

June 28, 2023

Project Number: 2468-23

Acadia Engineering
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Belleville, Ontario
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Attention: Steve Harvey, P.Eng

Subject: Hogan Properties, Belleville– Preliminary SWM Facility Sizing

INTRODUCTION

J.F. Sabourin and Associates Inc. (JFSA) has been commissioned by Acadia Engineering to complete preliminary Storm Water Management (SWM) facility sizing for the proposed development referred to as Hogan Properties. The site is located on the northern outskirts of the town of Belleville, Ontario and is just west of the intersection of Farnham Road and Scott Drive. The proposed development site is approximately **4.71 ha** and will consist primarily of single family homes. **Figure 1** provides an overview of the proposed development limits and their respective location. The following memo outlines the preliminary SWM facility sizing requirements for this site to ensure that the future development does not have any adverse impacts on existing developments, infrastructure, or flood-prone areas.

Figure 1: Site Overview



BACKGROUND DATA

The following outlines the data used to support this analysis:

- LiDAR data at 1.0 m x 1.0 m resolution
- Conceptual development plan – provided by Acadia.
- Ontario Soils Mapping Data - Land Information Ontario (LIO)
- Southern Ontario Land Resource Information System (SOLRIS) 3.0 - LIO

DESIGN STORMS

The 3-hour Chicago and 24-hour SCS type II distribution artificial rainfall events have been used as design standards to ensure that infrastructure, such as drainage systems and stormwater management structures, can adequately handle anticipated rainfall events and prevent flooding or other water-related issues. The IDF curves from the Belleville (6150689) Environment and Climate Change Canada (ECCC) gauge has been used for this analysis. This gauge has been intermittently operational since 1960 – 2016 and provides 44 years of historical rainfall data. Design storms were produced using the IDF data from the Belleville gauge and processed using STORMS 2010 (Software developed by JFSA) to convert this IDF data into full rainfall hyetographs. **Table 1** below outlines the total rainfall volumes for the various return periods and design storms. These rainfall hyetographs have been applied to both the pre- and post-development models. Copies of the Belleville IDF data and the hyetographs applied in the model have been provided in **Attachment A** of this report.

Table 1: Belleville Total Rainfall Depths (mm) for 3-Hour CHI and 12-Hour SCS Type II Storms

Return Period	2-Year	5-Year	10 Year	25-Year	50-Year	100-Year
CHI 3 Hour	31	40	46	53	59	65
SCS 24 Hour	51	65	74	86	95	104

PRE-DEVELOPMENT

Drainage Area

The total drainage area for this location is **5.89 ha** with the future development lands occupying approximately **4.71 ha** of the total drainage area. There is a drainage divide that runs through the centre of the site, resulting in the north half of the drainage area (**2.56 ha**) draining northeast to an existing ditch network located along Farnham Road, passing under Farnham Road through a culvert running west to east and outletting to the Moira River. The south half (**2.14 ha**) will drain southeast through a residential lot and into the existing ditch system on Farnham Road, and then run south along Farnham Road before reaching the Moira River. There are also two external drainage areas located to the west of the site, with **0.1 ha** draining north of the divide into the site, and **1.09 ha** draining south into the development area. The entire **5.89 ha**, despite initially draining to separate subcatchments, ultimately discharges to the Moira River and then into the Bay of Quinte. Refer to **Figure A1** in **Attachment A**, for the pre-development drainage divide.

Land Use

Under pre-development conditions, the site is undeveloped and consists primarily of farmlands with small areas of trees and roadways. **Figure A2** in **Attachment A** provides a visual overview of the respective land use data for each of the subcatchments within the study area.

Soil/Infiltration Data

Soil data from Land Information Ontario indicated that the soils are predominantly **clay loam** soils, which are considered a **Type C** SCS soil group. **Figure A3** in **Attachment A** provides a visual overview of the soil type data for each of the subcatchments within the study area.

