.64	0.40	1.00
668	CONDUIT	0.045	0	12:25	0.60	0.42	1.00
669	CONDUIT	0.050	1	05:12	0.37	0.39	1.00
670	CONDUIT	0.303	1	00:00	1.07	1.49	1.00
672	CONDUIT	0.307	1	01:19	1.08	1.35	1.00
673	CONDUIT	0.309	1	01:19	1.09	1.66	1.00
675	CONDUIT	0.313	1	01:19	1.11	1.23	1.00
680	CONDUIT	0.090	0	14:31	1.03	0.85	1.00
681	CONDUIT	0.090	0	14:19	0.96	0.61	1.00
682	CONDUIT	0.092	0	13:54	0.97	0.89	1.00
683	CONDUIT	0.381	0	21:51	1.35	1.48	1.00
684	CONDUIT	0.383	0	21:51	1.35	1.21	1.00
688	CONDUIT	0.387	0	22:42	1.37	1.36	1.00
689	CONDUIT	0.392	0	22:52	1.39	1.61	1.00
779	CONDUIT	0.395	0	22:53	1.40	1.47	1.00
780	CONDUIT	0.398	0	22:53	1.41	1.56	1.00
781	CONDUIT	0.406	0	22:50	1.43	1.61	1.00
782	CONDUIT	0.409	1	00:55	1.44	1.36	1.00
854	CONDUIT	0.054	0	14:25	1.38	0.35	0.42
855	CONDUIT	0.057	0	14:23	1.42	0.40	0.44
860	CONDUIT	0.060	0	14:24	1.45	0.39	0.45
861	CONDUIT	0.063	0	14:25	1.47	0.42	0.46
862	CONDUIT	0.066	0	14:25	1.52	0.43	0.46

866	CONDUIT	0.069	0	14:25	1.56	0.44	0.47
867	CONDUIT	0.071	0	14:25	1.52	0.44	0.49
868	CONDUIT	0.110	0	14:25	1.79	0.39	0.49
880	CONDUIT	0.113	0	14:25	1.81	0.55	0.50
881	CONDUIT	0.114	0	14:25	1.63	0.35	0.45
882	CONDUIT	0.123	0	14:25	1.41	0.49	0.74
883	CONDUIT	0.125	0	14:25	1.33	0.64	1.00
884	CONDUIT	0.127	0	14:25	1.31	0.61	1.00
885	CONDUIT	0.128	0	14:26	0.96	0.68	1.00
886	CONDUIT	0.415	1	00:53	1.47	1.23	1.00
887	CONDUIT	0.420	1	00:52	1.49	1.62	1.00
888	CONDUIT	0.427	1	00:51	1.51	1.17	1.00
889	CONDUIT	0.431	1	00:51	1.56	1.38	1.00
890	CONDUIT	0.532	1	00:50	2.01	0.98	1.00
891	CONDUIT	0.533	0	20:40	2.03	1.13	1.00
892	CONDUIT	0.535	0	20:50	2.20	0.98	1.00
9011	CONDUIT	0.486	0	00:01	3.05	1.22	1.00
9012	CONDUIT	0.002	0	00:00	0.01	0.00	1.00
9013	CONDUIT	2.854	0	15:36	3.63	6.51	1.00
9014	CONDUIT	0.041	0	13:52	0.89	0.16	0.27
9015	CONDUIT	0.041	0	13:52	0.99	0.12	0.25
9016	CONDUIT	0.042	0	13:53	1.05	0.13	0.24
9017	CONDUIT	0.042	0	13:54	1.03	0.13	0.24
9018	CONDUIT	0.042	0	13:54	1.07	0.12	0.24
9019	CONDUIT	0.043	0	13:54	1.56	0.07	0.18
9020	CONDUIT	0.043	0	13:55	1.55	0.07	0.19
9021	CONDUIT	0.048	0	13:50	1.61	0.08	0.20
9022	CONDUIT	0.049	0	13:50	1.61	0.08	0.20
9023	CONDUIT	0.049	0	13:50	1.14	0.10	0.21
9024	CONDUIT	0.049	0	13:50	1.10	0.10	0.22
9025	CONDUIT	0.050	0	13:50	1.11	0.10	0.22
9026	CONDUIT	0.050	0	13:50	1.12	0.09	0.21
9027	CONDUIT	0.000	0	00:00	0.00	0.00	1.00
9028	CONDUIT	0.000	0	00:00	0.00	0.00	1.00
9029	CONDUIT	0.168	0	18:36	1.05	0.26	1.00
932	CONDUIT	0.044	0	13:05	1.32	0.15	0.26
946	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
947	CONDUIT	0.000	0	00:00	0.00	0.00	0.50
948	CONDUIT	0.006	0	21:02	0.42	0.03	1.00
949	CONDUIT	0.012	0	21:02	0.61	0.20	1.00
952	CONDUIT	0.038	0	13:18	0.78	1.17	1.00
953	CONDUIT	0.040	0	13:13	0.81	1.32	1.00
955	CONDUIT	0.038	0	15:37	0.78	0.53	1.00
957	CONDUIT	0.957	0	18:08	1.10	0.45	1.00
958	CONDUIT	0.957	0	18:08	1.10	0.55	1.00
959	CONDUIT	0.957	0	18:08	1.10	0.70	1.00
960	CONDUIT	0.956	0	18:04	1.10	0.78	1.00
961	CONDUIT	0.957	0	18:08	1.10	0.59	1.00
962	CONDUIT	0.957	0	18:08	1.10	0.58	1.00
963	CONDUIT	0.956	0	18:06	1.10	0.68	1.00
964_1	CONDUIT	0.957	0	18:04	1.10	0.79	1.00
964_2	CONDUIT	0.981	0	18:23	1.13	0.58	1.00
965	CONDUIT	0.981	0	18:17	1.13	0.72	1.00
966	CONDUIT	0.981	0	18:08	1.13	0.71	1.00
967	CONDUIT	0.981	0	18:09	1.13	0.74	1.00
968	CONDUIT	0.981	0	18:08	1.13	0.67	1.00
969	CONDUIT	1.315	0	17:44	1.52	0.89	1.00
970	CONDUIT	1.315	0	18:05	1.52	1.16	1.00
971	CONDUIT	1.315	0	17:51	1.52	0.95	1.00
988	CONDUIT	0.077	0	17:09	1.10	0.42	0.45
989	CONDUIT	0.077	0	17:11	0.96	0.61	0.50
990	CONDUIT	0.078	0	17:11	0.94	0.79	0.52
990_1	CONDUIT	0.080	0	17:12	1.09	0.38	0.38
9902	CONDUIT	0.358	0	00:00	1.16	0.66	0.77
9904	CONDUIT	0.795	0	22:14	2.81	9.51	1.00
9905	CONDUIT	0.795	0	22:14	2.81	2.36	1.00
9906_1	CONDUIT	0.346	0	22:18	2.18	8.26	1.00
9906_2	CONDUIT	0.347	0	22:16	2.18	0.25	1.00
9907	CONDUIT	0.346	0	22:15	2.18	3.72	1.00
9908	CONDUIT	0.000	0	00:00	0.00	0.00	0.00
9909	CONDUIT	1.349	0	00:00	4.77	6.13	1.00
9910	CONDUIT	1.564	0	00:00	5.53	7.21	1.00
9911	CONDUIT	0.000	0	00:00	0.00	0.00	1.00
9912	CONDUIT	0.000	0	00:00	0.00	0.00	0.50
9914	CONDUIT	0.077	0	16:52	1.45	0.93	0.97
9915	CONDUIT	0.443	0	00:01	4.60	0.20	1.00
9916	CONDUIT	0.001	0	00:00	0.01	0.00	1.00
992_1	CONDUIT	0.080	0	17:13	0.95	0.40	0.56
992_2	CONDUIT	0.081	0	18:13	0.85	0.70	0.82
998	CONDUIT	0.081	0	18:23	1.13	0.34	0.94
999	CONDUIT	0.084	0	18:22	1.00	0.37	1.00
Dundas_1	PUMP	0.245	0	01:07		1.00	
Dundas_2	PUMP	0.000	0	00:00		0.00	
Dundas_3	PUMP	0.000	0	00:00		0.00	
East_PS_1	PUMP	0.200	0	00:00		1.00	
East_PS_2	PUMP	0.200	0	00:00		1.00	
East_PS_3	PUMP	0.000	0	00:00		0.00	
East_PS_4	PUMP	0.000	0	00:00		0.00	
FrontSt#1	PUMP	0.473	0	00:00		1.00	
FrontSt#2	PUMP	0.324	3	05:15		0.54	
FrontSt#3	PUMP	0.473	0	09:03		1.00	
FrontSt#4	PUMP	0.371	0	12:06		0.74	
2282_c	ORIFICE	0.000	0	00:00			0.00
9913	ORIFICE	1.062	0	14:55			1.00
3339_1	WEIR	0.679	1	03:17			1.00
3339_4	WEIR	0.742	0	12:42			1.00

****
Flow Classification Summary
****

Conduit	Adjusted /Actual Length	Dry	Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl
		---------- Fraction of Time in Flow Class ----------								
1001	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.81	0.00
1009	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.82	0.00
1010	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.80	0.00
1011	1.00	0.00	0.00	0.00	0.64	0.00	0.00	0.36	0.00	0.00
1023	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.79	0.02	0.00
1025	1.00	0.00	0.00	0.00	0.21	0.00	0.00	0.79	0.00	0.00
1026	1.00	0.00	0.00	0.00	0.21	0.00	0.00	0.79	0.01	0.00
1027	1.00	0.00	0.00	0.00	0.23	0.00	0.00	0.77	0.01	0.00
1028	1.00	0.00	0.00	0.00	0.68	0.32	0.00	0.00	0.00	0.00
1029	1.00	0.00	0.00	0.00	0.23	0.00	0.00	0.77	0.00	0.00
103	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00
1030	1.00	0.00	0.00	0.00	0.24	0.00	0.00	0.76	0.00	0.00
1032	1.00	0.00	0.00	0.00	0.21	0.00	0.00	0.79	0.00	0.00
1033	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.78	0.00
104	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.02	0.95	0.00
1045	1.00	0.00	0.00	0.00	0.21	0.79	0.00	0.00	0.82	0.00
1046	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1048	1.00	0.00	0.00	0.00	0.16	0.00	0.00	0.84	0.16	0.00
1050	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1052	1.00	0.00	0.00	0.00	0.23	0.00	0.00	0.77	0.00	0.00
1054_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1054_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
109	1.00	0.00	0.00	0.00	0.13	0.01	0.00	0.85	0.14	0.00
1090	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1091	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1092	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1093	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1096	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1103	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1116	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
1117	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1118	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1119	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
1120	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1179	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
1180	1.00	0.00	0.00	0.00	0.94	0.00	0.00	0.06	0.00	0.00
1181	1.00	0.00	0.00	0.00	0.94	0.00	0.00	0.06	0.00	0.00
1182	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.00	0.00	0.00
1183	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
1184	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1185	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1186	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1189	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1190	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.66	0.00
1193	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.12	0.00
1194	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.35	0.00
1195	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1196	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1198	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1199	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
1202	1.00	0.00	0.00	0.00	0.11	0.89	0.00	0.00	1.00	0.00
1203	1.00	0.00	0.00	0.00	0.32	0.20	0.00	0.49	0.17	0.00
1206	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1207	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1208	1.00	0.00	0.00	0.00	0.69	0.31	0.00	0.00	0.00	0.00
1209	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1210	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1212	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1213	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1214	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1215	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1216	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1220	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1221	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1222	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.11	0.00
1223	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1224	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1225	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1226	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1245	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1246	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1247	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1248	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1249	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1250	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1251	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1252	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.73	0.00
1255	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1256	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1290	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1291	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1292	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1293	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.12	0.00
1294	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1295	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1296	1.00	0.00	0.00	0.00	0.16	0.00	0.00	0.84	0.00	0.00
1297	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1298	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1299	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1300	1.00	0.00	0.00	0.00	0.15	0.00	0.00	0.85	0.00	0.00
1301	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1302	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1303	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1308	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1311	1.00	0.00	0.00	0.00	0.16	0.00	0.00	0.84	0.00	0.00
1312	1.00	0.00	0.00	0.00	0.06	0.00	0.00	0.94	0.00	0.00
1313	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.91	0.00	0.00
1314	1.00	0.00	0.00	0.00	0.22	0.02	0.00	0.75	0.03	0.00
1315	1.00	0.00	0.00	0.00	0.41	0.00	0.00	0.59	0.06	0.00
1316	1.00	0.00	0.00	0.00	0.65	0.00	0.00	0.35	0.09	0.00
132	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
133	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
134	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1348	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.78	0.00
1349	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00

1350	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1351	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
154	1.00	0.04	0.00	0.00	0.00	0.00	0.00	0.96	0.00	0.00
155	1.00	0.14	0.02	0.00	0.04	0.00	0.00	0.80	0.82	0.00
156	1.00	0.00	0.00	0.00	0.07	0.38	0.00	0.54	0.00	0.00
158	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
159	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
160	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
161	1.00	0.16	0.84	0.00	0.00	0.00	0.00	0.00	0.00	0.00
162	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
163	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
164	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
165	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
166	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
167	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
168	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
169	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
170	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1703	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
171	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1716	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1717	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1718	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1719	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
172	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1742	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1743	1.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1745	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1746	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1747	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1748	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1749	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
1750	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1751	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1752	1.00	0.00	0.00	0.00	0.01	0.99	0.00	0.00	0.00	0.00
1755	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1756	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1757	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1759	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1760	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1761	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1766	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1772	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1773	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1774	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1775	1.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1776	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
1777	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.98	0.00
1778	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.99	0.01	0.00
1779	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.06	0.00
1802	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1803	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1804	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
1805	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1806	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.93	0.00
1807	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.14	0.00
1808	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1809	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.07	0.00
1821	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1877	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1878	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.05	0.00
1879	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1880	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1881	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
1882	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1883	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1884	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.06	0.00
1885	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.08	0.00
1886	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1887	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.02	0.00	0.00
1888	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.96	0.00
1891	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1893	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.05	0.00
1905	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1912	1.00	0.00	0.00	0.00	0.08	0.00	0.00	0.92	0.00	0.00
1925	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1926	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1927	1.00	0.00	0.00	0.00	0.08	0.00	0.00	0.92	0.00	0.00
1929	1.00	0.00	0.00	0.00	0.01	0.00	0.00	0.99	0.00	0.00
1931	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1933	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
1934	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
1935	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1946	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1947	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1948	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1949	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1950	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
1951	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
1956	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1957	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.48	0.00
1958	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
1959	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1960	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1977	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1978	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
1979	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
1980	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2015	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.00	0.00	0.00
2016	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2017	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2018	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2019	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2020	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2021	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
2029	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2048	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2049	1.00	0.00	0.00	0.00	0.02	0.16	0.00	0.82	0.18	0.00
2056	1.00	0.00	0.00	0.00	0.26	0.74	0.00	0.00	0.01	0.00
208	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2082	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2083	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.94	0.00
2084	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2085	1.00	0.00	0.00	0.00	0.33	0.28	0.00	0.39	0.60	0.00
2086	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.98	0.00
2087	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
209	1.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2099	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
210	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.33	0.00
2135	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.89	0.00
2135_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2135_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2135_3	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2135_4	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.93	0.00
2136	1.00	0.00	0.00	0.00	0.27	0.00	0.00	0.73	0.00	0.00
2137	1.00	0.00	0.00	0.00	0.98	0.01	0.00	0.00	0.73	0.00
2138	1.00	0.00	0.00	0.00	0.27	0.73	0.00	0.00	0.00	0.00
2140	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2144	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.80	0.00
2145	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2146	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
2147	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2149	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2152	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.79	0.00
2153	1.00	0.00	0.00	0.00	0.24	0.00	0.00	0.76	0.00	0.00
216	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.94	0.00
2175	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2176	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2177	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2178	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2179	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2180	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2181	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
219	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.93	0.00
2219	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2220	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2221	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2222	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
2223	1.00	0.00	0.01	0.00	0.92	0.07	0.00	0.00	0.81	0.00
2224	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2225	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.05	0.00
2226	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2264	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2269	1.00	0.88	0.02	0.00	0.03	0.07	0.00	0.00	0.77	0.00
2270	1.00	0.00	0.00	0.00	0.58	0.42	0.00	0.00	0.30	0.00
2271	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2272	1.00	0.00	0.00	0.00	0.81	0.01	0.00	0.18	0.24	0.00
2273	1.00	0.00	0.90	0.00	0.03	0.07	0.00	0.00	0.87	0.00
2274	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
2277	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2278	1.00	0.00	0.00	0.00	0.22	0.00	0.78	0.00	0.00	0.00
2279	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2280	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2281	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2282	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2283	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2284	1.00	0.89	0.00	0.00	0.04	0.00	0.00	0.07	0.00	0.00
2285	1.00	0.02	0.77	0.00	0.21	0.00	0.00	0.00	0.70	0.00
2286	1.00	0.01	0.01	0.00	0.98	0.00	0.00	0.00	0.05	0.00
2287	1.00	0.00	0.01	0.00	0.99	0.00	0.00	0.00	0.00	0.00
2288	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2289	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
229	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
2291	1.00	0.00	0.00	0.00	0.27	0.00	0.00	0.72	0.00	0.00
2292	1.00	0.00	0.00	0.00	0.78	0.00	0.00	0.22	0.01	0.00
2339	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
2340	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
235	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
2390_1	1.00	0.03	0.00	0.00	0.07	0.00	0.90	0.00	0.00	0.00
2390_2	1.00	0.03	0.00	0.00	0.97	0.00	0.00	0.00	0.97	0.00
2390_3	1.00	0.03	0.00	0.00	0.97	0.00	0.00	0.00	0.00	0.00
2390_5	1.00	0.01	0.01	0.00	0.82	0.15	0.00	0.00	0.20	0.00
273	1.00	0.00	0.00	0.00	0.19	0.01	0.00	0.79	0.14	0.00
274	1.00	0.00	0.00	0.00	0.79	0.00	0.00	0.21	0.00	0.00
275	1.00	0.00	0.00	0.00	0.64	0.36	0.00	0.00	0.05	0.00
276	1.00	0.00	0.00	0.00	0.23	0.00	0.00	0.77	0.02	0.00
277	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
278	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
283	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.74	0.00
289	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
290	1.00	0.00	0.00	0.00	0.36	0.13	0.00	0.50	0.23	0.00
291	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
292	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3300	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
3301	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3302	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3303	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3304	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3305	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.21	0.00
3306	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3307	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3309	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3310	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3311	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3312	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.57	0.00
3313	1.00	0.00	0.00	0.00	0.17	0.00	0.00	0.83	0.00	0.00
3314	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3315	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3317	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3318	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3319	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3320	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00

3321	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3339_10	1.00	0.00	0.00	0.00	0.41	0.25	0.33	0.00	0.00	0.00
3339_11	1.00	0.07	0.27	0.00	0.26	0.00	0.40	0.00	0.00	0.00
3339_12	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3339_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3339_3	1.00	0.00	0.03	0.00	0.97	0.00	0.00	0.00	0.31	0.00
3339_5	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3339_6	1.00	0.07	0.25	0.00	0.68	0.00	0.00	0.00	0.76	0.00
3339_8	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3339_9	1.00	0.07	0.00	0.00	0.93	0.00	0.00	0.00	0.00	0.00
3340_	1.00	0.00	0.00	0.00	0.97	0.00	0.00	0.03	0.80	0.00
3341	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.83	0.00
3342	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3343	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3344	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.68	0.00
3345	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.84	0.00
3346	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.91	0.00
3347	1.00	0.00	0.00	0.00	0.09	0.00	0.00	0.91	0.01	0.00
3348	1.00	0.00	0.00	0.00	0.92	0.04	0.00	0.05	0.87	0.00
3364	1.00	0.00	0.00	0.00	0.18	0.00	0.00	0.82	0.00	0.00
3365	1.00	0.00	0.00	0.00	0.95	0.00	0.00	0.05	0.00	0.00
3366	1.00	0.00	0.00	0.00	0.57	0.00	0.00	0.43	0.00	0.00
3367	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.81	0.00
3368	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.77	0.00
3369	1.00	0.00	0.00	0.00	0.85	0.00	0.00	0.15	0.00	0.00
3370	1.00	0.00	0.00	0.00	0.44	0.00	0.00	0.56	0.00	0.00
3371	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
3372	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
3373	1.00	0.00	0.00	0.00	0.86	0.00	0.00	0.14	0.00	0.00
3374	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.79	0.00
3375	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.84	0.00
3376	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.00	0.00
3377	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.86	0.00
3378	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.85	0.00
3379	1.00	0.00	0.00	0.00	0.99	0.00	0.00	0.01	0.01	0.00
3380	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.89	0.00
3381	1.00	0.00	0.00	0.00	0.21	0.00	0.00	0.79	0.00	0.00
3382	1.00	0.00	0.00	0.00	0.95	0.00	0.00	0.05	0.01	0.00
3383	1.00	0.00	0.00	0.00	0.13	0.00	0.00	0.87	0.00	0.00
3384	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.92	0.00
3385	1.00	0.00	0.00	0.00	0.07	0.00	0.00	0.93	0.00	0.00
3386	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.92	0.00
3387	1.00	0.00	0.00	0.00	0.18	0.00	0.00	0.82	0.02	0.00
3388	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.92	0.00
3389	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3390	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.09	0.00
3391	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3392	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.13	0.00
3393	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
3394	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
3395	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3396	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.95	0.00
3398	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
3399	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.99	0.00
3400	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3401	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3402	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
3403	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
3500	1.00	0.00	0.00	0.00	0.26	0.00	0.00	0.74	0.00	0.00
3502	1.00	0.00	0.00	0.00	0.28	0.00	0.00	0.72	0.01	0.00
3503	1.00	0.00	0.00	0.00	0.26	0.00	0.00	0.74	0.00	0.00
3504	1.00	0.00	0.00	0.00	0.26	0.00	0.00	0.74	0.00	0.00
3505	1.00	0.00	0.00	0.00	0.26	0.00	0.00	0.74	0.00	0.00
3690	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
39	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
391	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
392	1.00	0.00	0.00	0.00	0.26	0.00	0.00	0.74	0.00	0.00
393	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.03	0.00
394	1.00	0.00	0.00	0.00	0.27	0.00	0.00	0.73	0.00	0.00
395	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.56	0.00
396	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
400	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.70	0.00
401	1.00	0.00	0.00	0.00	0.27	0.73	0.00	0.00	0.34	0.00
403	1.00	0.00	0.00	0.00	0.27	0.73	0.00	0.00	0.00	0.00
4035	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
4036	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
4037	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
4038	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	1.00	0.00
408	1.00	0.00	0.00	0.00	0.27	0.73	0.00	0.00	0.20	0.00
412	1.00	0.00	0.00	0.00	0.27	0.73	0.00	0.00	0.74	0.00
413	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.73	0.00
414	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
415	1.00	0.00	0.00	0.00	0.26	0.74	0.00	0.00	0.77	0.00
417	1.00	0.00	0.00	0.00	0.26	0.00	0.00	0.74	0.01	0.00
418	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
419	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.77	0.00
420	1.00	0.00	0.02	0.00	0.96	0.02	0.00	0.00	0.76	0.00
421	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
422	1.00	0.78	0.01	0.00	0.22	0.00	0.00	0.00	0.64	0.00
423	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
424	1.00	0.00	0.00	0.00	0.22	0.00	0.00	0.77	0.00	0.00
425	1.00	0.00	0.00	0.00	0.21	0.00	0.00	0.79	0.00	0.00
426	1.00	0.78	0.00	0.00	0.22	0.00	0.00	0.01	0.00	0.00
427	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
428	1.00	0.00	0.00	0.00	0.25	0.00	0.00	0.75	0.00	0.00
429	1.00	0.00	0.74	0.00	0.26	0.00	0.00	0.00	0.64	0.00
436	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.88	0.00
437	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.04	0.00
438	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.77	0.00
439	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
442	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.83	0.00
443	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.78	0.00
444	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
445	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
446	1.00	0.00	0.00	0.00	0.96	0.04	0.00	0.00	0.01	0.00
447	1.00	0.00	0.00	0.00	0.23	0.77	0.00	0.00	0.01	0.00