Curve Number (CN)

Curve Numbers (CN) were calculated, based on underlying Land Use Type and Soil Classification at each location within the subcatchments based on values outlined in **Tables A2** and **A3** in the SWMHYMO Manual. Each Curve Number was then weighted based on the total area within a given subcatchment to determine the weighted CN for that subcatchment. **Table A1** in **Attachment A** provides a full summary of the CN calculations for each of the pre-development subcatchments.

Time to Peak (t_p)

For natural areas within the study area, the time-to-peak values for each of the subcatchments have been calculated based on existing topography. Flow paths have been discretized based on the topographic data using GIS tools and the longest major flow path within each subcatchment identified; refer to **Figure A4** in **Attachment A** for the flow paths discretized for each subcatchment. The upstream and downstream topographic elevations and flow lengths were identified for each subcatchment and used in the calculations. For these natural subcatchments, the Federal Aviation Administration (FFA) method was determined to be the most appropriate method to calculate the Time to Peak. Full details of these calculations have been provided in **Table A2** in **Attachment A**, along with other time-to-peak values using alternative t_p calculation methods.

Initial Abstraction

For undeveloped lands, an initial abstraction value of **4.67 mm** has been assumed which is typical for undeveloped lands commonly used throughout Ontario (parameters are in line with typical rates applied in Ontario per Ministry of Environment Stormwater Management Planning and Design Manual and the City of Ottawa Storm Sewer Design Guidelines). Full SWMHYMO modelling input and summary files for pre-development conditions have been provided in **Attachment A**.

Results

Table 2 below presents the peak flows from the various development area under pre-development conditions:

Table 2: Pre-Development Peak Flows (m^3/s)

DESIGN STORM	Ext-FarnS (1.09 ha)	Ext-FarnN (0.1 ha)	Dev-FarnS (2.14 ha)	Dev-FarnN (2.56 ha)
25mmCHI4Hr	0.010	0.001	0.014	0.016
2YRCHI3Hr	0.016	0.002	0.022	0.026
5YRCHI3HR	0.027	0.004	0.037	0.043
10YRCHI3HR	0.036	0.005	0.049	0.057
25YRCHI3HR	0.047	0.006	0.064	0.074
50YRCHI3HR	0.056	0.008	0.077	0.089
100YRCHI3HR	0.066	0.009	0.091	0.104
2YRSCS24HR	0.033	0.005	0.043	0.049
5YRSCS24HR	0.050	0.007	0.068	0.077
10YRSCS24HR	0.063	0.009	0.086	0.097
25YRSCS24HR	0.080	0.011	0.110	0.123
50YRSCS24HR	0.093	0.013	0.129	0.144
100YRSCS24HR	0.107	0.015	0.148	0.165

POST-DEVELOPMENT

Drainage Area

The post-development model has been developed to reflect the proposed draft plan development grades and respective SWM outlet locations. The proposed development draft plan and the associated drainage areas have been provided in **Figure B1 of Attachment B**. Under post-development conditions, the entirety of the **4.71 ha** site will drain east and northeast to a SWM facility which will attenuate peak flows to pre-development rates. Note that as the entire development will be draining to the north outlet the post-development flows for the site have been set to match the pre-development peak flows to the north (Catchment Dev-FarnN), as outlined in **Table 2** above.

Under post-development conditions, it is assumed that runoff from the two external areas (Ext-FarnS and Ext-FarnN) will be conveyed around the subdivision to the south. As the **2.14 ha** of drainage area from area Dev-FarnS will go to the SWM pond within the subdivision, the addition of Ext-FarnN (**0.1 ha**) draining south does not have any adverse impacts on peak flows to the southern portion of the Farnham Roadside ditch.

Land Use/ Imperviousness

Under post-development conditions, it was assumed that the site would have an average imperviousness of **67%**, which is typical for a residential subdivision of this type. Note that for this study it is assumed that **57%** of all impervious areas will be directly connected to the storm sewer infrastructure, which is a conservative assumption.