448	1.00	0.00	0.00	0.00	0.15	0.01	0.00	0.84	0.02	0.00
449	1.00	0.15	0.01	0.00	0.16	0.00	0.00	0.68	0.03	0.00
45	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.94	0.00
450	1.00	0.16	0.00	0.00	0.11	0.00	0.00	0.73	0.03	0.00
451	1.00	0.00	0.00	0.00	0.18	0.02	0.00	0.80	0.02	0.00
452	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
453	1.00	0.84	0.00	0.00	0.15	0.00	0.00	0.01	0.00	0.00
454	1.00	0.00	0.02	0.00	0.23	0.75	0.00	0.00	0.79	0.00
455	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.03	0.00
456	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.78	0.00
457	1.00	0.00	0.00	0.00	0.20	0.00	0.80	0.00	0.00	0.00
458	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.79	0.00
459	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.80	0.00
460	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.73	0.00
461	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
465	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
468	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
469	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
474	1.00	0.00	0.00	0.00	0.21	0.79	0.00	0.00	0.01	0.00
475	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.79	0.00
476	1.00	0.00	0.00	0.00	0.52	0.48	0.00	0.00	0.85	0.00
477	1.00	0.00	0.00	0.00	0.13	0.00	0.00	0.87	0.00	0.00
478	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.19	0.00
499	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
500	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
502	1.00	0.01	0.00	0.00	0.17	0.00	0.00	0.82	0.00	0.00
505	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.77	0.00
5050	1.00	0.00	0.00	0.00	0.25	0.01	0.00	0.74	0.00	0.00
506	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
507	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
51	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.96	0.00
510	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.81	0.00
511	1.00	0.00	0.00	0.00	0.22	0.00	0.00	0.78	0.02	0.00
512	1.00	0.00	0.00	0.00	0.89	0.00	0.00	0.11	0.68	0.00
513	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.83	0.00
515	1.00	0.00	0.74	0.00	0.26	0.00	0.00	0.00	0.69	0.00
520	1.00	0.00	0.00	0.00	0.17	0.00	0.00	0.83	0.00	0.00
53_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
53_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.88	0.00
551	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
552	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.81	0.00
558	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
560	1.00	0.00	0.00	0.00	0.18	0.00	0.00	0.82	0.00	0.00
60	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
61	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.90	0.00
62	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
63	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
63_1	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
64_	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
646	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.06	0.00
647	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
649	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.80	0.00
650	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
651	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.62	0.00
663	1.00	0.00	0.00	0.00	0.17	0.00	0.00	0.83	0.01	0.00
664	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.83	0.00
665	1.00	0.00	0.00	0.00	0.18	0.00	0.00	0.82	0.01	0.00
666	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.82	0.00
667	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.81	0.00
668	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
669	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.80	0.00
670	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
672	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
673	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
675	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
680	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
681	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.86	0.00
682	1.00	0.00	0.00	0.00	0.15	0.00	0.00	0.85	0.00	0.00
683	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
684	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.08	0.00
688	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
689	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
779	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
780	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
781	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
782	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.09	0.00
854	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
855	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
860	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
861	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
862	1.00	0.00	0.00	0.00	0.00	0.17	0.00	0.83	0.00	0.00
866	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
867	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
868	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.07	0.00
880	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
881	1.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
882	1.00	0.00	0.00	0.00	0.06	0.94	0.00	0.00	1.00	0.00
883	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.03	0.00
884	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.91	0.00
885	1.00	0.00	0.00	0.00	0.98	0.00	0.00	0.02	0.86	0.00
886	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.01	0.00
887	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.06	0.00
888	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.06	0.00
889	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.02	0.00
890	1.00	0.00	0.00	0.00	0.16	0.84	0.00	0.00	0.84	0.00
891	1.00	0.00	0.00	0.00	0.16	0.84	0.00	0.00	0.00	0.00
892	1.00	0.00	0.00	0.00	0.11	0.00	0.00	0.89	0.00	0.00
9011	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9012	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9013	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9014	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9015	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9016	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9017	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9018	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9019	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00

9020	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9021	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9022	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9023	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9024	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9025	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9026	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
9027	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9028	1.00	0.00	0.78	0.00	0.22	0.00	0.00	0.00	0.00	0.00
9029	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
932	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
946	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
947	1.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
948	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.92	0.00
949	1.00	0.00	0.00	0.00	0.17	0.00	0.00	0.83	0.01	0.00
952	1.00	0.12	0.68	0.00	0.20	0.00	0.00	0.00	0.70	0.00
953	1.00	0.11	0.01	0.00	0.19	0.00	0.00	0.69	0.01	0.00
955	1.00	0.12	0.00	0.00	0.17	0.00	0.00	0.70	0.73	0.00
957	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
958	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
959	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
960	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
961	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
962	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
963	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
964_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
964_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
965	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
966	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
967	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
968	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
969	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
970	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
971	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
988	1.00	0.00	0.00	0.00	0.15	0.00	0.00	0.84	0.00	0.00
989	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
990	1.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00	0.00	0.00
990_1	1.00	0.00	0.00	0.00	0.03	0.00	0.00	0.97	0.00	0.00
9902	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.91	0.00
9904	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9905	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9906_1	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9906_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9907	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9908	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
9909	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9910	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9911	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9912	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9914	1.00	0.01	0.01	0.00	0.95	0.02	0.00	0.00	0.36	0.00
9915	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
9916	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
992_1	1.00	0.00	0.00	0.00	0.20	0.00	0.00	0.80	0.03	0.00
992_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00
998	1.00	0.00	0.00	0.00	0.16	0.00	0.00	0.84	0.05	0.00
999	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.84	0.00

****
Conduit Surcharge Summary
****

Conduit	--------- Hours Full -------- Both Ends	Upstream	Dnstream	Hours Above Full Normal Flow	Hours Capacity Limited
1001	14.38	14.38	16.53	0.01	0.01
1009	14.23	14.23	16.02	0.01	0.01
1010	16.02	16.02	17.07	0.01	0.01
1011	16.63	16.63	16.97	0.01	0.01
1023	17.12	17.12	18.72	0.01	0.01
1025	18.80	18.80	18.82	0.01	0.01
1026	18.93	18.93	19.78	0.01	0.01
1027	19.88	19.88	20.97	0.01	0.01
1028	21.07	21.07	21.69	0.01	0.01
1029	21.43	21.43	21.66	0.01	0.01
1030	22.09	22.09	22.53	0.01	0.01
1032	18.99	18.99	19.08	0.01	0.01
1033	19.28	19.28	20.63	0.01	0.01
1045	11.18	11.18	18.99	0.01	0.01
1048	0.01	0.01	2.76	0.01	0.01
1050	96.00	96.00	96.00	24.70	91.32
1052	20.43	20.43	20.89	0.01	0.01
1054_1	96.00	96.00	96.00	0.01	0.01
1054_2	96.00	96.00	96.00	0.01	0.06
1179	41.26	41.26	50.29	0.01	0.01
1180	51.62	51.62	52.99	0.01	0.22
1181	55.07	55.07	67.73	0.01	0.01
1182	89.71	89.71	90.77	0.01	0.01
1183	90.77	90.77	95.01	0.01	0.01
1184	95.24	95.24	95.27	0.01	0.01
1185	95.29	95.29	95.32	0.01	0.01
1186	95.33	95.33	95.86	0.01	0.01
1189	23.86	23.86	24.27	0.01	0.01
1190	24.27	24.27	31.43	0.01	0.01
1193	31.43	31.43	37.83	0.01	0.01
1194	38.49	38.49	52.08	0.01	0.01
1195	52.08	52.08	55.13	0.01	0.01
1202	0.01	0.01	5.42	0.01	0.01
1203	5.42	5.42	23.90	0.01	0.01
1246	0.01	0.01	62.39	0.01	0.01
1295	0.01	0.01	75.86	0.01	0.01
1313	2.93	2.93	5.51	0.01	0.01
1314	6.19	6.19	15.10	0.01	0.01
1315	24.74	24.74	29.51	0.01	0.01
1316	32.00	32.00	41.00	0.01	0.01
155	0.35	0.35	2.85	0.01	0.01
156	3.14	3.14	3.73	0.01	0.01
1926	0.01	0.01	0.01	0.59	0.01
2049	0.01	0.01	14.58	0.01	0.01
2056	23.52	23.52	24.60	0.01	0.01
2099	18.06	18.06	18.09	16.48	16.67
210	0.01	0.01	0.01	1.52	0.01
2136	25.75	25.75	25.88	0.01	0.01
2137	25.21	25.21	25.74	0.01	0.01
2138	25.74	25.74	25.75	0.01	8.40
2140	96.00	96.00	96.00	0.01	0.01
2147	96.00	96.00	96.00	0.01	0.01
2149	96.00	96.00	96.00	0.01	0.01
2152	19.75	19.75	22.35	0.01	0.01
2153	22.19	22.19	22.27	0.01	0.01
2219	18.41	18.42	18.41	18.93	18.41
2220	18.72	18.73	18.72	18.74	18.72
2221	19.05	19.05	19.17	18.27	18.51
2222	17.18	17.21	17.18	17.35	17.18
2223	15.09	15.09	17.29	0.01	0.01
2224	16.30	16.54	16.30	18.38	16.30
2225	16.52	16.52	16.68	15.80	15.93
2226	11.39	14.50	11.39	61.12	11.39
2264	18.15	18.15	18.23	15.37	15.51
2269	0.01	0.01	83.27	0.01	0.01
2270	16.00	16.00	33.29	0.01	0.01
2271	95.30	95.30	95.32	0.01	0.01
2272	33.29	33.29	51.20	0.01	0.01
2273	0.01	0.01	83.02	0.01	0.01
2277	39.08	39.08	95.96	0.01	0.01
2278	20.85	20.85	21.25	0.01	0.01
2279	95.99	95.99	96.00	0.01	0.01
2280	96.00	96.00	96.00	96.00	0.01
2281	96.00	96.00	96.00	96.00	96.00
2282	96.00	96.00	96.00	96.00	96.00
2283	96.00	96.00	96.00	96.00	96.00
2285	6.12	6.12	82.69	0.01	0.01
2286	65.03	65.03	94.72	0.01	0.01
2287	94.74	94.74	95.32	0.01	0.01
2288	96.00	96.00	96.00	0.01	0.01
2289	96.00	96.00	96.00	0.01	0.01
2291	25.73	25.73	25.97	1.79	1.79
2292	38.22	87.04	38.22	89.78	38.22
2390_1	3.39	3.39	93.35	0.01	0.01
2390_2	0.01	0.01	93.36	0.01	0.01
2390_3	93.36	93.36	93.36	6.77	10.30
2390_5	0.01	0.01	74.06	0.01	0.01
273	3.83	3.83	18.11	0.01	0.01
274	18.68	18.72	18.74	1.14	7.21
275	18.76	18.76	19.73	0.01	0.01
276	19.73	19.73	21.45	0.01	0.01
277	23.34	23.34	23.65	0.01	0.01
278	24.17	24.17	24.26	0.01	0.01
283	23.65	23.65	24.17	0.01	0.01
3300	0.01	0.01	0.01	15.58	0.01
3301	0.01	16.45	0.01	26.11	0.01
3302	16.45	18.09	16.45	15.14	16.45
3303	18.09	22.78	18.09	27.55	18.09
3304	23.42	25.14	23.42	58.83	23.42
3305	25.13	25.46	25.14	26.08	25.13
3306	24.10	24.10	25.46	23.15	23.34
3307	24.22	24.72	24.22	38.61	24.22
3309	24.58	24.93	24.58	32.21	24.58
3310	24.93	25.02	24.93	26.10	24.93
3311	25.00	25.00	25.02	19.55	23.85
3312	24.60	24.60	95.38	0.01	0.01
3313	15.66	95.54	15.66	95.72	15.66
3314	95.52	95.56	95.54	95.69	95.52
3315	95.56	95.77	95.56	95.84	95.56
3317	95.77	95.89	95.77	95.90	95.77
3318	95.22	95.22	95.89	0.01	0.01
3319	95.22	95.87	95.22	95.91	95.22
3320	95.87	95.96	95.87	95.96	95.87
3321	95.96	95.99	95.96	95.99	95.96
3339_10	23.35	23.35	95.86	0.01	0.01
3339_11	20.23	20.23	87.82	0.01	0.01
3339_12	24.42	24.42	95.44	0.01	0.01
3339_2	95.86	95.86	95.86	95.87	95.85
3339_3	42.59	42.59	95.39	0.01	0.01
3339_5	93.04	93.04	95.86	0.01	0.01
3339_6	16.21	16.21	87.82	0.01	0.01
3339_8	95.39	95.39	95.44	85.34	85.10
3339_9	87.82	87.82	87.87	19.65	19.83
3340	15.71	15.71	15.98	5.07	3.41
3341	15.40	15.40	15.71	0.01	0.01
3342	14.82	14.82	15.38	0.01	0.01
3343	12.41	12.41	14.62	0.01	0.01
3344	9.38	9.38	12.49	0.01	0.01
3345	8.44	8.44	9.38	0.01	0.01
3346	7.34	7.34	8.44	0.01	0.01
3347	6.43	6.43	7.18	0.01	0.01
3348	5.81	5.81	6.26	0.01	0.01
3364	16.15	16.15	16.43	0.01	0.01
3365	16.03	16.03	16.11	0.01	0.01
3366	15.68	15.68	15.97	0.01	0.01
3367	15.39	15.39	15.68	0.01	0.01
3368	15.02	15.02	15.39	0.01	0.01
3369	14.93	14.93	14.97	0.01	0.01
3370	14.76	14.76	14.88	0.01	0.01
3371	14.41	14.41	14.74	0.01	0.01
3372	14.35	14.35	14.41	0.01	0.01
3373	13.93	13.93	14.29	0.01	0.01
3374	13.46	13.46	13.91	0.01	0.01
3375	12.98	12.98	13.46	0.01	0.01
3376	12.40	12.40	12.95	0.01	0.01

3377	11.80	11.80	12.40	0.01	0.01
3378	11.12	11.12	11.80	0.01	0.01
3379	10.30	10.30	11.08	0.01	0.01
3380	9.31	9.31	10.30	0.01	0.01
3381	9.19	9.21	9.21	0.01	4.31
3382	7.81	7.81	9.07	0.01	0.01
3383	6.39	6.39	7.46	0.01	0.01
3384	4.81	4.81	6.39	0.01	0.01
3385	0.61	0.61	4.18	0.01	0.01
3500	22.51	22.51	22.64	7.62	16.21
3502	23.40	23.40	23.82	0.01	0.01
3503	23.86	23.86	24.32	0.01	0.01
3504	24.39	24.39	24.61	0.01	7.00
3505	24.69	24.69	24.70	15.74	16.37
3690	19.17	19.17	31.09	18.31	18.34
391	24.26	24.26	24.43	0.01	0.01
392	24.43	24.43	24.57	0.01	0.01
393	24.82	24.82	25.08	0.01	0.01
394	25.08	25.08	25.34	0.01	0.01
395	25.75	25.75	25.88	0.01	0.01
396	25.88	25.88	26.03	0.01	0.01
400	25.56	25.56	25.86	0.01	0.01
401	25.21	25.21	25.56	0.01	0.01
403	24.86	24.86	25.29	0.01	6.77
408	24.60	24.60	25.21	0.01	0.01
412	23.67	23.67	25.09	0.01	0.01
413	25.09	25.09	25.80	0.01	0.01
414	25.77	25.78	25.77	24.67	23.70
415	21.07	21.07	23.06	0.01	0.01
417	23.06	23.06	23.67	0.01	0.01
418	22.67	22.67	22.86	0.01	0.01
419	21.57	21.57	22.69	0.01	0.01
420	20.60	20.60	21.59	0.01	0.01
421	21.39	21.39	22.82	0.01	0.01
422	20.52	20.52	82.41	0.01	0.01
424	21.23	21.23	21.54	4.38	4.51
425	21.66	52.77	21.66	27.60	21.66
426	19.83	19.83	20.31	0.01	0.01
427	22.26	22.32	22.26	18.48	17.47
428	22.26	22.26	23.00	0.01	0.01
429	20.44	20.44	82.59	0.01	0.01
436	9.56	9.56	11.07	0.01	0.01
437	11.07	11.07	14.59	0.01	0.01
438	20.61	20.61	21.93	0.01	0.01
439	21.93	21.93	22.32	0.01	0.01
442	15.04	15.04	20.19	0.01	0.01
443	19.36	19.36	21.12	0.01	0.01
444	21.15	21.15	21.21	0.01	0.01
445	20.13	20.19	21.88	8.96	11.67
446	19.48	19.48	20.42	0.01	0.01
447	20.42	20.42	21.07	0.01	0.01
448	11.51	11.51	14.30	0.01	0.01
449	5.45	5.45	14.19	0.01	0.01
450	5.45	5.45	9.60	0.01	0.01
451	15.82	15.82	17.50	0.01	0.01
452	94.21	94.21	94.84	0.01	0.01
453	12.62	12.62	12.76	0.01	0.01
454	16.50	16.50	20.61	0.01	0.01
455	17.99	17.99	18.48	6.14	6.22
456	18.48	18.48	18.90	0.01	0.01
457	18.47	18.47	18.76	0.01	0.01
458	18.80	18.80	19.59	0.01	0.01
459	18.14	18.14	18.65	0.01	0.01
460	18.64	18.64	23.28	0.55	0.01
461	18.84	18.94	19.59	1.02	0.09
465	51.15	51.15	89.01	0.01	0.01
468	89.01	89.01	94.08	0.01	0.01
469	94.08	94.08	94.21	16.63	18.19
474	16.52	16.52	18.07	0.01	0.01
475	18.07	18.07	51.15	0.01	0.01
476	12.11	12.11	14.08	0.01	2.81
477	11.62	14.08	11.62	17.96	11.62
478	15.40	15.40	16.52	0.01	0.01
499	95.15	95.15	95.20	14.28	14.41
500	95.20	95.20	95.51	11.85	12.73
502	14.15	14.15	15.10	0.01	0.01
505	19.31	19.31	24.71	14.51	14.54
5050	22.68	22.68	23.31	0.01	0.01
506	24.71	24.71	94.81	14.81	14.86
507	78.46	78.46	95.15	0.01	0.01
510	18.15	18.24	18.32	17.99	17.44
511	17.90	17.90	19.01	14.75	14.77
512	16.44	16.44	17.80	0.01	0.01
513	15.76	15.76	16.44	0.01	0.01
515	17.68	17.68	20.53	0.01	0.01
520	15.56	15.56	15.64	0.01	0.01
551	17.26	17.26	17.33	14.82	14.88
552	17.33	17.33	17.59	0.01	0.01
558	16.44	16.44	16.68	0.01	0.01
560	16.73	16.73	16.76	0.01	11.78
646	17.59	17.59	17.72	15.24	15.30
647	17.72	17.72	17.79	16.20	16.25
649	17.45	17.45	17.82	0.01	0.01
650	17.82	17.82	17.85	16.30	16.52
651	17.85	17.85	18.06	11.36	11.71
663	14.57	14.57	15.28	0.01	0.01
664	15.30	15.30	15.98	0.01	0.01
665	15.98	15.98	16.58	0.01	0.01
666	16.56	16.56	16.82	0.01	0.01
667	16.83	16.83	17.14	0.01	0.01
668	17.14	17.14	17.39	0.01	0.01
669	17.39	17.39	17.80	0.01	0.01
670	18.09	18.09	18.14	17.64	17.67
672	18.14	18.14	18.17	16.91	17.03
673	18.15	18.17	18.15	18.19	18.11
675	18.23	18.23	18.34	15.33	17.38
680	10.94	10.94	11.95	0.01	0.01
681	11.95	11.95	13.23	0.01	0.01
682	13.23	13.23	13.56	0.01	0.01
683	18.33	18.33	18.42	17.76	17.81
684	18.41	18.41	18.73	15.66	16.10
688	18.72	18.72	19.05	17.18	17.25
689	31.09	31.09	67.86	18.25	18.31
779	77.10	77.10	93.99	17.68	17.74
780	17.21	17.29	17.21	18.03	17.21
781	16.97	17.18	16.97	18.22	16.97
782	16.92	16.97	16.92	17.18	16.92
882	0.01	0.01	3.09	0.01	0.01
883	3.09	3.09	6.41	0.01	0.01
884	6.41	6.41	8.56	0.01	0.01
885	8.56	8.56	11.50	0.01	0.01
886	16.30	16.30	16.52	15.67	15.90
887	14.50	16.68	14.50	18.19	14.50
888	9.56	11.39	9.56	14.07	9.56
889	9.12	9.56	9.12	17.15	9.12
890	9.04	9.04	10.16	0.01	0.01
891	9.21	10.16	9.21	13.10	9.21
892	9.21	9.21	9.97	0.01	0.01
9011	96.00	96.00	96.00	2.70	0.01
9012	96.00	96.00	96.00	0.01	0.01
9013	96.00	96.00	96.00	95.87	96.00
9029	47.56	47.56	58.66	0.01	0.01
948	5.80	5.80	14.47	0.01	0.01
949	14.47	14.47	15.45	0.01	0.01
952	16.48	16.48	16.99	6.89	0.01
953	16.99	16.99	17.68	7.20	0.01
955	13.57	13.57	15.77	0.01	0.01
957	95.99	95.99	96.00	0.01	0.01
958	96.00	96.00	96.00	0.01	0.01
959	96.00	96.00	96.00	0.01	0.01
960	96.00	96.00	96.00	0.01	0.01
961	96.00	96.00	96.00	0.01	0.01
962	96.00	96.00	96.00	0.01	0.01
963	96.00	96.00	96.00	0.01	0.01
964_1	96.00	96.00	96.00	0.01	0.02
964_2	96.00	96.00	96.00	0.01	0.01
965	96.00	96.00	96.00	0.01	0.01
966	96.00	96.00	96.00	0.01	0.01
967	96.00	96.00	96.00	0.01	0.01
968	96.00	96.00	96.00	0.01	0.01
969	96.00	96.00	96.00	0.01	0.01
970	96.00	96.00	96.00	27.29	31.37
971	96.00	96.00	96.00	0.01	7.27
9904	94.66	94.68	95.81	93.94	94.00
9905	96.00	96.00	96.00	86.77	88.99
9906_1	96.00	96.00	96.00	94.04	93.98
9906_2	96.00	96.00	96.00	0.01	0.01
9907	96.00	96.00	96.00	93.62	93.75
9909	96.00	96.00	96.00	48.13	34.11
9910	96.00	96.00	96.00	22.51	17.88
9914	0.01	0.01	93.47	0.01	0.01
9915	96.00	96.00	96.00	0.01	0.01
9916	96.00	96.00	96.00	0.01	0.01
998	0.01	0.01	10.17	0.01	0.01
999	10.85	10.85	15.15	0.01	0.01

****
Pumping Summary
****

Pump	Percent Utilized	Number of Start-Ups	Min Flow CMS	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr	Power Usage Kw-hr	% Time Off Pump Curve Low	% Time Off Pump Curve High
Dundas_1	24.62	1138	0.00	0.19	0.24	16.440	534.88	0.0	0.4
Dundas_2	0.00	0	0.00	0.00	0.00	0.000	0.00	0.0	0.0
Dundas_3	0.00	0	0.00	0.00	0.00	0.000	0.00	0.0	0.0
East_PS_1	100.00	1	0.00	0.16	0.20	56.960	1096.52	0.0	11.3
East_PS_2	88.59	2	0.00	0.05	0.20	16.690	334.06	0.0	3.1
East_PS_3	0.00	0	0.00	0.00	0.00	0.000	0.00	0.0	0.0
East_PS_4	0.00	0	0.00	0.00	0.00	0.000	0.00	0.0	0.0
FrontSt#1	97.96	83	0.00	0.44	0.47	147.845	6128.03	0.0	48.5
FrontSt#2	60.44	98	0.00	0.12	0.32	25.298	925.72	0.0	0.0
FrontSt#3	50.33	165	0.00	0.40	0.47	70.017	3415.63	0.0	0.4
FrontSt#4	27.70	2	0.00	0.35	0.37	33.230	1684.16	0.0	0.0

Analysis begun on: Tue Jan 28 11:56:56 2025
Analysis ended on: Tue Jan 28 12:02:03 2025
Total elapsed time: 00:05:07

Appendix C

Servicing Study Presentation
(February 12th, 2025)

February 12, 2025

Black Bear Ridge Water and Wastewater Servicing Study

Key Findings

CANADA BEST MANAGED COMPANIES | Platinum member

J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS

Agenda

Future Servicing

Water Treatment

Water Storage and Distribution

Sanitary Collection

Wastewater Treatment

Routing Options

Recommendations

Future Servicing Areas and Timelines

- **Black Bear Ridge**, located northeast of Belleville, covers an area of approximately 335 hectares with frontage on Harmony Road. Anticipated build-out will include over 3000 residential units and golf course resort developments in multiple phases over the next 20 to 30 years.
- **Harmony Public School** is located south of the Black Bear Ridge development area with frontage on Harmony Road. Anticipated build-out of the school will include 900 students. It's anticipated that the school will be serviced through Black Bear Ridge wastewater and water infrastructure.
- ~~**Foxboro** is located northwest of Belleville's urban serviced boundary, is an existing settlement area.~~
- **Corbyville Village** is located within Belleville's urban serviced boundary, is anticipated to build-out over 700 residential units.

Short-Term (0-10 years)
2023-2033

Mid-Term (10-20 years)
2033-2043

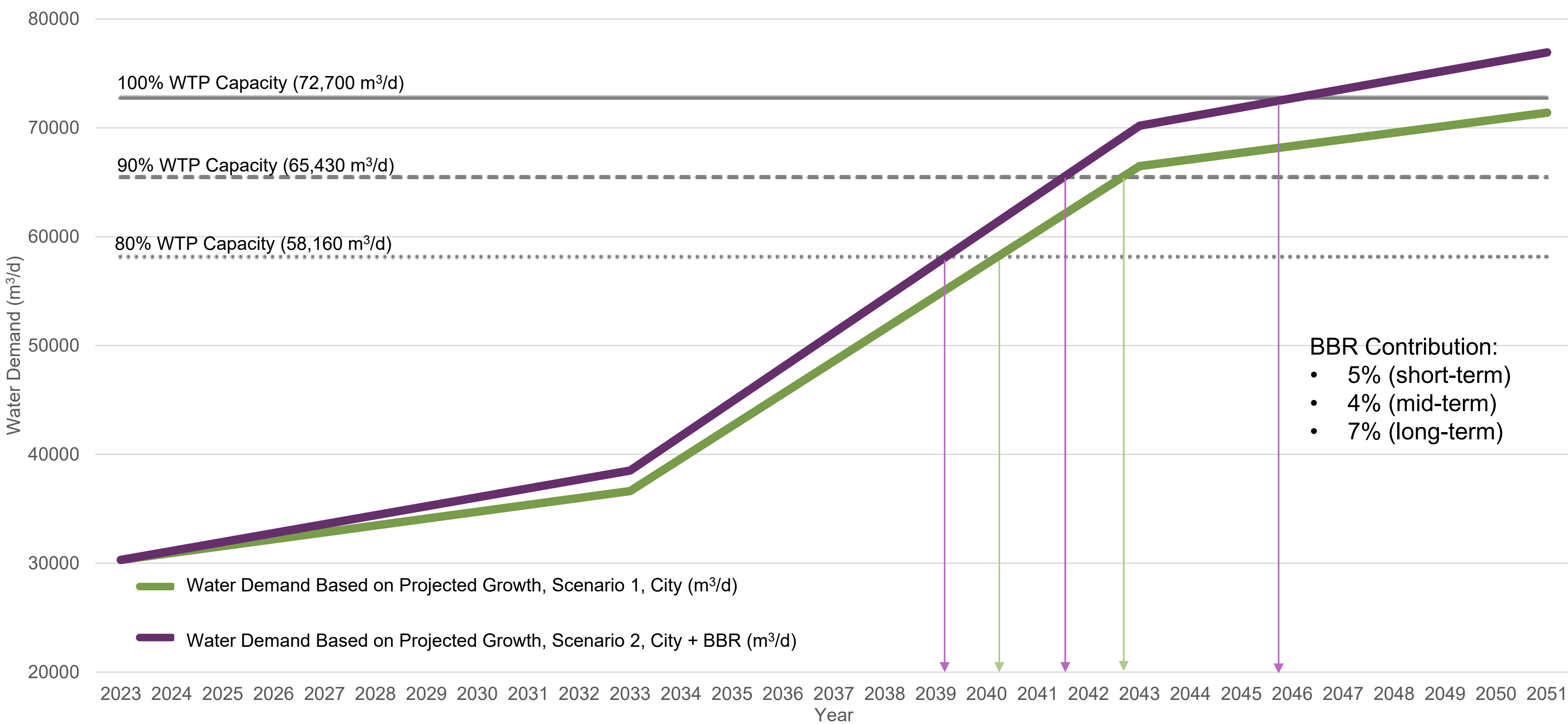
Long-Term (20+ years)
2043+

JLR Servicing Memo Scope of Work

- Model water and wastewater systems for future development with and without BBR.
- Confirm servicing route options for Black Bear Ridge ~~and Foxboro~~.
- Identify and evaluate alternative solutions to support future servicing.
- Develop a list of projects, associated timelines and costs.
- Propose split between Black Bear Ridge and City to fund infrastructure upgrades

Water Treatment Plant

Water Treatment Plant Capacity Evaluation



Water Storage

Storage - Existing

Parameter	Existing (2023)
Cumulative Equivalent Population [1]	61,682
Fire Flow [2] (L/s)	378
Duration [2] (Hours)	6
A – Fire Storage [3] (m^3)	8,165
B – Equalization Storage [4] (m^3)	7,578
C – Emergency Storage [5] (m^3)	3,936
Total Storage Requirement (m^3)	**19,678**
Existing Available Storage (m^3)	26,614
Surplus (m^3)	**6,936**

- Existing storage for the entire distribution system is being supplied in Zone 1, including WTP reservoirs, high lift pump wells, North Park Reservoir, Pine St. Reservoir and John St. Elevated Tower
- Adam St. Booster Station supplies required domestic and fire flow to Zone 2. Zone 2 does not currently have storage.

Storage – Short Term

	Short-Term Scenario 1 - City Growth Only			Short-Term Scenario 2 - City + BBR		
Parameter	Zone 1	Zone 2	Zone 3	Zone 1	Zone 2	Zone 3
Cumulative Equivalent Population (1)	66,815	7,957	0	66,815	7,957	3,824
Fire Flow (2) (L/s)	378	174	0	378	174	122
Duration (2) (Hours)	6	3	0	6	3	2
A – Fire Storage (3) (m^3)	8,165	1,876		8,165	1,876	881
B – Equalization Storage (4) (m^3)	6,543	975		8,185	975	468
C – Emergency Storage (5) (m^3)	3,677	713		4,087	713	337
Storage Requirement Per Zone (m^3)	18,384	3,563		20,437	3,563	1,687
Additional Storage Requirement for Upper Zone (m3) - 25% of MDF	975	0	0	1,443	468	0
Total Required Storage	**19,359**	**3,563**	**0**	**21,880**	**4,032**	**1,687**
Existing Available Storage (m^3)	26,614	0	0	26,614	0	0
Surplus (m^3)	**7,255**	**-3,563**	**0**	**4,734**	**-4,032**	**-1,687**

Storage – Mid Term

	Mid-Term Scenario 1 - City Growth Only			Mid-Term Scenario 2 - City +BBR		
Parameter	Zone 1	Zone 2	Zone 3	Zone 1	Zone 2	Zone 3
Cumulative Equivalent Population [(1)]	100,677	34,998	0	100,677	34,998	7,559
Fire Flow [(2)] (L/s)	378	357	0	378	357	171
Duration [(2)] (Hours)	6	5	0	6	5	3
A – Fire Storage [(3)] (m^3)	8,165	6,418	0	8,165	6,418	1,844
B – Equalization Storage [(4)] (m^3)	12,333	4,287	0	12,333	4,287	926
C – Emergency Storage [(5)] (m^3)	5,124	2,676	0	5,124	2,676	692
Storage Requirement Per Zone (m^3)	25,622	13,382	0	25,622	13,382	3,462
Additional Storage Requirement for Upper Zone (m3) - 25% of MDF	4,287	0		5,213	926	0
Total Required Storage	**29,910**	**13,382**	**0**	**30,836**	**14,308**	**3,462**
Existing Available Storage (m^3)	26,614			26,614		
Surplus (m^3)	**-3,296**	**-13,382**	**0**	**-4,222**	**-14,308**	**-3,462**

Storage – Long Term

	Long-Term Scenario 1 - City Growth Only			Long-Term Scenario 2 - City +BBR		
Parameter	Zone 1	Zone 2	Zone 3	Zone 1	Zone 2	Zone 3
Cumulative Equivalent Population [1]	109,857	35,854	0	109,857	35,854	11,294
Fire Flow [2] (L/s)	378	360	0	378	360	202
Duration [2] (Hours)	6	5	0	6	5	3
A – Fire Storage [3] (m^3)	8,165	6,484	0	8,165	6,484	2,186
B – Equalization Storage [4] (m^3)	13,458	4,392	0	13,458	4,392	1,384
C – Emergency Storage [5] (m^3)	5,406	2,719	0	5,406	2,719	892
Storage Requirement Per Zone (m^3)	27,028	13,595	0	27,028	13,595	4,462
Additional Storage Requirement for Upper Zone (m3) - 25% of MDF	4,392			5,776	1,384	0
Total Required Storage	**31,420**	**13,595**	**0**	**32,804**	**14,979**	**4,462**
Existing Available Storage (m^3)	26,614			26,614		
Surplus (m^3)	**-4,806**	**-13,595**	**0**	**-6,190**	**-14,979**	**-4,462**

Discrepancies Noted with Jewell's Report

Table 2-2: Calculation of ADD (from Dillon)

Water User	Servicing Report [L/c/d]	MOECC [L/c/d]	Design [L/c/d]	Population [cap] or Area [m2]	ADD [L/s]
RESIDENTIAL	350	270 to 450	350	9147 cap	37.1
RESORT A	500	225	500	250 cap	1.5
RESORT B	500	225	500	250 cap	1.5
HARMONY RD.	350	270 to 450	350	486 cap	1.97
FOXBORO	350	270 to 450	350	450 cap	1.82
JAMES PROPERTY	NA	270 to 450	350	4560 cap	18.48
SCHOOL (HARMONY RD.)	NA	70 to 140 L/Student/8 hrs	140 L/Student/8 hrs	900 cap	4.38
COMMUNITY CENTER (HARMONY RD.)	NA	NA	140 L/person/8 hrs	173 cap	0.84
COMMERCIAL	5 L/m2/day	2.5 to 5 L/m2/day	5 L/m2/day	38,277 m2	2.22
Total					**69.81**

Not included

Corbyville (Zone 2); less population

Less flow

Storage Upgrades Summary

Storage Deficiencies	Short-Term Scenario 1 - City Growth Only	Short-Term Scenario 2 - City + BBR	Mid-Term Scenario 1 - City Growth Only	Mid-Term Scenario 2 - City +BBR	Long-Term Scenario 1 - City Growth Only	Long-Term Scenario 2 - City Growth +BBR
Zone 1	N/A	N/A	-3,296	-4,222	-4,806	-6,190
Zone 2	-3,563	-4,032	-13,382	-14,308	-13,595	-14,979
Zone 3	N/A	-1,687	N/A	-3,462	N/A	-4,462

- According to Thurlow Water Pressure Study and Master Plan, a floating storage was recommended in Zone 2 to support future growth → Based on JLR's results, this recommendation is being carried forward.
- The storage capacity increase can be achieved via a phased approach, e.g., add floating storage for short-term and add in-ground storage for mid- and long-term.

Water Booster Station

Existing Booster Stations

	ADD	MDD[1]	Suff. Floating Storage	Firm Capacity	MDD of Firm Capactiy	Stand-By Capacity	Add OF STAND-by Capacity	LOS Criteria Meet
	(Ml/d)	(ML/D)						
Existing								
Belleville Zone 1	19.18	26.85	☑	107.20	**25.05%**	116.39	**16.48%**	☑
Belleville - Zone 2	2.41	16.77		3.46	**485.18%**	3.46	**69.77%**	☒
Belleville Zone 3	0.00	0.00		0.00	**0.00%**	4.00	**0.00%**	☑
Short Term								
Belleville Zone 1 w/o BBR	23.39	32.74	☑	107.20	**30.54%**	116.39	**20.09%**	☑
Belleville Zone 1 w/ BBR	23.39	32.74	☑	107.20	**30.54%**	116.39	**20.09%**	☑
Belleville - Zone 2 w/o BBR	2.79	18.93		3.46	**547.82%**	3.46	**80.59%**	☒
Belleville - Zone 2 w/ BBR	2.79	18.93		3.46	**547.82%**	3.46	**80.59%**	☒
Belleville Zone 3 w/o BBR	0.00	0.00		0.00	**0.00%**	4.00	**0.00%**	☑
Belleville Zone 3 w/ BBR	1.34	1.87		0.00	**0.00%**	4.00	**33.46%**	☒
Mid Term								
Belleville Zone 1 w/o BBR	35.24	49.33	☑	107.20	**46.02%**	116.39	**30.27%**	☑
Belleville Zone 1 w/ BBR	35.24	49.33	☑	107.20	**46.02%**	116.39	**30.27%**	☑
Belleville - Zone 2 w/o BBR	12.25	47.99		3.46	**1388.72%**	3.46	**354.44%**	☒
Belleville - Zone 2 w/ BBR	12.25	47.99		3.46	**1388.72%**	3.46	**354.44%**	☒
Belleville Zone 3 w/o BBR	0.00	0.00		0.00	**0.00%**	4.00	**0.00%**	☑
Belleville Zone 3 w/ BBR	2.65	3.70		0.00	**0.00%**	4.00	**66.15%**	☒
Long Term								
Belleville Zone 1 w/o BBR	38.45	53.83	☑	107.20	**50.21%**	116.39	**33.03%**	☑
Belleville Zone 1 w/ BBR	38.45	53.83	☑	107.20	**50.21%**	116.39	**33.03%**	☑
Belleville - Zone 2 w/o BBR	12.55	48.67		3.46	**1408.35%**	3.46	**363.11%**	☒
Belleville - Zone 2 w/ BBR	12.55	48.67		3.46	**1408.35%**	3.46	**363.11%**	☒
Belleville Zone 3 w/o BBR	0.00	0.00		0.00	**0.00%**	4.00	**0.00%**	☑
Belleville Zone 3 w/ BBR	3.95	5.53		0.00	**0.00%**	4.00	**98.83%**	☒

Note 1: Zone 2 does not have adequate floating storage and therefore is need to provide the greater of the peak hour demand or maximum day plus fire demand

Booster Station Upgrades

	ADD (Ml/d)	MDD (ML/D)	Suff. Floating Storage ***	Firm Capacity	MDD of Firm Capactiy	Stand-By Capacity	Add OF STAND-by Capacity	LOS Criteria Meet
Existing								
Belleville Zone 1	19.18	26.85	☑	107.20	**25.05%**	116.39	**16.48%**	☑
Belleville - Zone 2	2.41	16.77 **		3.46	**485.18%**	3.46	**69.77%**	☒
Belleville Zone 3	0.00	0.00		0.00	**0.00%**	4.00	**0.00%**	☑
Short Term	**0.00**	**0.00**	**0.00**	**0.00**		**0.00**		
Belleville Zone 1 w/o BBR	23.39	32.74	☑	107.20	**30.54%**	116.39	**20.09%**	☑
Belleville Zone 1 w/ BBR	23.39	32.74	☑	107.20	**30.54%**	116.39	**20.09%**	☑
Belleville - Zone 2 w/o BBR*	2.79	3.90	☑	**17.28**	**22.56%**	17.28	**16.12%**	☑
Belleville - Zone 2 w/ BBR*	2.79	3.90	☑	**17.28**	**22.56%**	17.28	**16.12%**	☑
Belleville Zone 3 w/o BBR	0.00	0.00	☑	**4.00**	**0.00%**	4.00	**0.00%**	☑
Belleville Zone 3 w/ BBR	1.34	1.87	☑	**4.00**	**46.85%**	4.00	**33.46%**	☑
Mid Term	**0.00**	**0.00**	**0.00**	**0.00**		**0.00**		
Belleville Zone 1 w/o BBR	35.24	49.33	☑	107.20	**46.02%**	116.39	**30.27%**	☑
Belleville Zone 1 w/ BBR	35.24	49.33	☑	107.20	**46.02%**	116.39	**30.27%**	☑
Belleville - Zone 2 w/o BBR*	12.25	17.15	☑	**17.28**	**99.24%**	17.28	**70.89%**	☑
Belleville - Zone 2 w/ BBR*	12.25	17.15	☑	**17.28**	**99.24%**	17.28	**70.89%**	☑
Belleville Zone 3 w/o BBR	0.00	0.00	☑	**4.00**	**0.00%**	4.00	**0.00%**	☑
Belleville Zone 3 w/ BBR	2.65	3.70	☑	**4.00**	**92.60%**	4.00	**66.15%**	☑
Long Term	**0.00**	**0.00**	**0.00**	**0.00**		**0.00**		
Belleville Zone 1 w/o BBR	38.45	53.83	☑	107.20	**50.21%**	116.39	**33.03%**	☑
Belleville Zone 1 w/ BBR	38.45	53.83	☑	107.20	**50.21%**	116.39	**33.03%**	☑
Belleville - Zone 2 w/o BBR*	12.55	17.57	☑	**27.65**	**63.54%**	27.65	**45.39%**	☑
Belleville - Zone 2 w/ BBR*	12.55	17.57	☑	**27.65**	**63.54%**	27.65	**45.39%**	☑
Belleville Zone 3 w/o BBR	0.00	0.00	☑	**8.00**	**0.00%**	8.00	**0.00%**	☑
Belleville Zone 3 w/ BBR	3.95	5.53	☑	**8.00**	**69.18%**	8.00	**49.41%**	☑

Note: *Firm capacity includes fire pump. Capacity of BS should be reviewed to be more required capacity and pump requirments