Soil/Infiltration Data

To represent the proposed developed land infiltration rates, Horton's infiltration has been used. For these lands, the following Horton's Infiltration parameters have been applied: $F_0=76.2$ mm/hr, $F_c=13.2$ mm/hr, $DCAY=4.14$ /hr, $F=0$ mm. These Horton infiltration rates are typical for urban grassed areas and are commonly used throughout Ontario (infiltration parameters are in line with typical rates per City of Ottawa Storm Sewer Design Guidelines)

Time to Peak (t_p)

Under post-development conditions, the flow lengths of the subcatchments have been represented through LGI (Flow Length Impervious) and LGP (Flow Length Pervious) parameters. LGP has been set at 40 m for all subcatchments, which is reflective of the average typical rear yard lot length. LGI has been calculated as follows, as per the SWMHYMO manual:

$$LGI = \sqrt{\frac{Area (m^2)}{1.5}},$$

Initial Abstraction

For pervious and impervious surfaces an initial abstraction value of **4.67 mm** and **1.57 mm** respectively has been assumed which is typical for natural and developed lands commonly used throughout Ontario (parameters are in line with typical rates per City of Ottawa Storm Sewer Design Guidelines).

SWM Facility

The SWM facility within the development has been iteratively sized to ensure that the post-development runoff from the site will be attenuated in the facility to the rates under predevelopment. The SWM facility has been conceptually sized using a ROUTE RESERVOIR command in SWMHYMO, which represents the facility simply as an outflow/storage curve. A detailed stage storage/curve of the pond has been provided by Acadia and included in **Table B1 in Attachment B**. To produce an outflow/storage curve to place in the model the pond outlet configuration has been iteratively designed using various orifice and weir equations, see **Table B5 in Attachment B** for the outlet structure calculations.

Sediment Forebay

The proposed facility has been equipped with a sediment forebay to improve pollutant removal by allowing the larger particles to settle out before entering the main cell of the pond. The forebay enters the pond from the west before spilling into the main cell.

The forebay has been provided with a permanent pool depth of 1.45 m to minimize the potential for re-suspension. Per the MOE design criteria, the forebay has been graded at a 3H:1V slope, and the forebay berm has been set at the permanent pool elevation. The forebay berm will separate the forebay from the rest of the facility to reduce the transfer of sediment to the main cell of the pond. The forebay is sized to meet the greater of the settling and dispersion criteria, as stated in the SWMP Design Manual. Calculations for the minimum dispersion length, settling length and average velocity have been included in **Calculation Sheet B-1 of Appendix B**.

Permanent Pool

The pond should have a permanent pool depth between 1.0 and 3.0 m, as stipulated in the SWMP Design Manual. Therefore, the proposed facility has been designed with a permanent pool depth of **1.45 m** at an elevation of **110.70 m**. The permanent pool has been sized based on enhanced protection per Table 3.2 (enhanced protection level for a wet pond) in the SWMP Design Manual. Based on a **4.71 ha** drainage area with an average imperviousness of **67%** (refer to **Tables B2 & B3 of Appendix B**), a minimum of **218 m³/ha** must be provided. The required permanent pool storage volume is calculated as follows:

$$(218 - 40) \text{ m}^3/\text{ha} \times 4.71 \text{ ha} = 838 \text{ m}^3$$

The proposed pond has been designed with a permanent pool volume of **915 m³**, which is more than the minimum permanent pool volume the SWMP Design Manual requires.

Quality Control

The quality control volume is based on a volume of 40 m³/ha. The required quality control volume is calculated as follows:

$$40 \text{ m}^3/\text{ha} \times 4.71 \text{ ha} = 188 \text{ m}^3$$

The proposed facility provides **599 m³** of extended detention volume at an elevation of **111.25 m**, with a maximum extended detention storage depth of **0.55 m** above the permanent pool elevation of **110.70 m**. Refer to **Table B4 of Appendix B**. The quality control orifice is **110 mm** in diameter and is set at **117.0 m**. The quality control orifice is in the outlet structure at the west end of the pond.