** MDD +FF *** After floating storage is added.

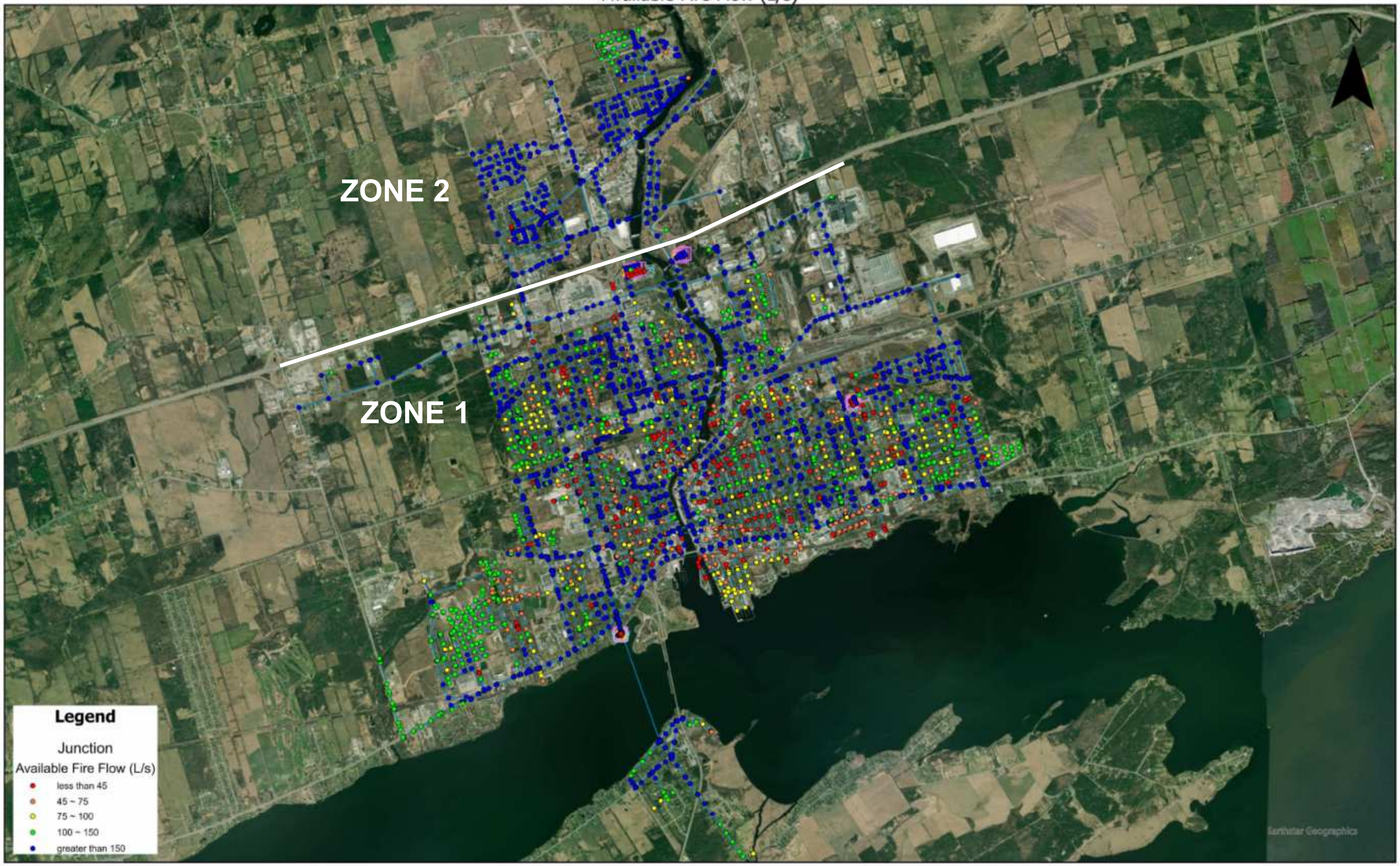
Water Distribution

Future Water Servicing – Design Criteria

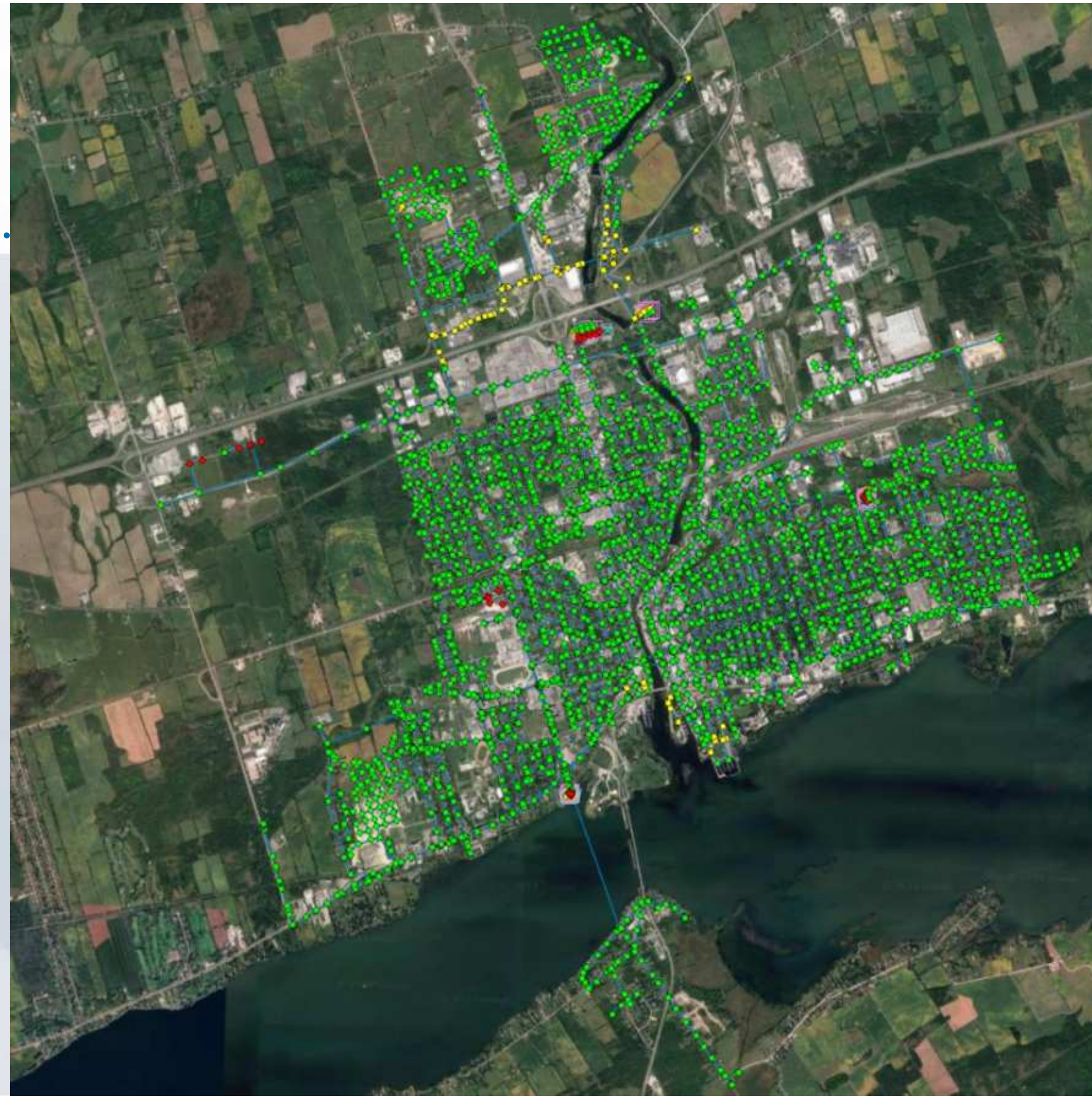
- Zone delineation:
  - Maintain existing Zone 1 for south of HWY 401
  - Maintain existing Zone 2 for Cannifton and include Corbyville
  - Create a new Zone 3 for Black Bear Ridge

- Triggers:
  - Under domestic usage, pressure shall maintain between 40-80 psi under average day, max day and peak hour conditions. When pressure falls outside of this range, an upgrade will be recommended.
  - Fire flow shall be maintained within 5% model output with and without BBR for each of the future time period. If the fire flow reduction is more than 5%, an upgrade will be recommended.

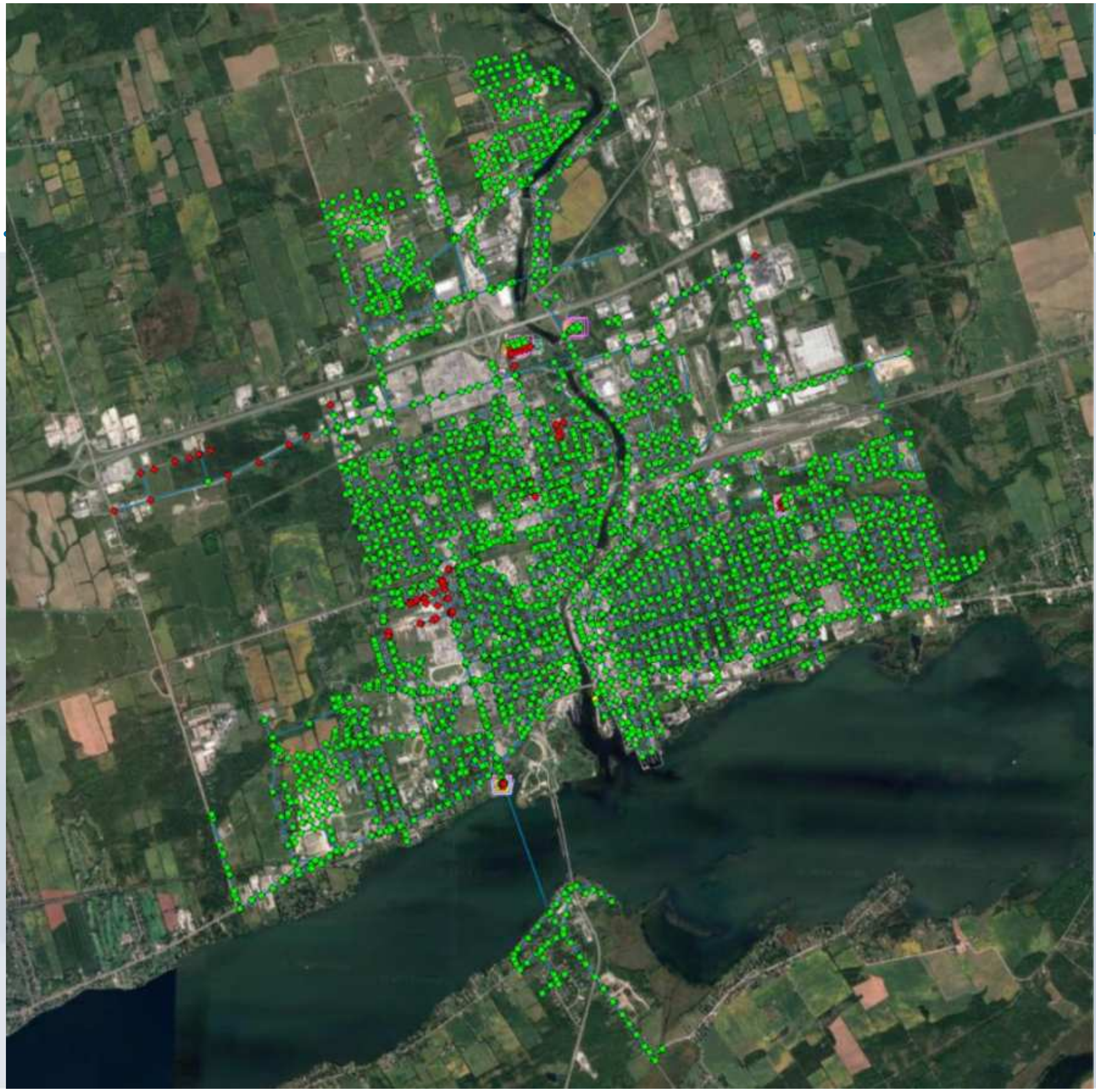
Belleville Existing System - Maximum Day Plus Fire Flow
Available Fire Flow (L/s)



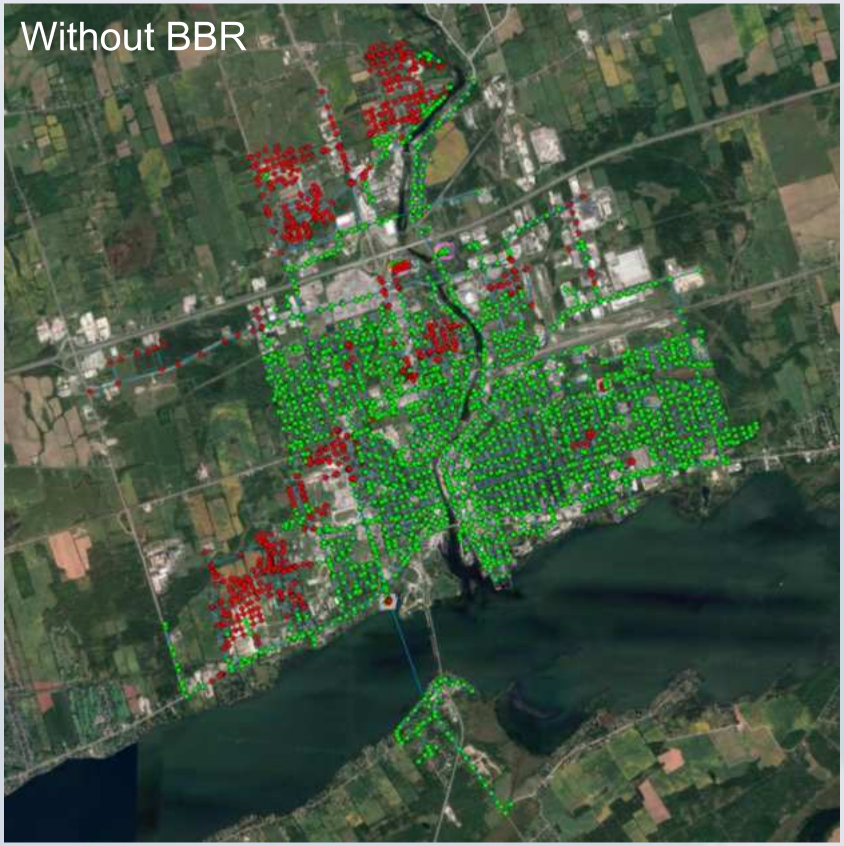
Existing Max Day

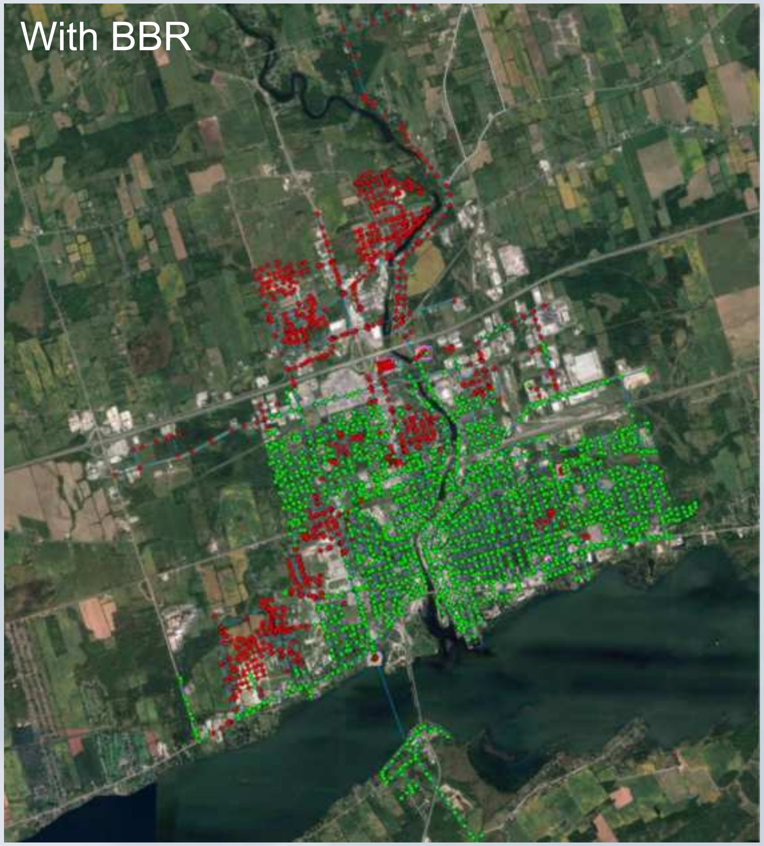


Existing Peak Demand (PHD)

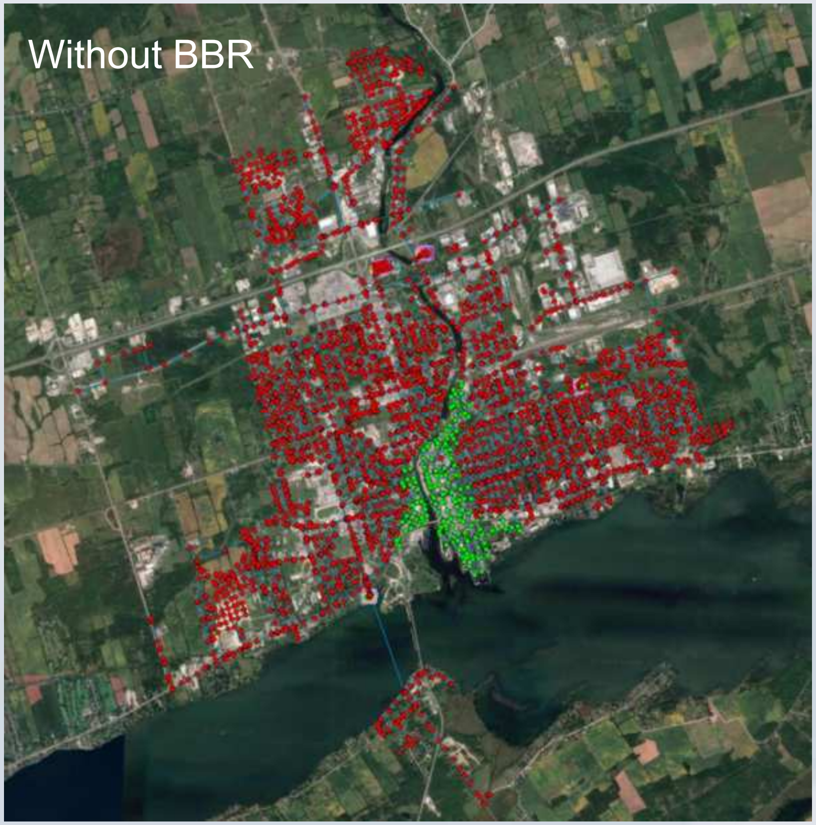


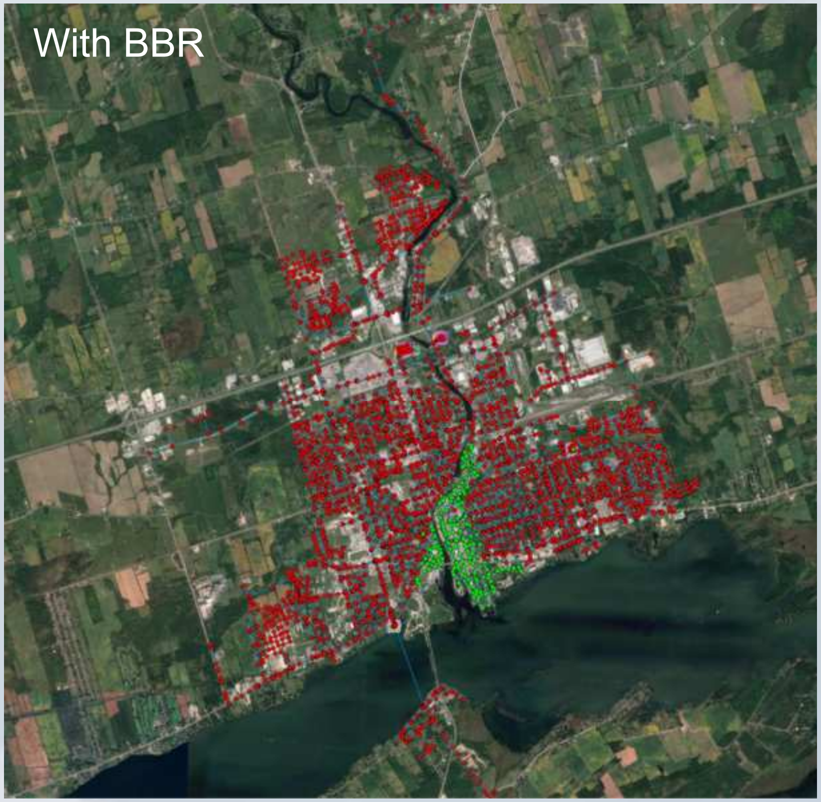
Short-Term (PHD)



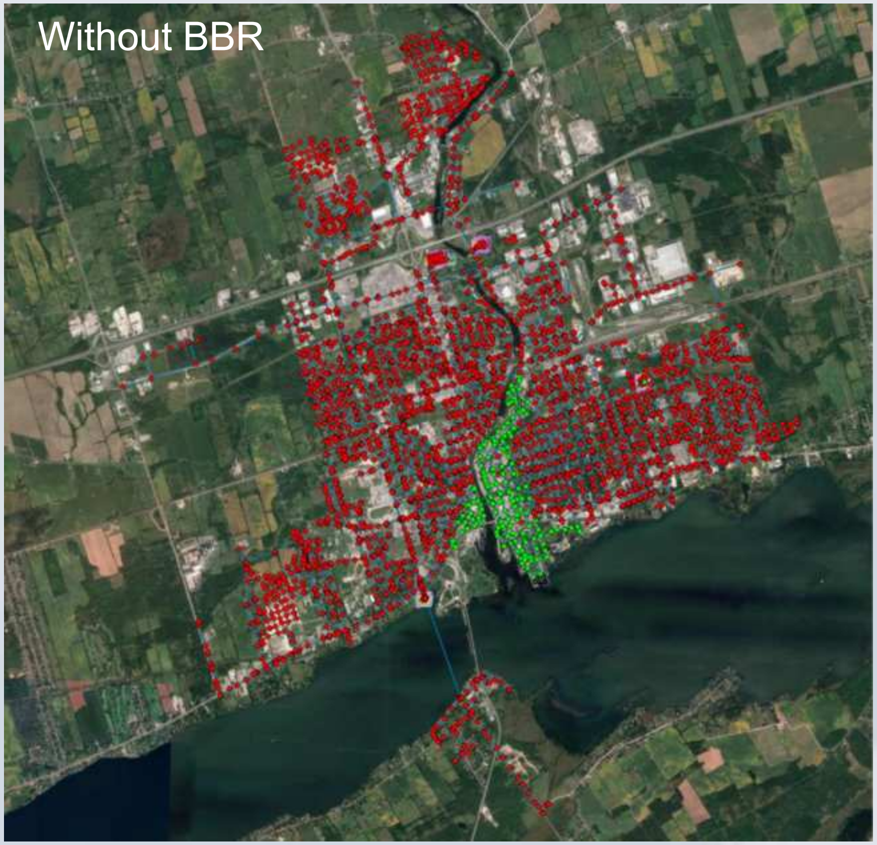


Mid-Term (PHD)





Long-Term (PHD)



How do we address Zone 1 deficiencies? Long-Term PHD

Option 1

- North Park pump upgraded and set to John Street Tank’s existing HGL (132.9m)

Option 2

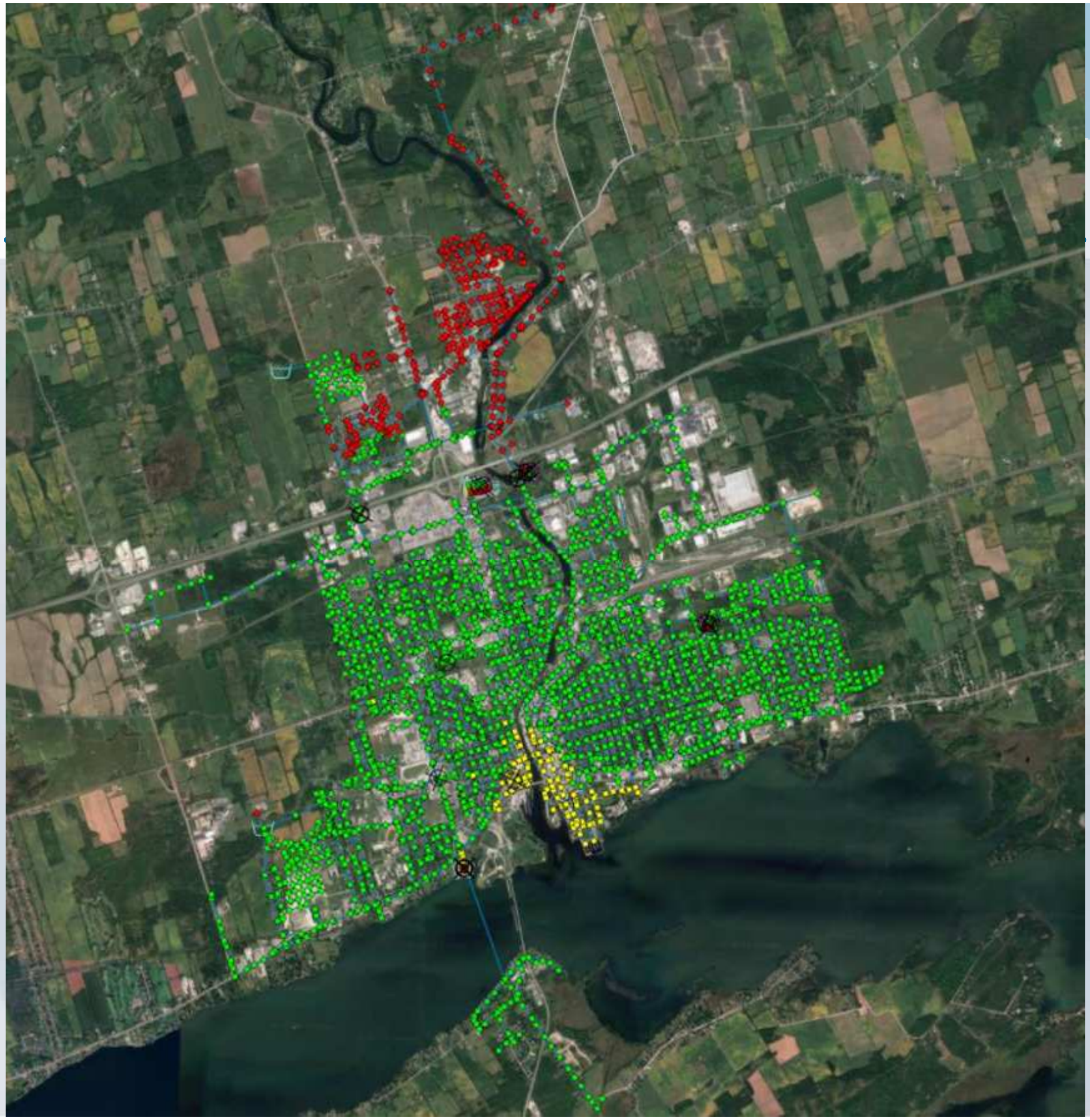
- Increase North Park and John Street both to John Street Tower’s maximum HGL (138m)

Option 3

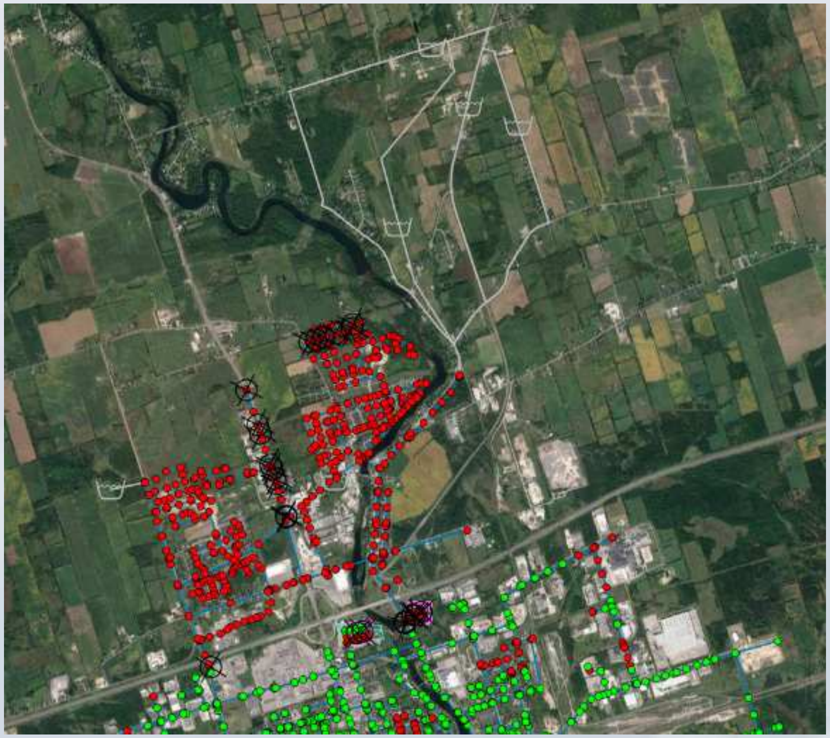
- Add a new reservoir and/or pumping station near Avonlough

Black Bear Impact on Zone 1

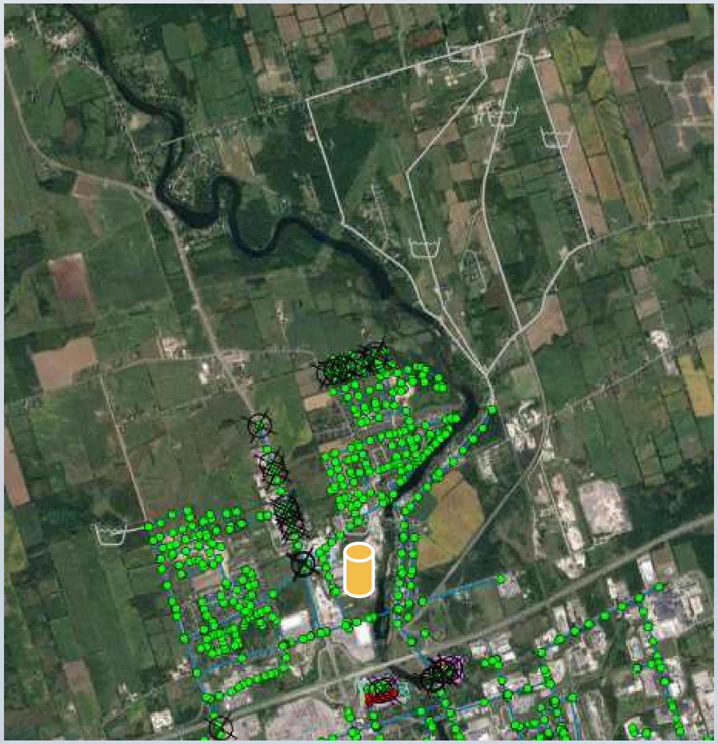
- Adam St. Booster Station is turned off in model, assuming floating storage is being provided in Zone 2.
- Zone 1 will not be affected by BBR once the previous upgrades are completed.



How do we address Zone 2 deficiencies? Long-Term PHD

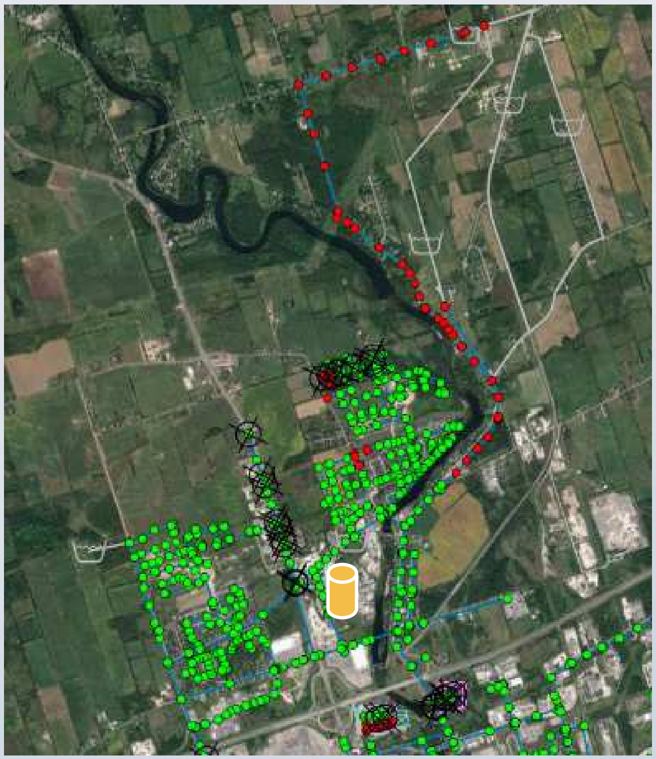


- No floating storage

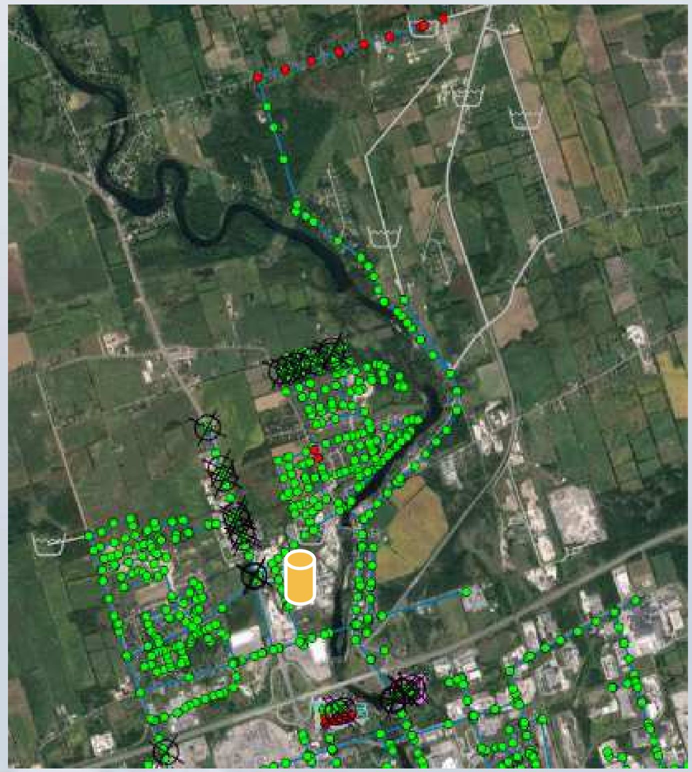


- With floating storage

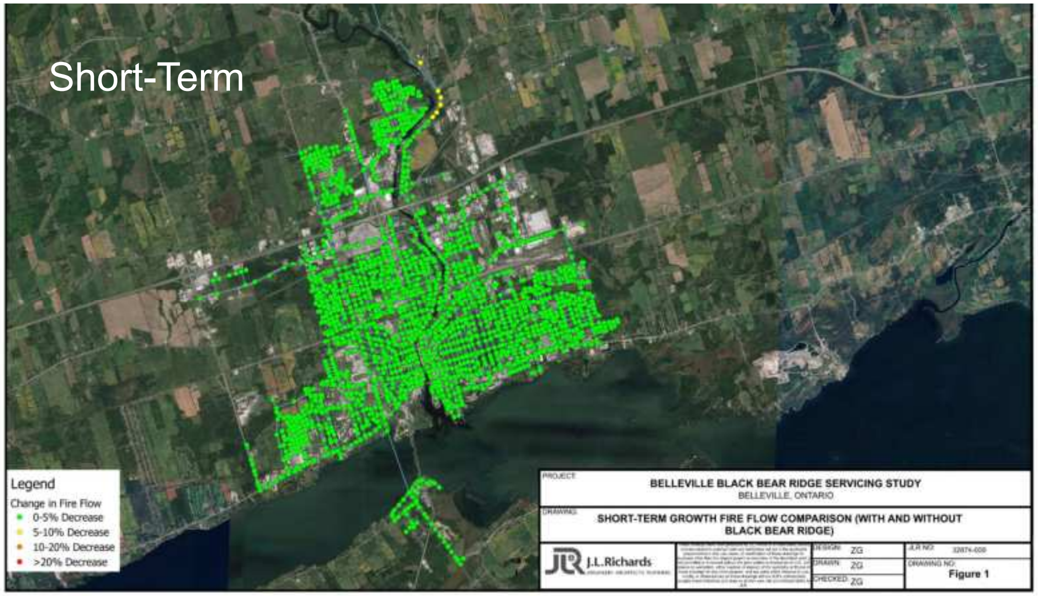
Black Bear Impact on Zone 2 Long-Term PHD

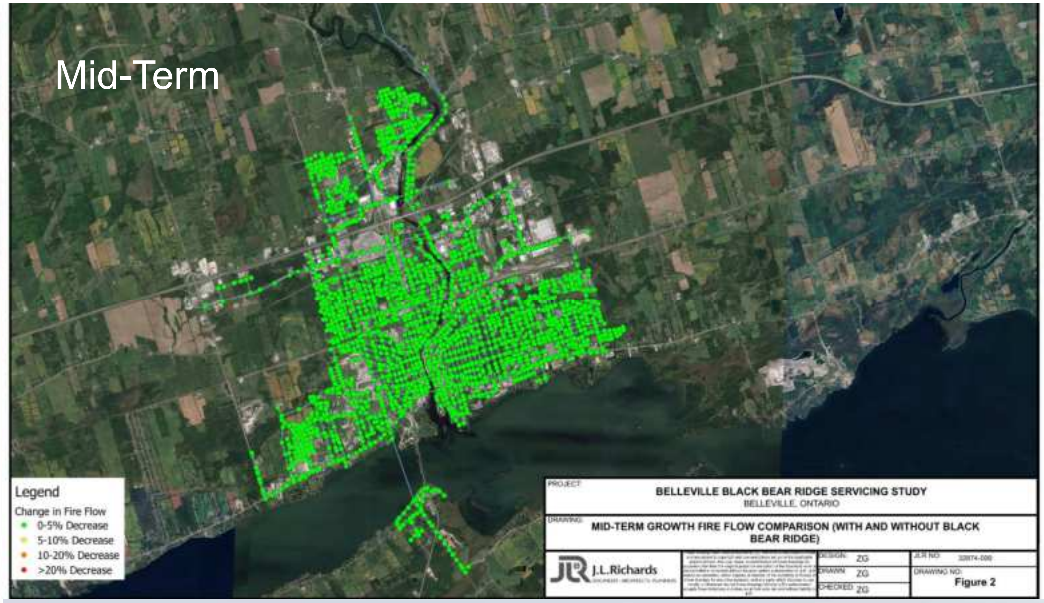


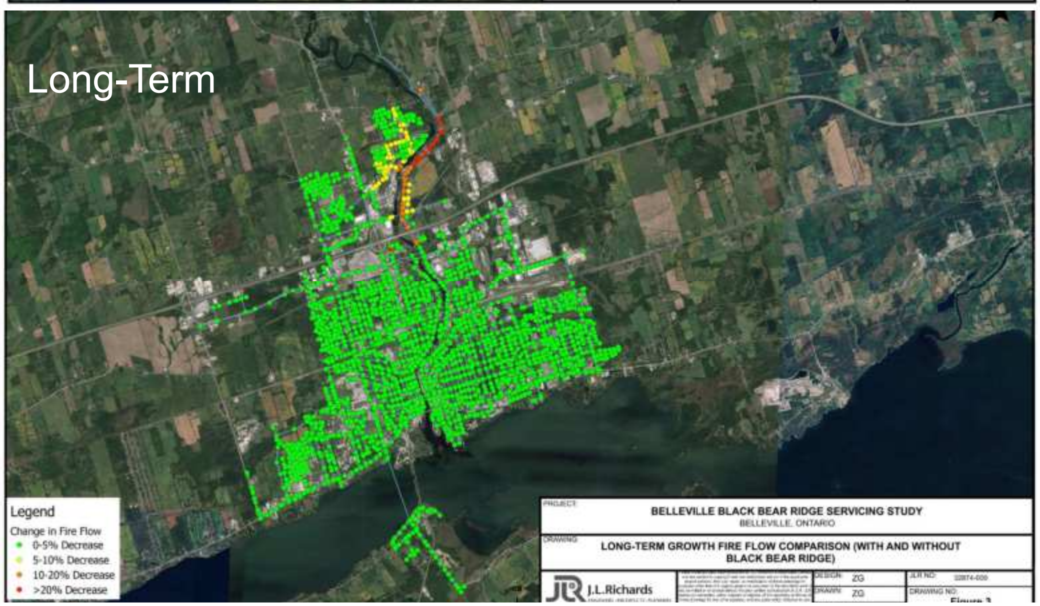
- With floating storage
- No upgrades along Cannifton Rd. N



- With floating storage
- Upgrades along Cannifton Rd. N





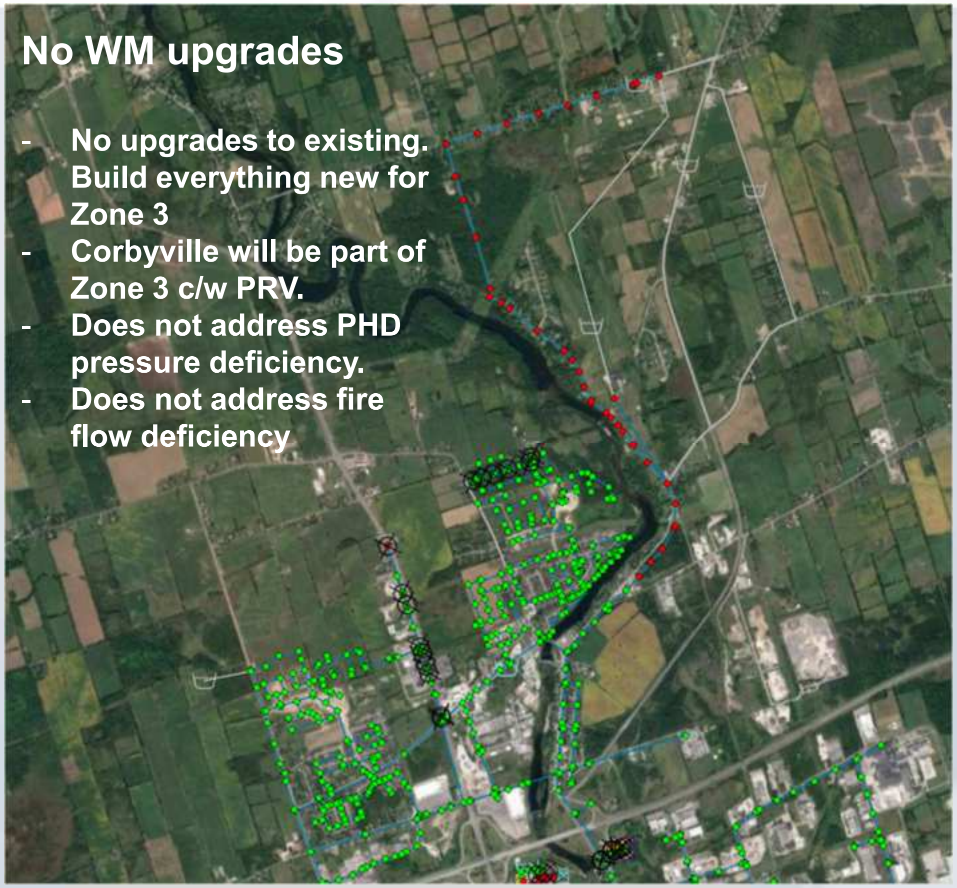


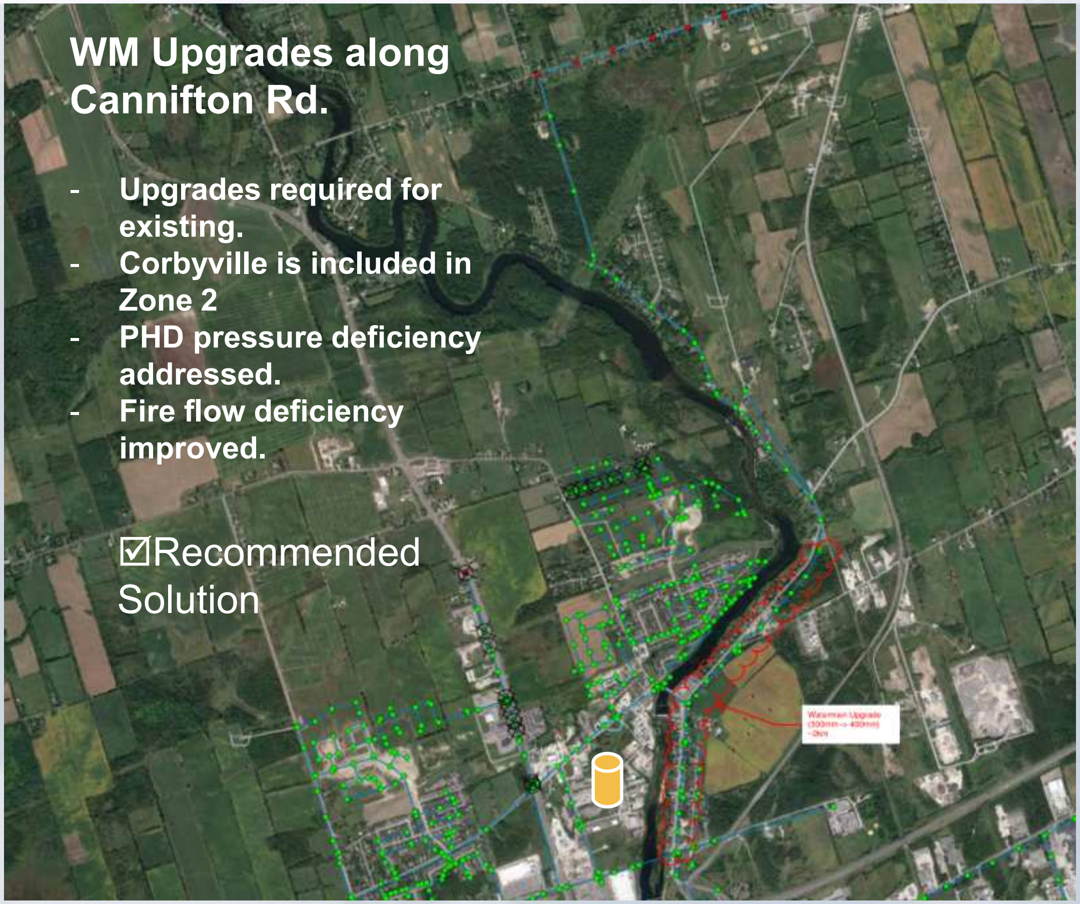
Fire Flow Change Overtime with and without BBR

→ Design consideration: Fire flow shall be maintained within 5% with and without BBR for each time period.

→ Supports the recommendation of upgrading WM along Cannifton Rd. N

Zone 2 Cannifton Rd. N WM Upgrades - Pros/Cons





PHD Change Over Time

Peak Hour Demand - Zone 1									
Pressure (kPa)		EXISTING	S1 SHORT	S1 MID	S1 LONG	S2 SHORT	S2 MID	S2 LONG
From	To							
	<=276	2.6%	0.7%	0.8%	0.8%	0.7%	0.8%	0.8%
>276	<=350	35.4%	6.7%	11.3%	11.5%	6.7%	11.3%	11.5%
>350	<=480	52.8%	74.4%	72.4%	72.2%	74.4%	72.4%	72.3%
>480	<=552	9.1%	15.5%	14.2%	14.1%	15.5%	14.1%	14.1%
>552	<=689	0.0%	2.7%	1.3%	1.3%	2.7%	1.3%	1.3%
>689		0%	0%	0%	0%	0%	0%	0%

Peak Hour Demand - Zone 2								
Pressure (kPa)		EXISTING	S1 SHORT	S1 MID	S1 LONG	S2 SHORT	S2 MID	S2 LONG
From	To							
	<=276	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.4%
>276	<=350	12.6%	0.0%	16.6%	17.4%	0.6%	24.2%	34.3%
>350	<=480	75.6%	73.7%	70.5%	68.9%	74.9%	67.5%	60.7%
>480	<=552	11.8%	22.6%	13.6%	13.6%	21.4%	9.0%	5.4%
>552	<=689	0.0%	4.4%	0.0%	0.0%	3.8%	0.0%	0.0%
>689		0%	0%	0%	0%	0%	0%	0%

- S1 (Scenario 1) – Without BBR
- S2 (Scenario 2) – With BBR

- Generally, the flow change over time remains within the desirable range with and without BBR.