Quantity Control

Quantity control will be provided by one **160 mm** diameter vertical circular orifice, and one **240 mm** diameter vertical circular orifice, set at inverts of **111.25 m** and **111.75 m**, respectively. The orifices will be in the outlet structure at the west end of the pond. The top of the outlet structure will be set above the 100-year pond level. Calculations in support of the quantity control orifice are provided in **Table B5 of Appendix B**. The proposed SWM pond will outlet to the existing roadside ditch on Farnham Road.

Conveyance of Emergency Overflows

In the event of a blockage or a storm greater than the 100-year event, a **20 m**-wide emergency overflow weir has been provided for the pond. Its crest elevation has been set at an elevation of **112.20 m**, which is above the maximum 100-year pond level under free outlet conditions, and provides 0.3 m of freeboard to the top of the pond at **112.50 m**.

SWM Pond Operation

As mentioned above the SWM facility will be designed to ensure peak flows to the existing storm sewer network do not exceed pre-development conditions. **Table 3** below outlines the pre-and post-development flows and the associated required SWM facility storage volumes and associated water levels in the pond to ensure that the proposed development meets these rates. Full SWMHYMO modelling input and summary files for post-development conditions have been provided in **Attachment B**.

From **Table 3** below it is seen that the development will need approximately **2,140 m³** of active storage to attenuate post-development flows to less than or equal to **955 L/s** for up to and including the 100-year event. It is also important to note that the proposed development will result in peak flows to the storm sewer decreasing for events larger than the 5-year for the 12-hour SCS storm and increasing for all events for the 3-hour Chicago storms. For both 100-year events, the peak outflow is less than the capacity of the pipe ensuring that the proposed development will not have any adverse impacts on existing developments, infrastructure, or flood-prone areas.

Table 3: SWM Facility Sizing

DESIGN STORM	Pre Dev (2.562 ha) Peak Flows (m ³ /s)	Post Dev (4.71 ha) Peak Flow (m ³ /s)	Peak Flow Difference (m ³ /s)	Required storage volume (m ³)	Pond Elevation (m)	Active Storage Depth (m)
Quality Control*	-	0.002	-	188	110.87	0.17
25mmCHI4Hr	0.016	0.016	0.000	566	111.17	0.47
2YRCHI3Hr	0.026	0.023	-0.003	729	111.29	0.59
5YRCHI3HR	0.043	0.042	-0.001	980	111.47	0.77
10YRCHI3HR	0.057	0.052	-0.005	1,169	111.59	0.89
25YRCHI3HR	0.074	0.064	-0.010	1,399	111.73	1.03
50YRCHI3HR	0.089	0.083	-0.006	1,577	111.84	1.14
100YRCHI3HR	0.104	0.104	0.000	1,738	111.93	1.23
2YRSCS24HR	0.049	0.041	-0.008	971	111.46	0.76
5YRSCS24HR	0.077	0.057	-0.020	1,293	111.67	0.97
10YRSCS24HR	0.097	0.074	-0.023	1,513	111.80	1.10
25YRSCS24HR	0.123	0.108	-0.015	1,766	111.95	1.25
50YRSCS24HR	0.144	0.128	-0.016	1,951	112.05	1.35
100YRSCS24HR	0.165	0.146	-0.019	2,140	112.15	1.45

* Quality control volume Per MOE design guidelines

Conclusion

A preliminary SWM facility sizing has been completed for the proposed development site referred to as Hogan Properties, Belleville. The SWM facility has been sized to mitigate post-development flows to pre-development conditions. Based on this analysis it was found that the development will need approximately **2,140 m³** of active storage to attenuate post-development flows to less than or equal to pre-development conditions up to and including the 100-year event.

Yours truly,
J.F Sabourin and Associates Inc.