Max Day + Fire Flow Change Over Time

MDDFF - Zone 1									
Fire Flow (L/s)		EXISTING	S1 SHORT	S1 MID	S1 LONG	S2 SHORT	S2 MID	S2 LONG
From	To							
	<45	5.5%	5.8%	6.0%	5.9%	5.8%	6.0%	5.9%
>=45	<=75	8.6%	9.4%	9.9%	9.9%	9.5%	9.9%	10.0%
>75	<=100	10.8%	10.5%	10.6%	10.6%	10.4%	10.6%	10.6%
>100	<=150	19.9%	15.1%	15.1%	15.0%	15.0%	15.1%	15.0%
>150		55.3%	59.3%	58.4%	58.5%	59.3%	58.4%	58.5%

MDDFF - Zone 2								
Fire Flow (L/s)		EXISTING	S1 SHORT	S1 MID	S1 LONG	S2 SHORT	S2 MID	S2 LONG
From	To							
	<45	0.2%	1.0%	1.0%	1.0%	1.0%	1.0%	1.0%
>=45	<=75	1.0%	1.0%	5.6%	5.6%	1.2%	5.6%	5.6%
>75	<=100	0.0%	5.0%	1.0%	1.0%	5.0%	1.0%	1.2%
>100	<=150	6.6%	5.4%	11.7%	11.7%	5.4%	11.7%	12.9%
>150		92.2%	87.7%	80.7%	80.7%	87.5%	80.7%	79.3%

- S1 (Scenario 1) – Without BBR
- S2 (Scenario 2) – With BBR

- Generally, the flow change over time remains within the desirable range with and without BBR.

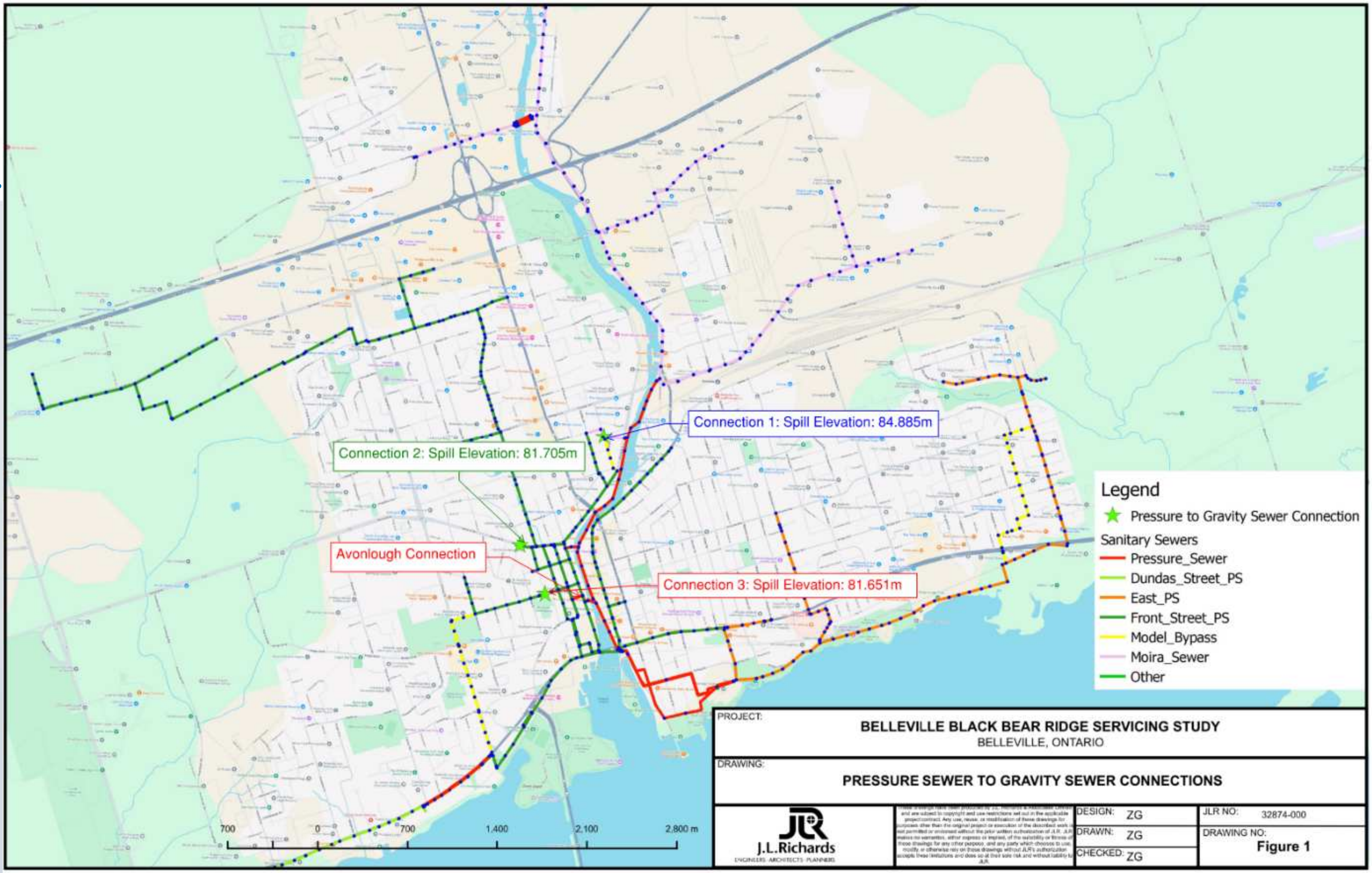
Sanitary

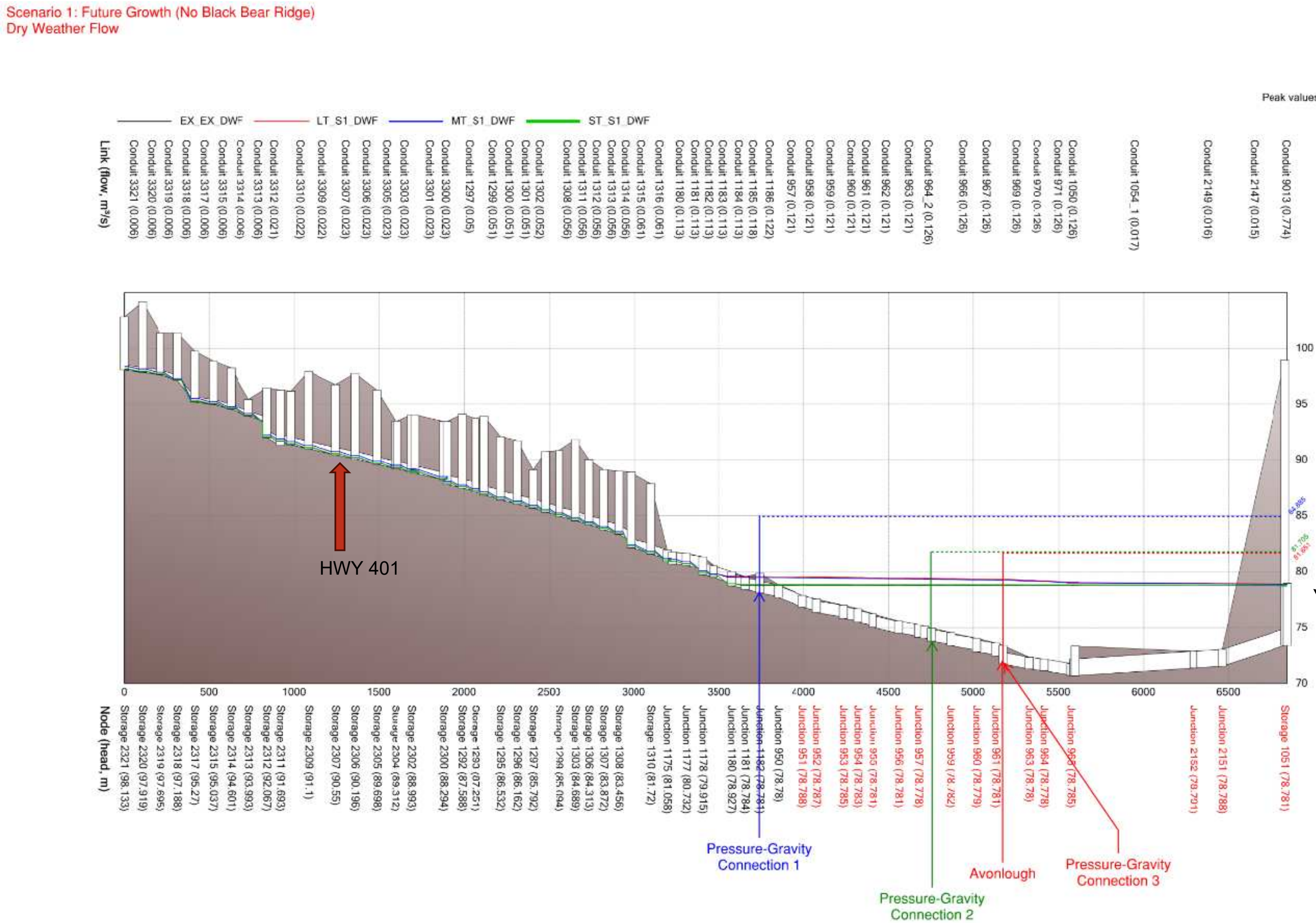
Future Sanitary Servicing - Design Criteria

- Gravity Sewers:
  - Sewer capacity greater than dry weather flow
  - HGL within 300mm of the pipe obvert or greater than 2m below finished ground during the specified rainfall derived infiltration and inflow (RDII) event
- Pumping Stations
  - Pump station firm capacity greater than the 1:10-year RDII flow
  - Pump station peak capacity greater than the 1:100-year RDII flow
- Pressure Sewers
  - Velocity greater than 0.9m/s in dry weather flow

Future Sanitary Servicing - Methodology

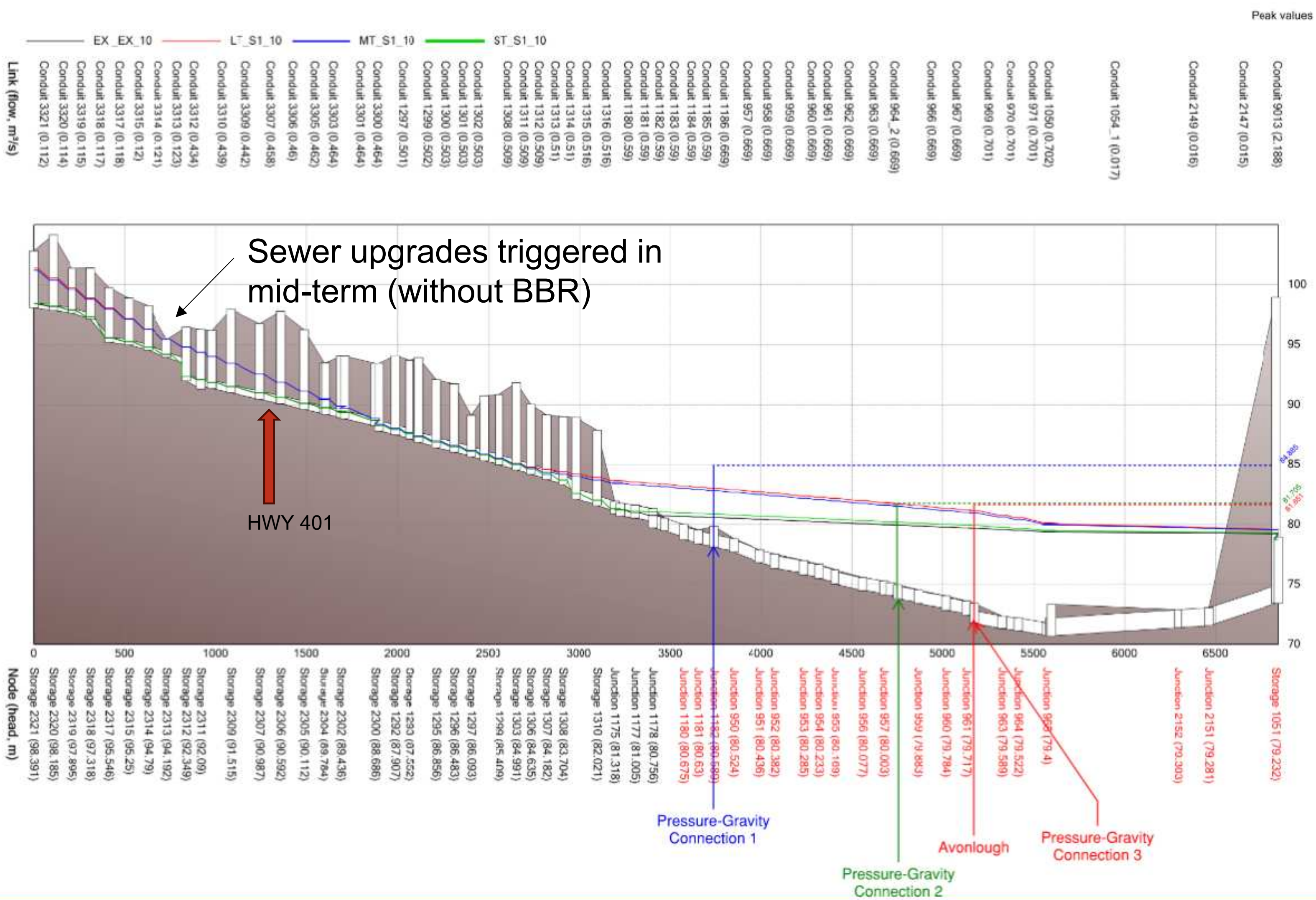
- Model scenarios:
  - Dry weather flow
  - 1:10 year storm
  - 1:100 year storm
- BBR discharge location:
  - Option 1: Connection at north-end of Cannifton Rd. N sewer
  - Option 2: Connection at Black Diamond Rd.


Connection 1: Spill Elevation: 84.885m
Connection 2: Spill Elevation: 81.705m
Avonlough Connection
Connection 3: Spill Elevation: 81.651m
Legend
Pressure to Gravity Sewer Connection
Sanitary Sewers
Pressure_Sewer
Dundas_Street_PS
East_PS
Front_Street_PS
Model_Bypass
Moira_Sewer
Other
700
0
700
1,400
2,100
2,800 m
PROJECT:
BELLEVILLE BLACK BEAR RIDGE SERVICING STUDY
BELLEVILLE, ONTARIO
DRAWING:
PRESSURE SEWER TO GRAVITY SEWER CONNECTIONS
J.L.Richards
ENGINEERS · ARCHITECTS · PLANNERS
DESIGN: ZG
DRAWN: ZG
CHECKED: ZG
JLR NO: 32874-000
DRAWING NO:
Figure 1

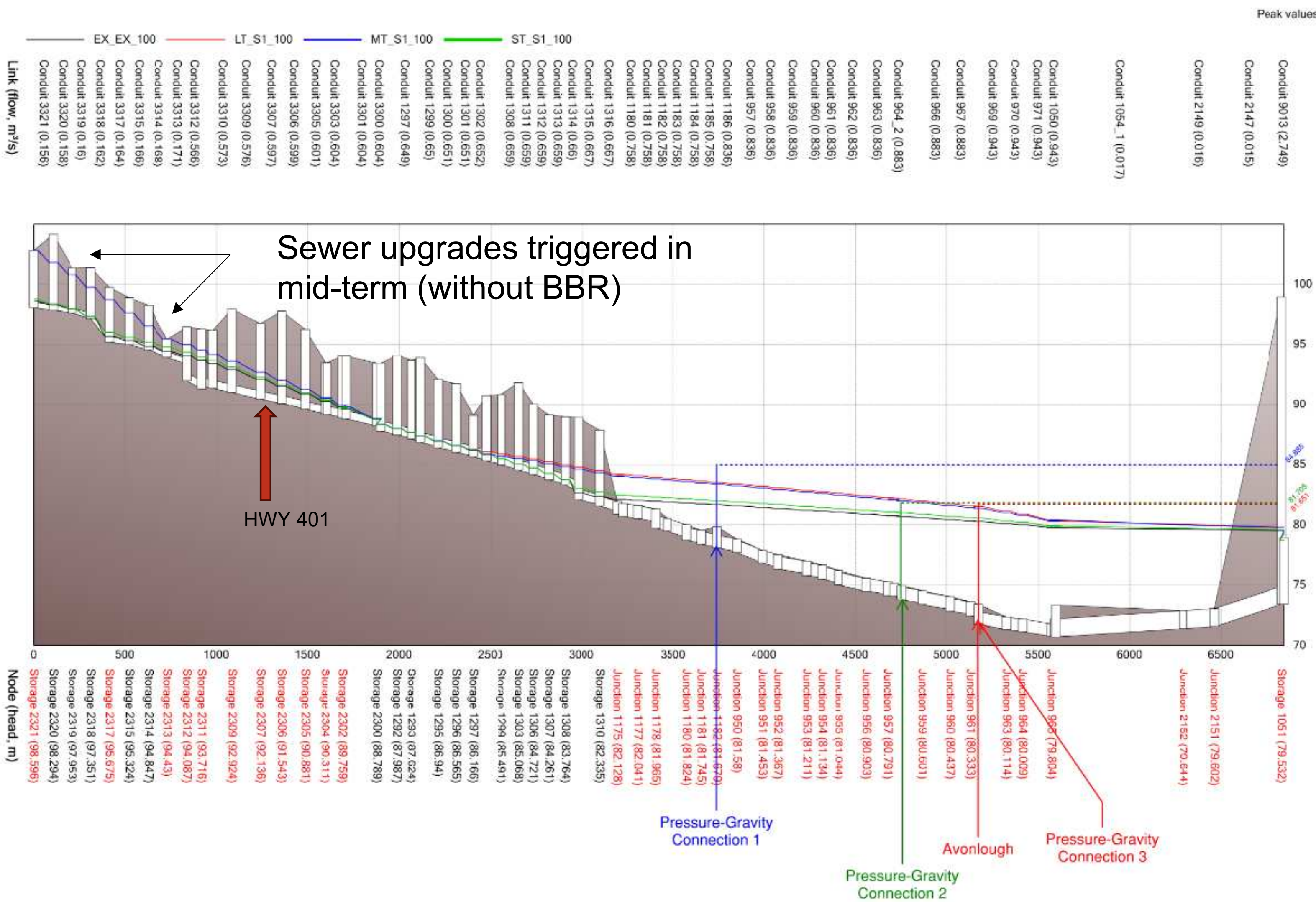


No issue
(HGL below spill elevation)

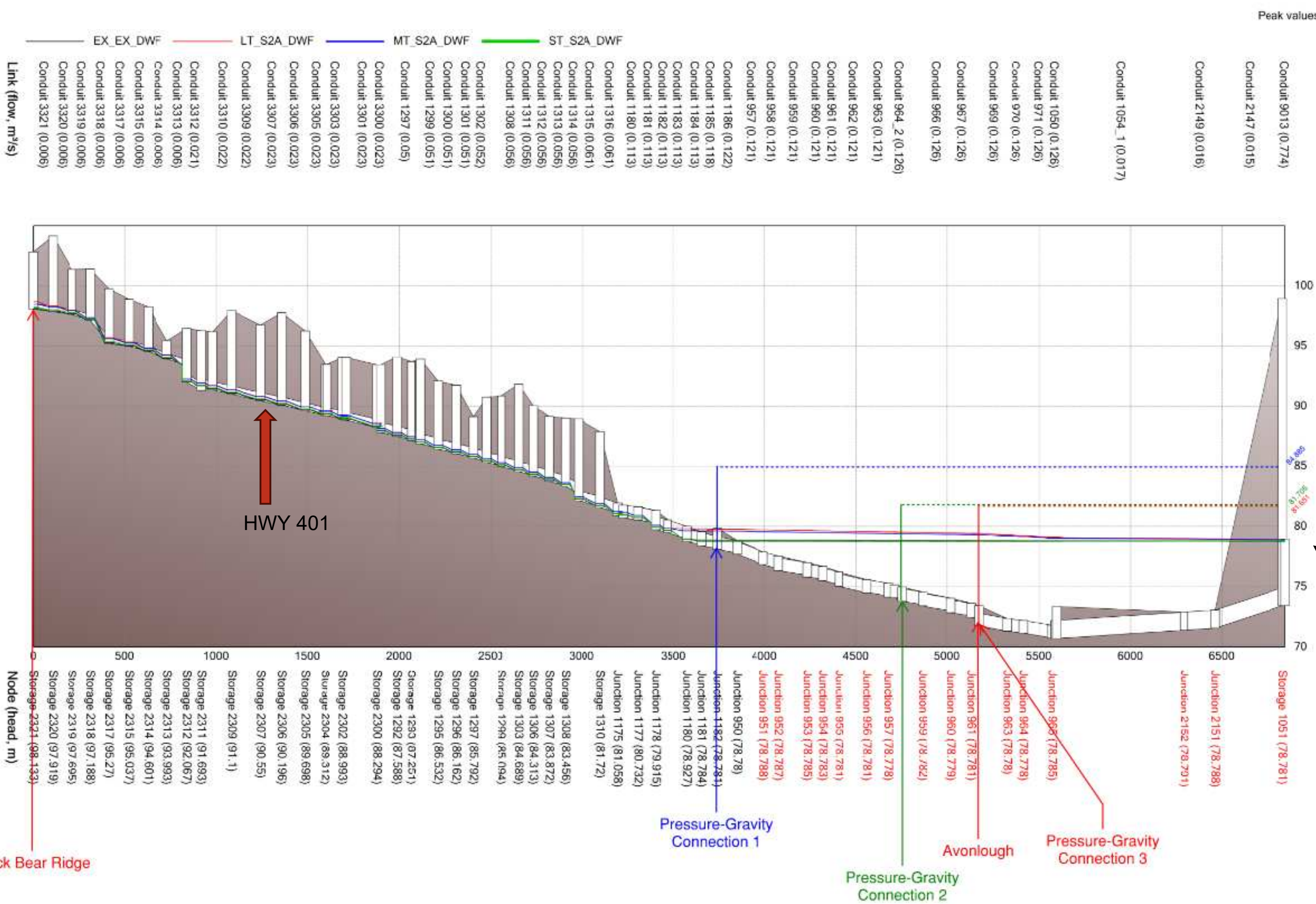
Scenario 1: Future Growth (No Black Bear Ridge)
1:10-Year Storm



Scenario 1: Future Growth (No Black Bear Ridge)
1:100-Year Storm

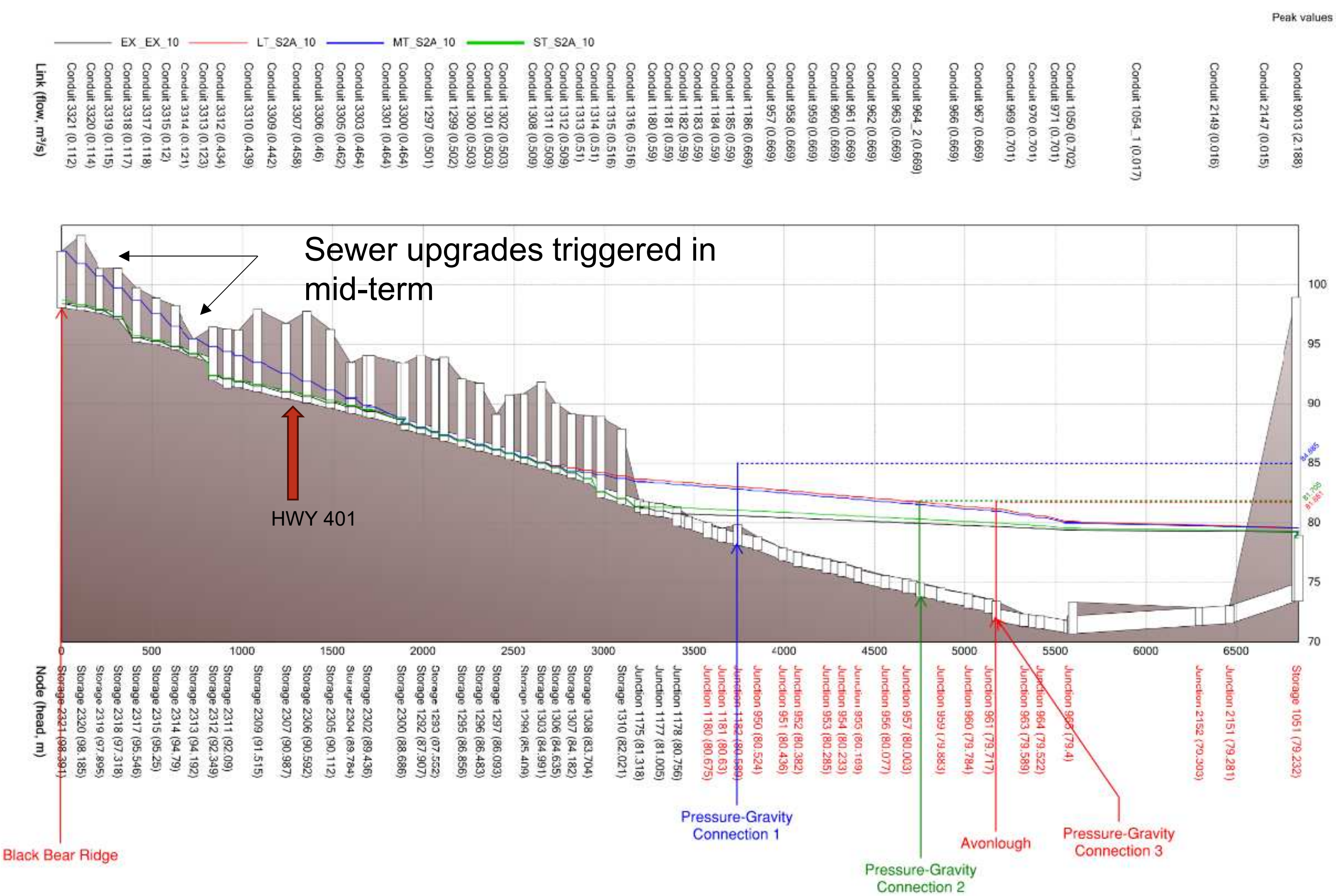


Scenario 2A: Future Growth with Black Bear Ridge Connection at most
Northern Point of Trunk Sewer
Dry Weather Flow

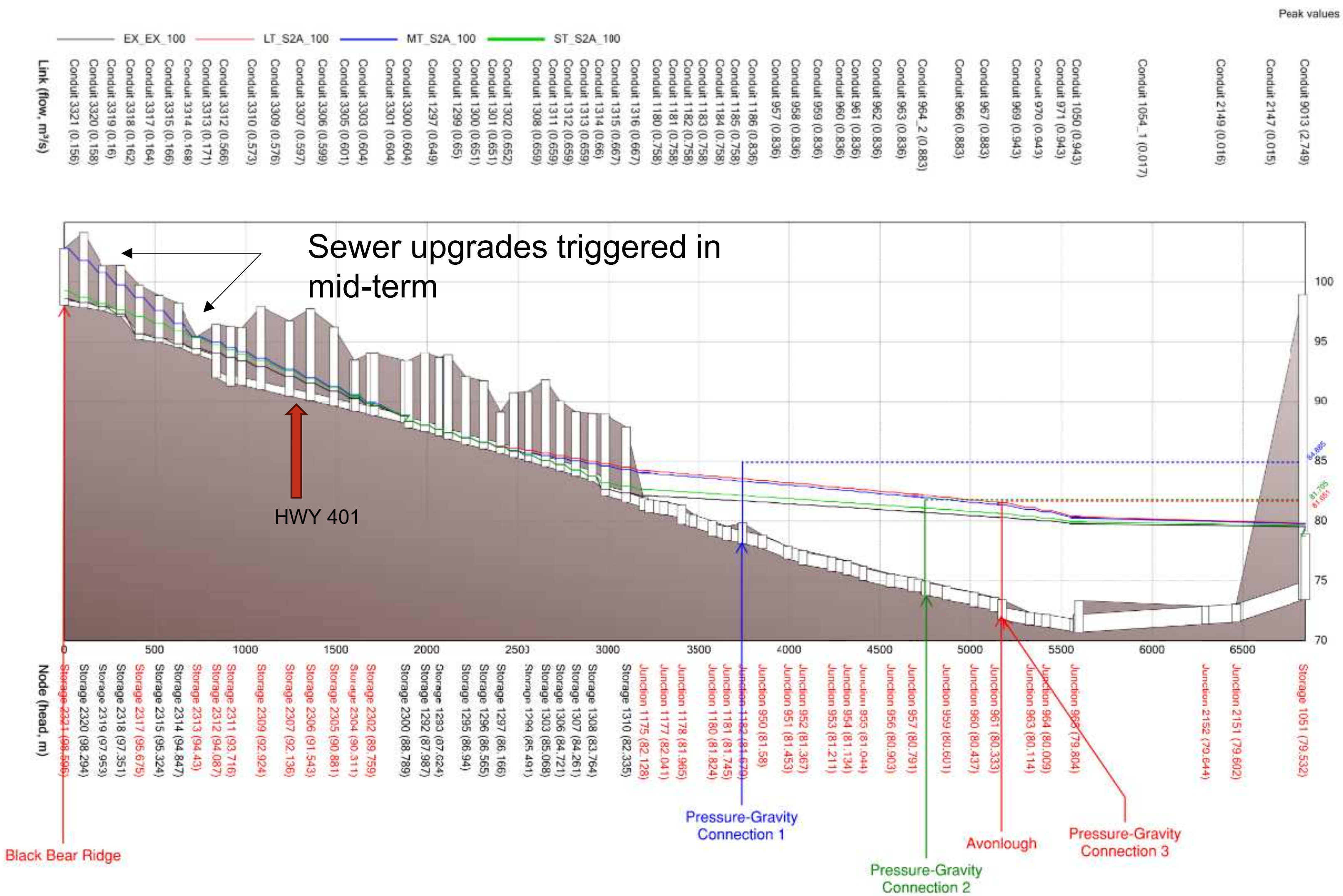


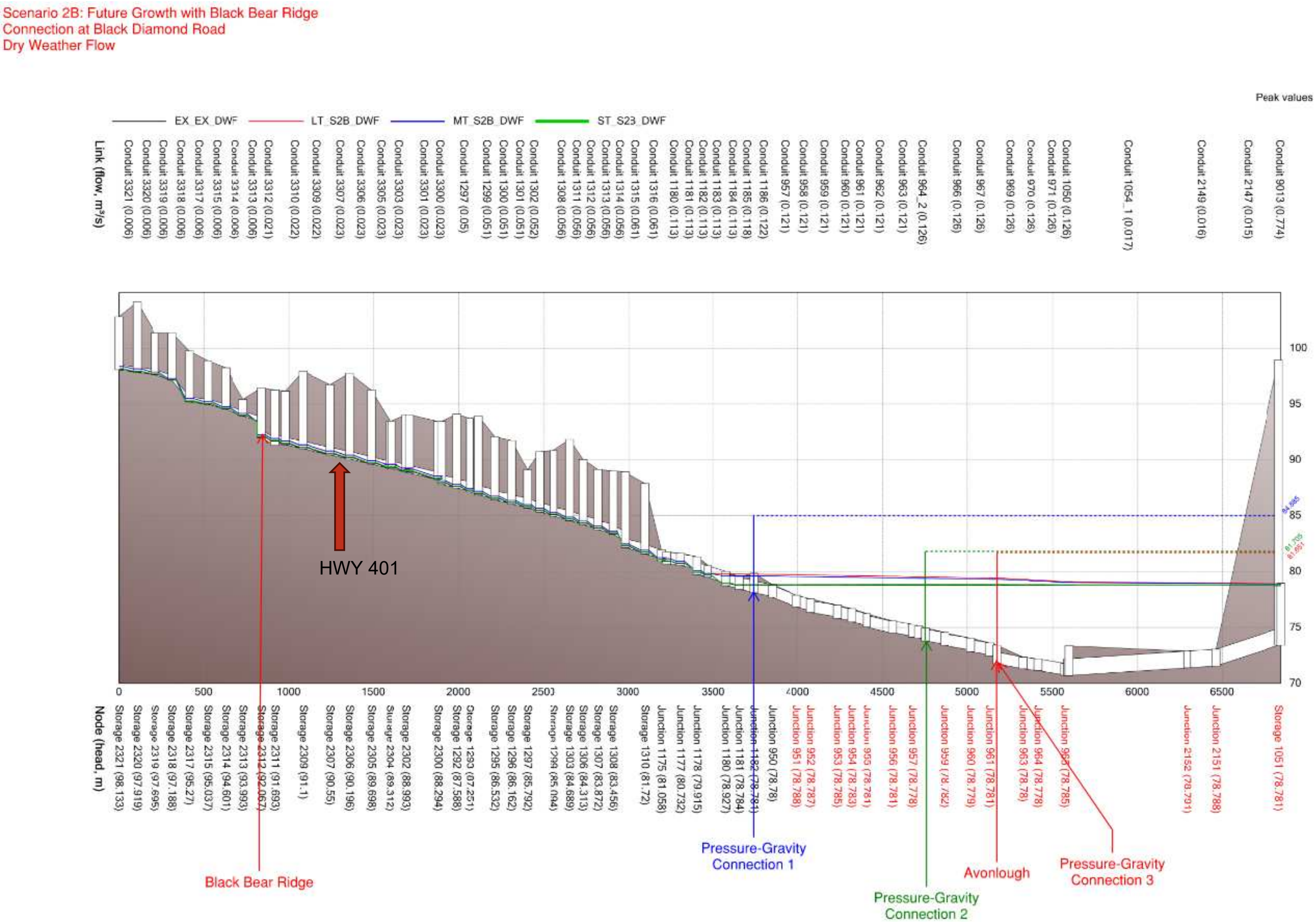
No issue
(HGL below spill elevation)

Scenario 2A: Future Growth with Black Bear Ridge Connection at most Northern Point of Trunk Sewer
1:10-Year Storm



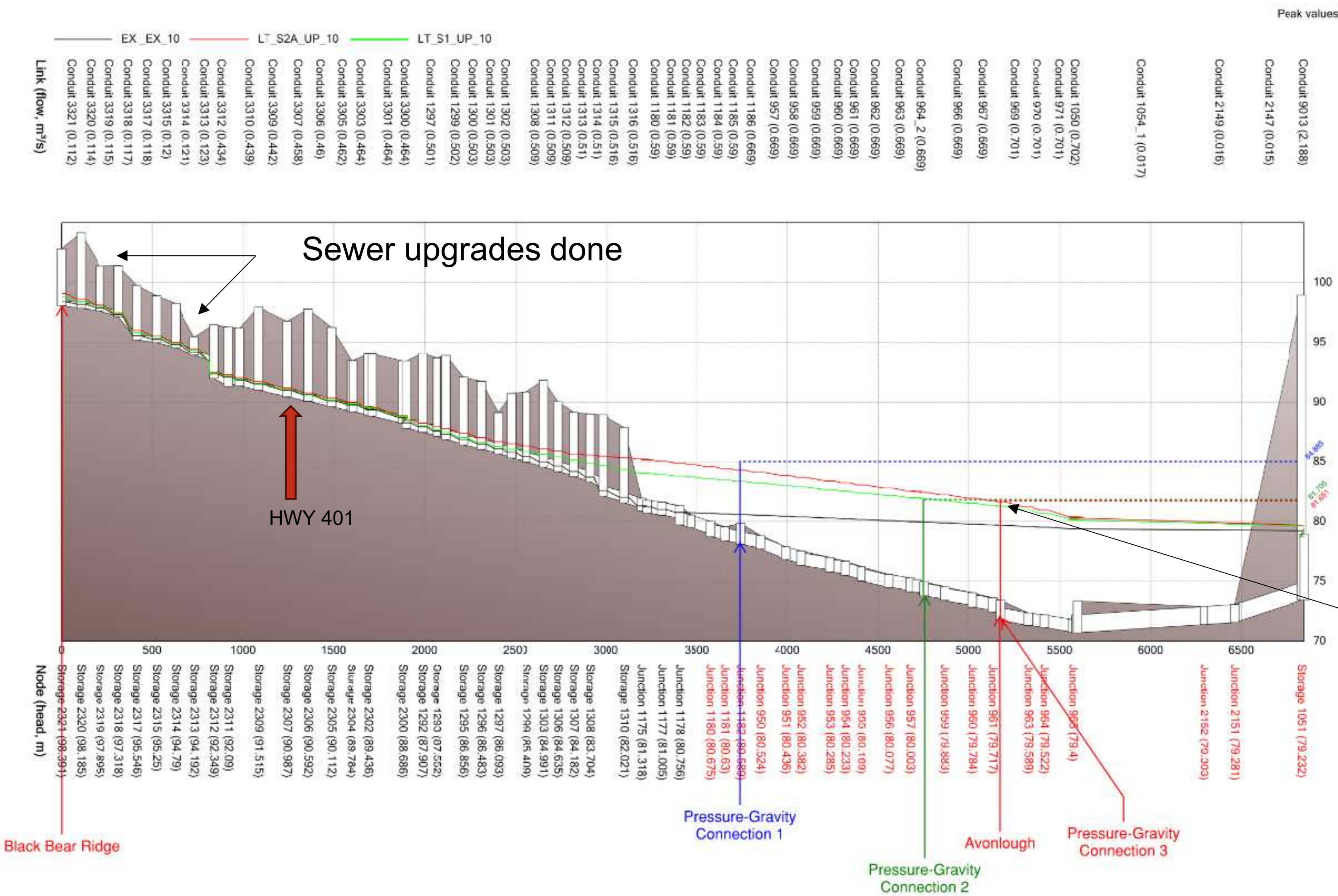
Scenario 2A: Future Growth with Black Bear Ridge Connection at most Northern Point of Trunk Sewer
1:100-Year Storm



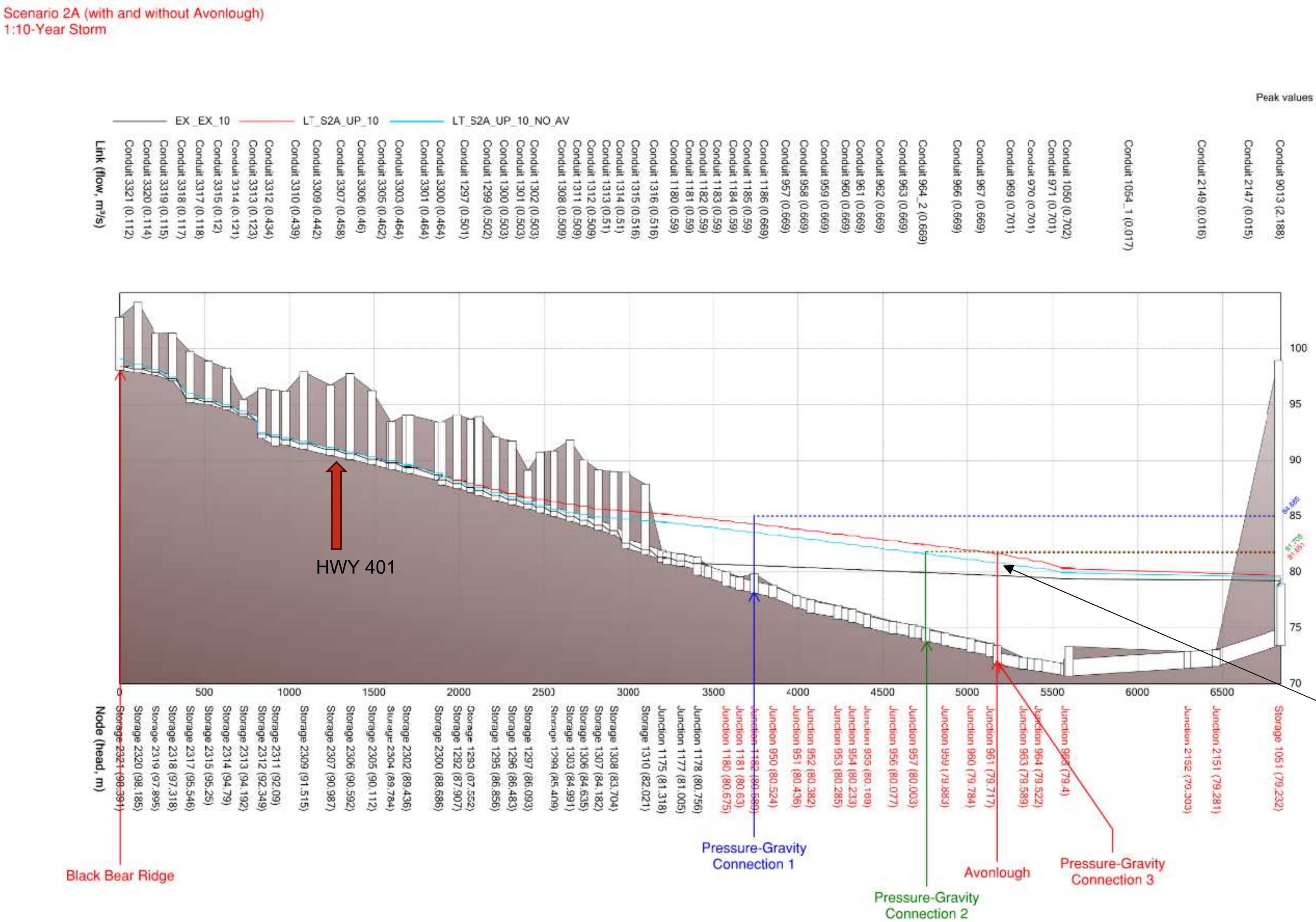


- Modelling runs were completed for BBR connection at Black Diamond Rd. and showed similar impacts to downstream sewers.
- This option is not recommended as it does not offer benefit to reduced sewer upgrades.

Scenario 2A vs. Scenario 1 (with vs. without Black Bear Ridge)
1:10-Year Storm



Avonlough flow should bypass pressure sewer

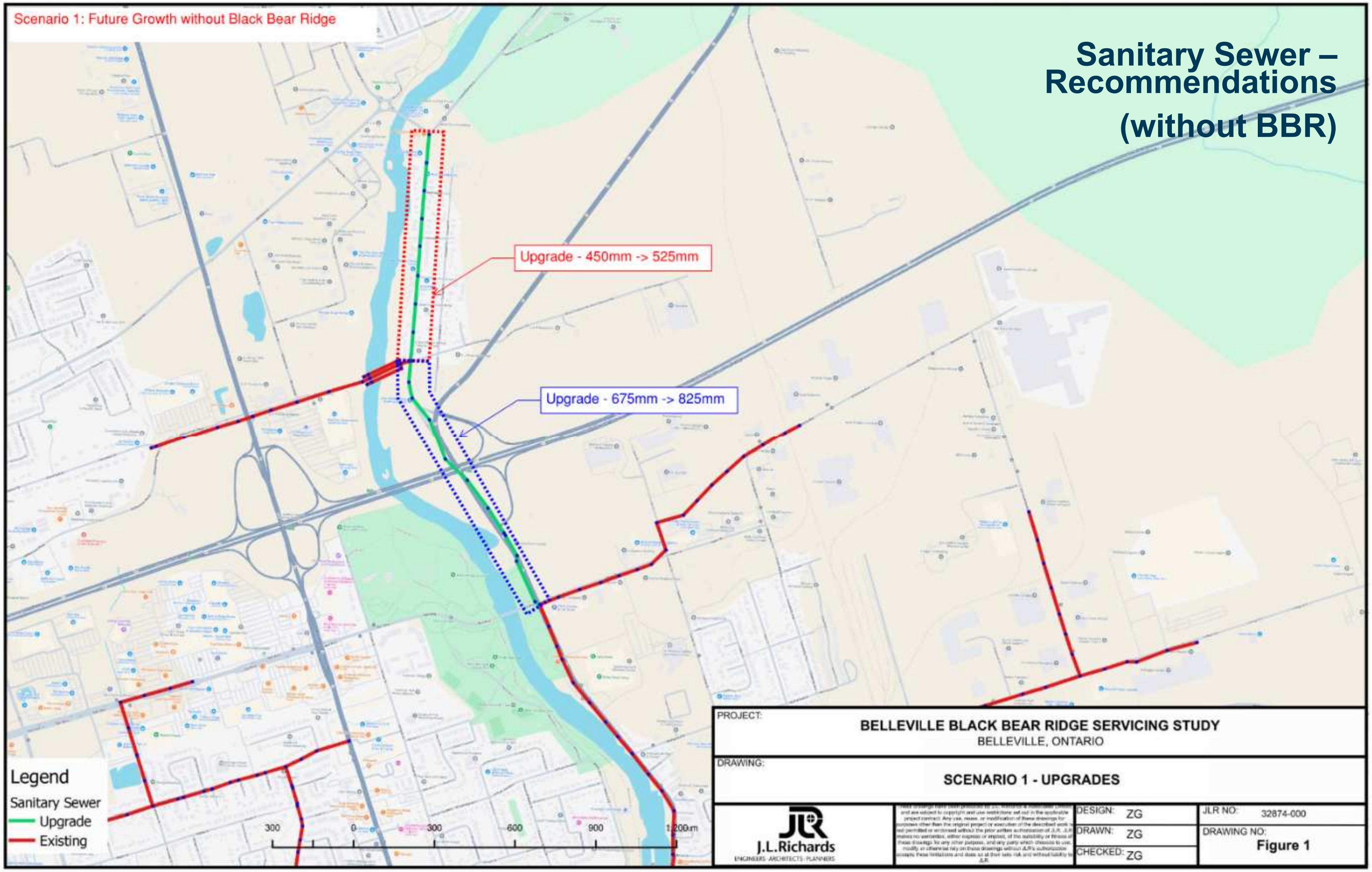


No issue upstream and downstream of Connection 3 once Avonlough is re-directed (HGL below spill elevation)