Jonathon Burnett, B. Eng, P.Eng
Water Resources Engineer



cc: J. F Sabourin, M.Eng, P.Eng
Director of Water Resources Projects

Figures

Figure 1: Site Overview

Tables

Table 1: Total Rainfall Depths (mm) for 3-Hour CHI and 12-Hour SCS Type II Storms

Table 2: Pre-Development Peak Flows (m³/s)

Table 3: SWM Facility Sizing

Attachments

Attachment A: Pre-Development

Attachment B: Post Development



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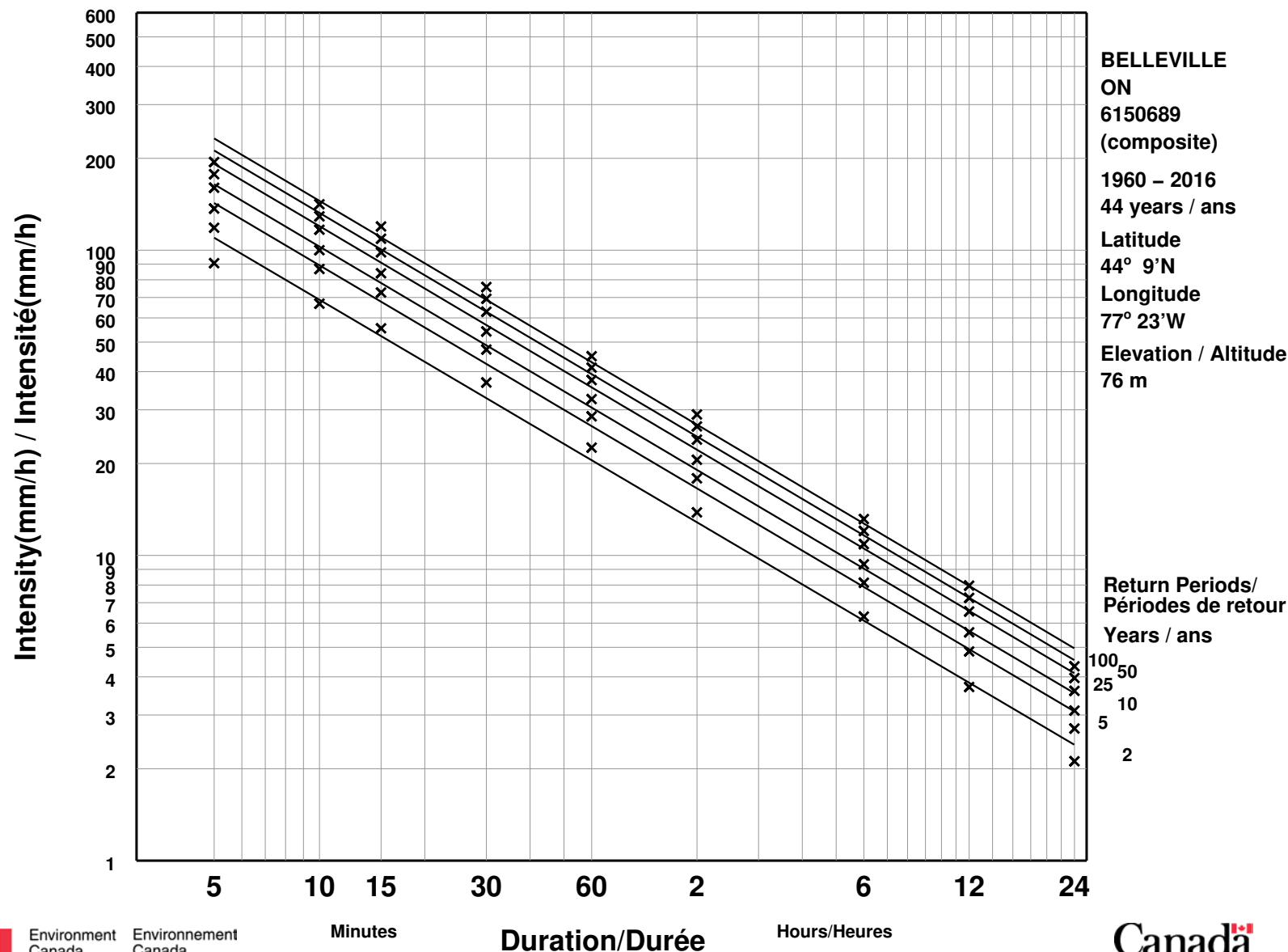
Attachment A

Pre-Development

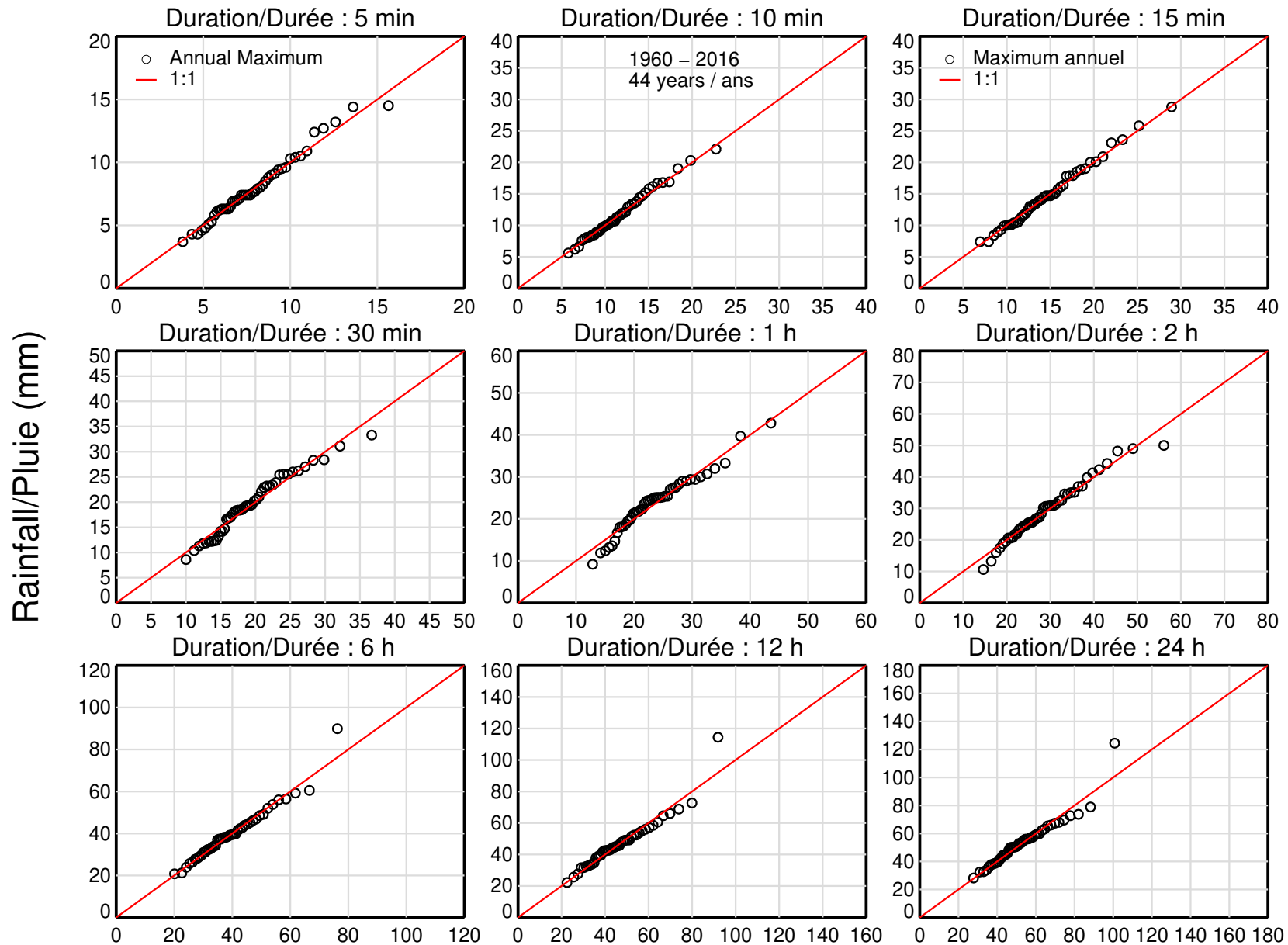
Short Duration Rainfall Intensity–Duration–Frequency Data