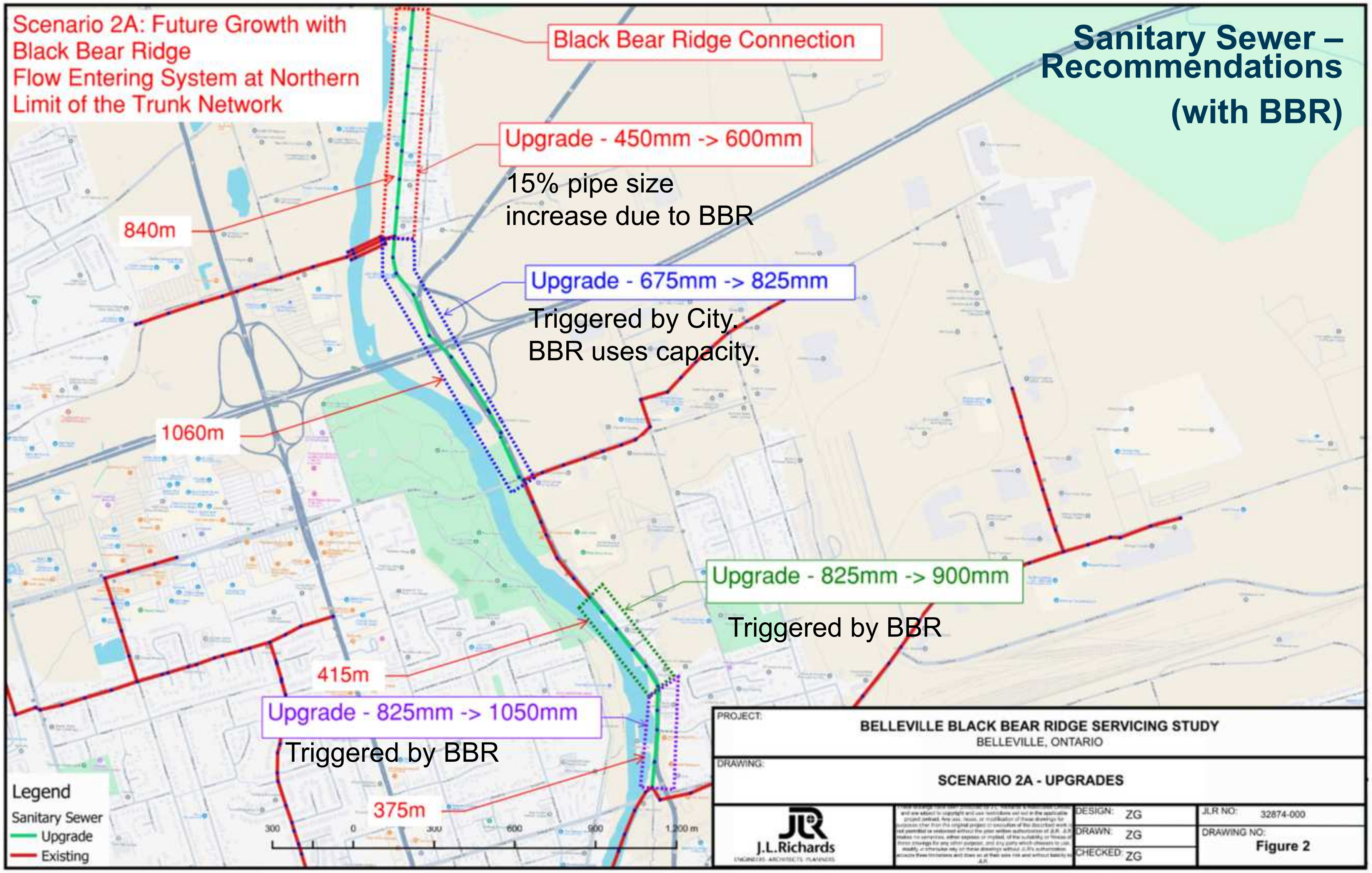
Wastewater Modelling Results

- Under mid- and long-term scenarios, sanitary flow from Avonlough SPS must bypass the pressure sewer (with or without BBR).
- Regardless of where BBR enters the system, the increased flow increases the extents of the upgrades required.

Sanitary Sewer – Recommendations (without BBR)

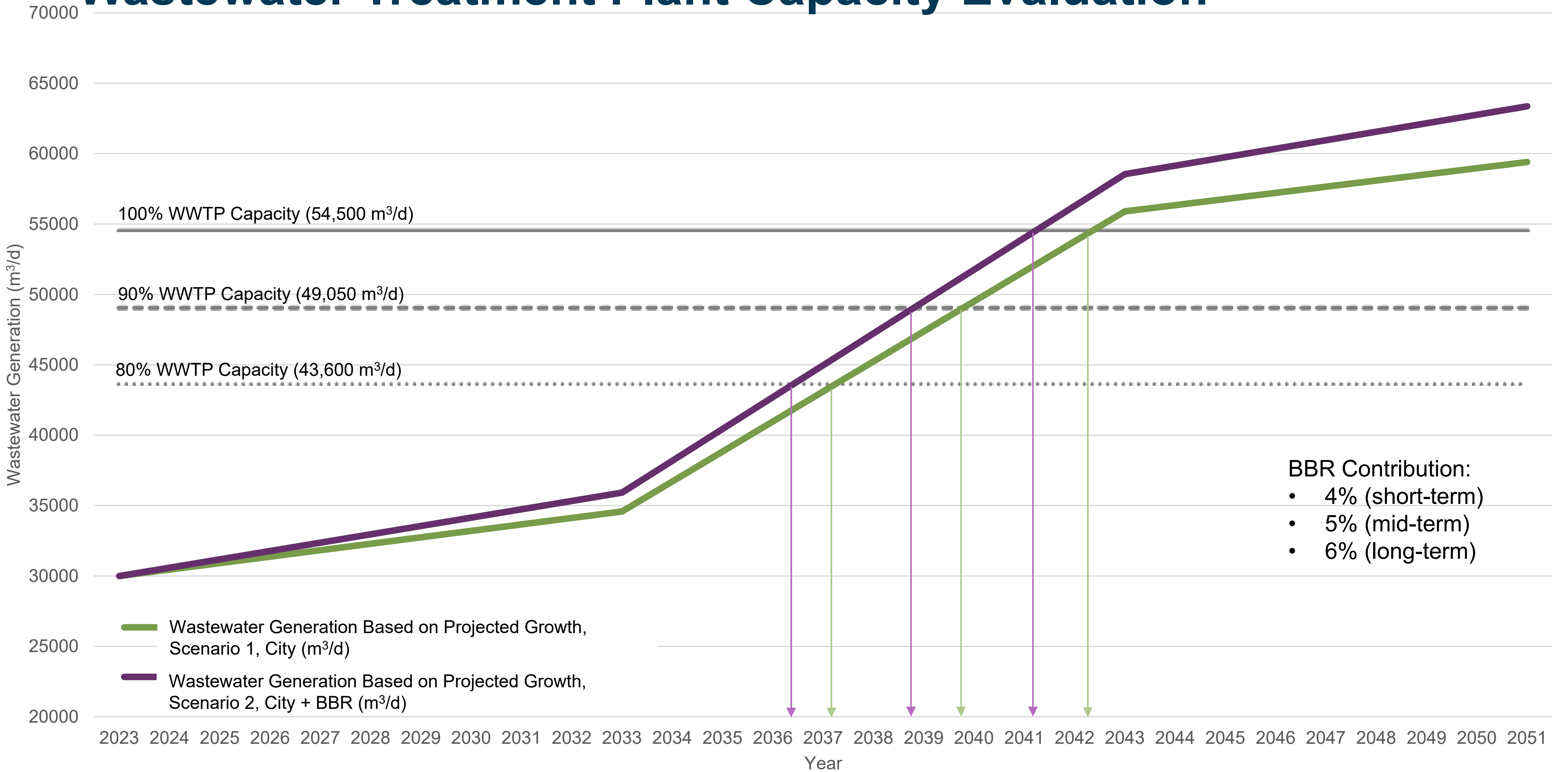


Sanitary Sewer – Recommendations (with BBR)



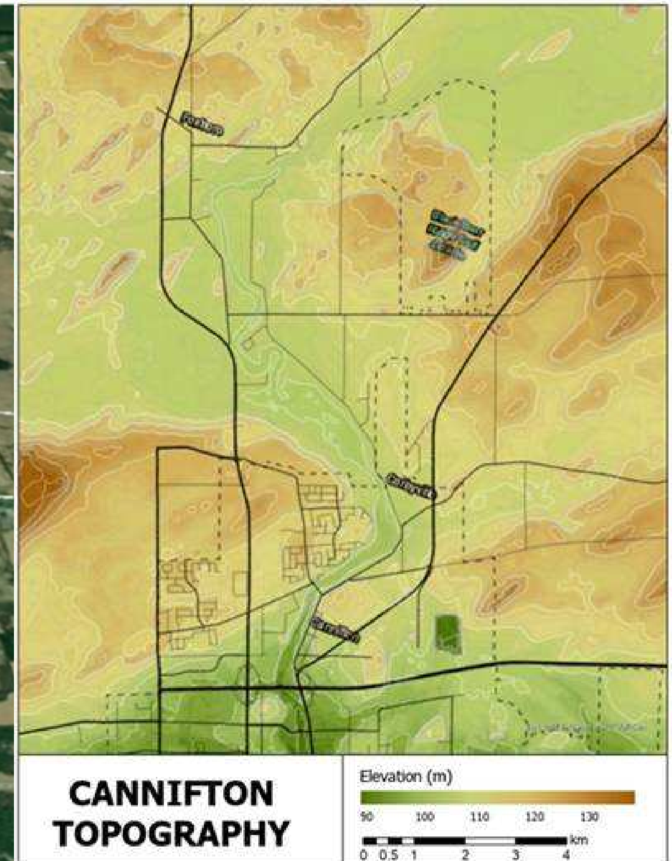
Wastewater Treatment Plant

Wastewater Treatment Plant Capacity Evaluation

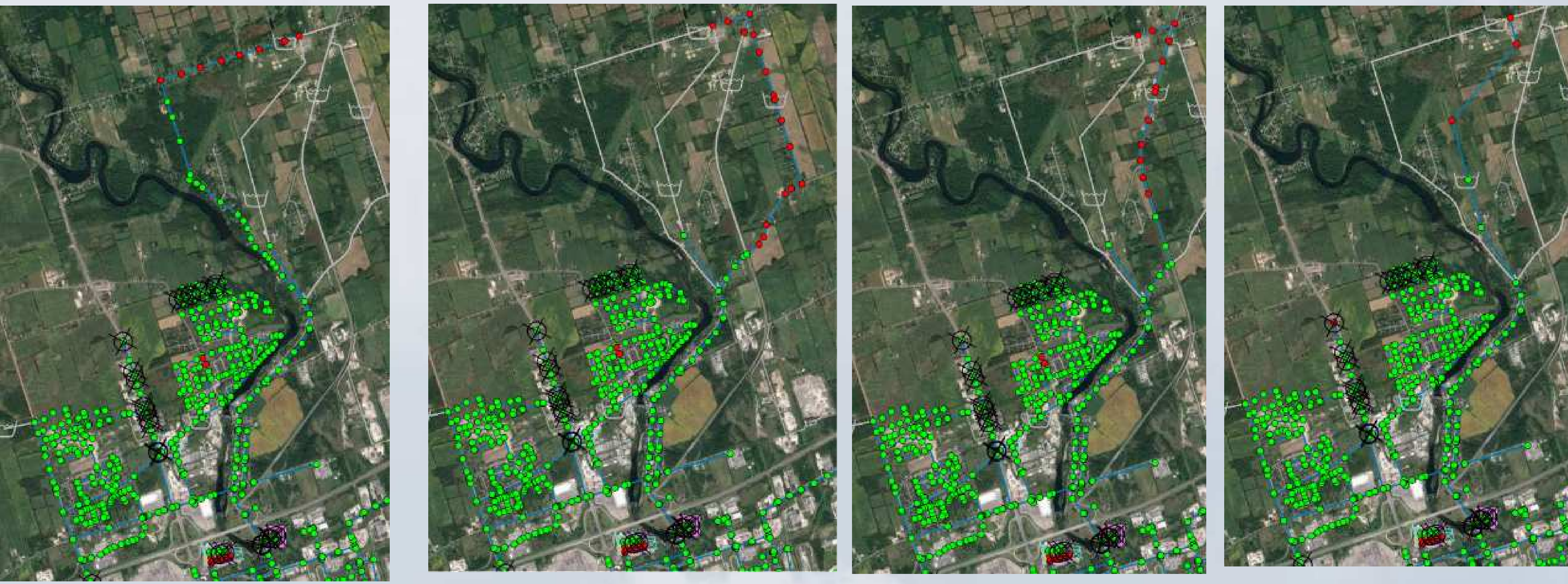


Evaluation – Routing Options

Updated Routing Options



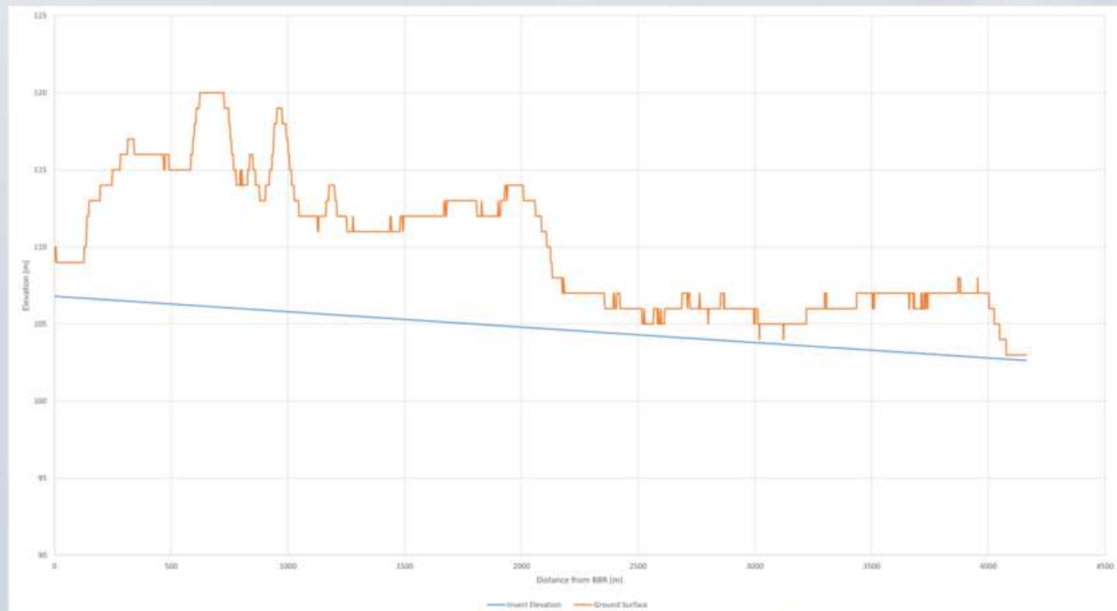
Routing Options – Water Model Results



- Transition between green and red indicates pressure dropping below 20psi and triggers boosting.

Sanitary Sewer – Upper Connection

- The figure represents the topography along routing Option 4 from BBR to Corbyville. Blue line represents the profile of a gravity connection.
- Routing Options 1 and 4 show feasibility for a gravity sewer from BBR to Corbyville. A 600 mm sewer would be required at a minimum slope of 0.1%.
- A sanitary pump station can be constructed in Corbyville that conveys wastewater from BBR and Corbyville. The forcemain will tie into the north-end of the City trunk sewer along Cannifton Rd N.



Evaluation Criteria

Criteria	Option 1 - Plumpton Road	Option 2 - Ritz Road	Option 3 - Hwy 37	Option 4 - Corbyville
Technical Considerations	• Least intermediate elevation changes. • Potential gravity option to Corbyville • Shorter distance (3.8km)	• Most intermediate elevation changes • No gravity option to Corbyville • Medium distance (4.2km)	• Moderate intermediate elevation changes • No gravity option to Corbyville • Longest Distance (4.5km)	• Least intermediate elevation changes. • Potential gravity option to Corbyville. • Shortest distance (3.6km).
Future Servicing Considerations	• Central location to service Corbyville and BBR. • Closer potential future connection to Foxboro. • Zone 3 Booster Station can be located in Corbyville development area.	• Additional watermain routing required to service Corbyville • Further future connection to Foxboro. • Zone 3 Booster Station cannot be located in Urban Boundary or known developments.	• Additional watermain routing required to service Corbyville. • Further future connection to Foxboro. • Zone 3 Booster Station cannot be located in Urban Boundary or known developments.	• Central location to service Corbyville and BBR. • Further future connection to Foxboro. • Zone 3 Booster Station can be located in Corbyville development area.
Access Considerations	• Proposed works are within the local road allowance	• Proposed works are within the local road allowance	• Proposed works are within local road allowance and Provincial road allowance.	• Proposed works are not within an existing road allowance.
Environmental Impact and Risk	• Least amount of alignment adjacent to environmentally sensitive areas.	• Moderate amount of alignment adjacent to environmentally sensitive areas.	• Moderate amount of alignment adjacent to environmentally sensitive areas.	• Most amount of alignment adjacent to environmentally sensitive areas.

existing, potential future

Evaluation Criteria

Criteria	Option 1 - Plumpton Road	Option 2 - Ritz Road	Option 3 - Hwy 37	Option 4 – Corbyville
Cost Sharing Considerations	Yes	No	No	Yes
Capital Cost	$$$ • Shorter option (3.8km)	$$$ • Longer option (4.2km). • Additional watermain routing to service Corbyville.	$$$$ • Longest option (4.5km). • Additional watermain routing to service Corbyville.	$$$ • Shortest option (3.6km) • Limited construction access.
Operation and Maintenance Cost	$$ • Shorter option (3.8km)	$$$ • Longer option (4.2km)	$$$ • Longest option (4.5km)	$$$ • Shortest option (3.6km) • Maintenance of unopened road allowance
Final Evaluation	**Preferred**	**Less Preferred**	**Least Preferred**	**Less Preferred**

Recommendations

OPC Table has been updated and provided in the Phase 2: Servicing Study Report. The numbers provided herein are not final.

provide detailed calc on the split

remove Harmony School and community centre demand from BBR's share

Short-Term Capital Projects

Option 1

Project #	Short-Term	Project Description	OPC (+/-50%)	City and Other's Share	BBR's Share
1	Storage (Zone 1)	New floating storage in Zone 1 (4.2ML), including EA, engineering and construction	$ 11,000,000	$ 8,590,000	$ 2,410,000
2	Storage (Zone 2)	New floating storage in Zone 2 (4ML), including EA, engineering and construction	$ 10,000,000	$ 8,840,000	$ 1,160,000
3	Storage (Zone 3)	New floating storage in Zone 3 (4.5ML)	$ 12,000,000	$ -	$ 12,000,000
4	Booster Pumping (Zone 2)	Adam St. Booster Pump Station Pump Modification, including engineering and construction	$ 2,500,000	$ 1,960,000	$ 540,000
5	Booster Pumping (Zone 3)	Zone 3 Booster Station, including EA, engineering and construction	$ 2,400,000	$ -	$ 2,400,000
6	Sanitary Collection	New gravity sewer along Routing Option 4 connecting BBR to Corbyville (2.8 km of 600mm diameter sewer)	$ 12,600,000	$ -	$ 12,600,000
7	Sewage Pump Station	New sewage pump station in Corbyville (150 L/s) and new forcemain (200 mm) connecting Corbyville to northern trunk sewer along Cannifton Rd.N	$ 10,050,000	$ 1,570,000	$ 8,480,000
8	Water Distribution	New watermain along Routing Option 4 connecting BBR and Cannifton Rd N. (3.8 km of 400mm dia watermain) *Assumed in common trench as sanitary and is a price adder	$ 4,560,000	$ 710,000	$ 3,850,000
		TOTAL (SHORT-TERM)	$ 65,110,000	$ 21,670,000	$ 43,440,000

Mid-Term Capital Projects

Project #	Mid-Term	Project Description	OPC (+/-50%)	City and Other's Share	BBR's Share
9	Storage (Zone 2)	New in-ground storage in Zone 2 (10 ML), including EA, engineering and construction *assume at Adam St. Booster Pump Station	$ 32,000,000	$ 30,580,000	$ 1,420,000
10	Sanitary Collection	Northern Trunk Sewer Upgrades along Cannifton Rd. N including HWY401 Crossing, including engineering and construction (840m of 600mm dia sewer upgrade, 1060m of 825mm dia sewer upgrade, directional drilling for new HWY401 crossing at 825 mm)	$ 15,222,000	$ 12,940,000	$ 2,290,000
11	Water Distribution	Watermain Upgrades along Cannifton Rd. N (2km of 400mm dia watermain upgrade) *Assumed in common trench as sanitary and is a price adder	$ 2,400,000	$ -	$ 2,400,000
12	Sanitary Collection	Southern Trunk Sewer Upgrades south of HWY401, including engineering and construction (415m of 900mm dia sewer upgrade, 375m of 1050mm dia sewer upgrade)	$ 4,480,000	$ -	$ 4,480,000
13	Sewage Pump Station	Increase Corbyville Sewage Pump Station Capacity	$ 1,000,000	$ 160,000	$ 840,000
14	Wastewater Treatment Plant	Expand Belleville WWTP to 64,000 m3/d ADF, including EA, design and construction	$ 44,620,000	$ 41,940,000	$ 2,680,000
		TOTAL (MID-TERM)	$ 99,722,000	$ 85,620,000	$ 14,110,000

compare to Scott St. river crossing

Long-Term Capital Projects

Project #	Long-Term	Project Description	OPC (+/-50%)	City and Other's Share	BBR's Share
15	Water Treatment Plant	Expand Belleville WTP to 77,000 m3/d MDD, including EA, design and construction	$ 5,000,000	$ 4,650,000	$ 350,000
16	Storage (Zone 1)	New at-grade storage and booster pump station in in Zone 1 (2 ML), including EA, engineering and construction	$ 7,000,000	$ 5,380,000	$ 1,620,000
		TOTAL (LONG-TERM)	$ 12,000,000	$ 10,030,000	$ 1,970,000

	GRAND TOTAL (CITY BUILD-OUT)	$ 176,832,000	$ 117,320,000	$ 59,520,000

Next steps

- City should undertake a Schedule ‘B’ Class EA on treated water storage and water distribution system in Avonlough / Loyalist Secondary Plan area in Zone 1.
- City should undertake a Schedule ‘B’ Class EA to select the location of the Zone 2 floating storage and confirm Adam St. Booster Pump Station pumping requirements.
- BBR should undertake a Schedule ‘B’ Class EA for Zone 3 booster pump station and storage.
- City/BBR should investigate land acquisition requirements for Zone 3 booster station, potential Corbyville sewage pump station locations.
- City should consider directing flow from Avonlough Sewage Pump Station to Belleville WWTP, instead of the pressure sewer.
- City should consider an update to the Wet Weather/Wastewater Master Plan to incorporate BBR contributions.