2022/10/31

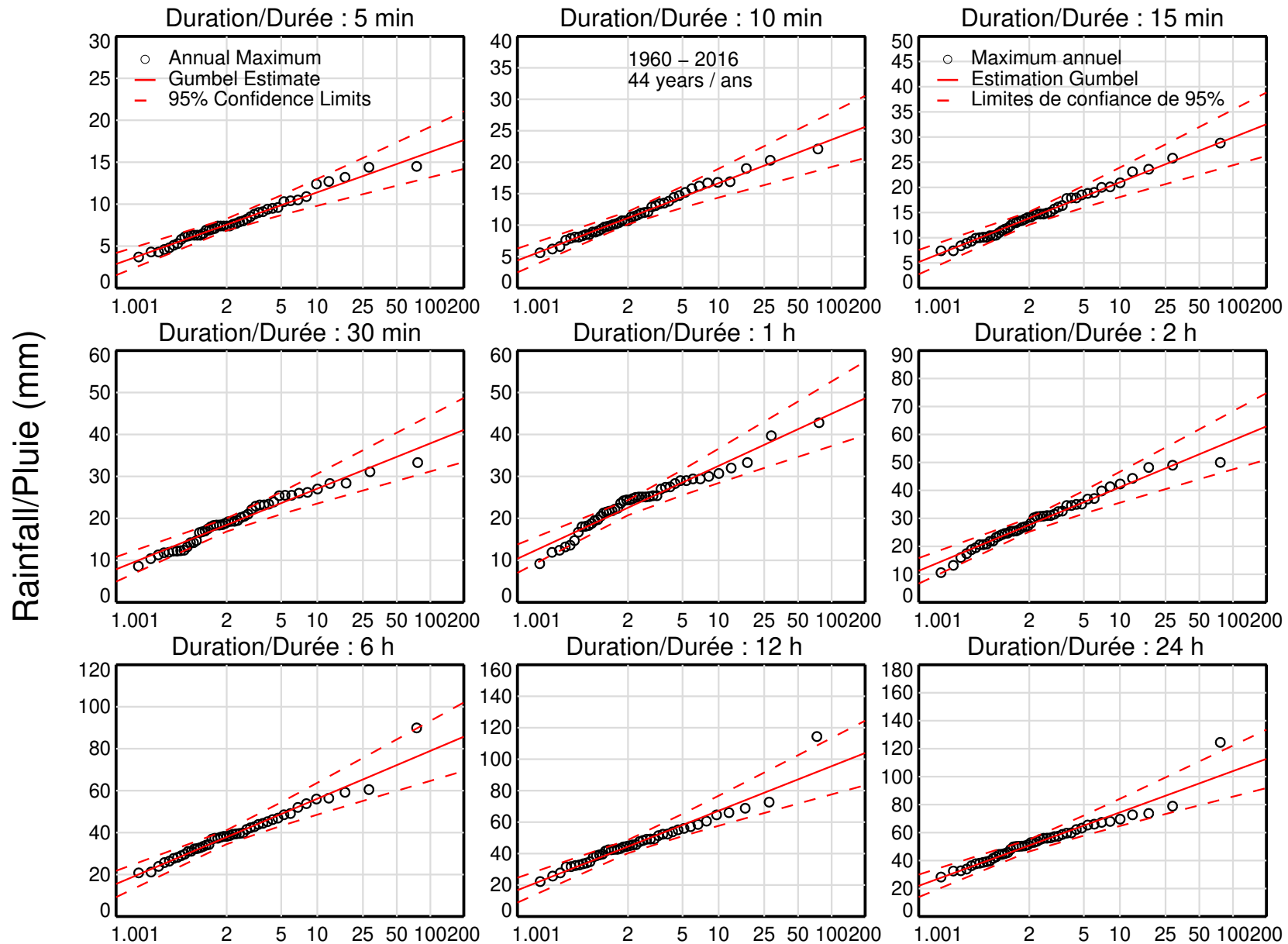
Données sur l'intensité, la durée et la fréquence des chutes de pluie de courte durée



Quantile-Quantile : BELLEVILLE, ON 6150689



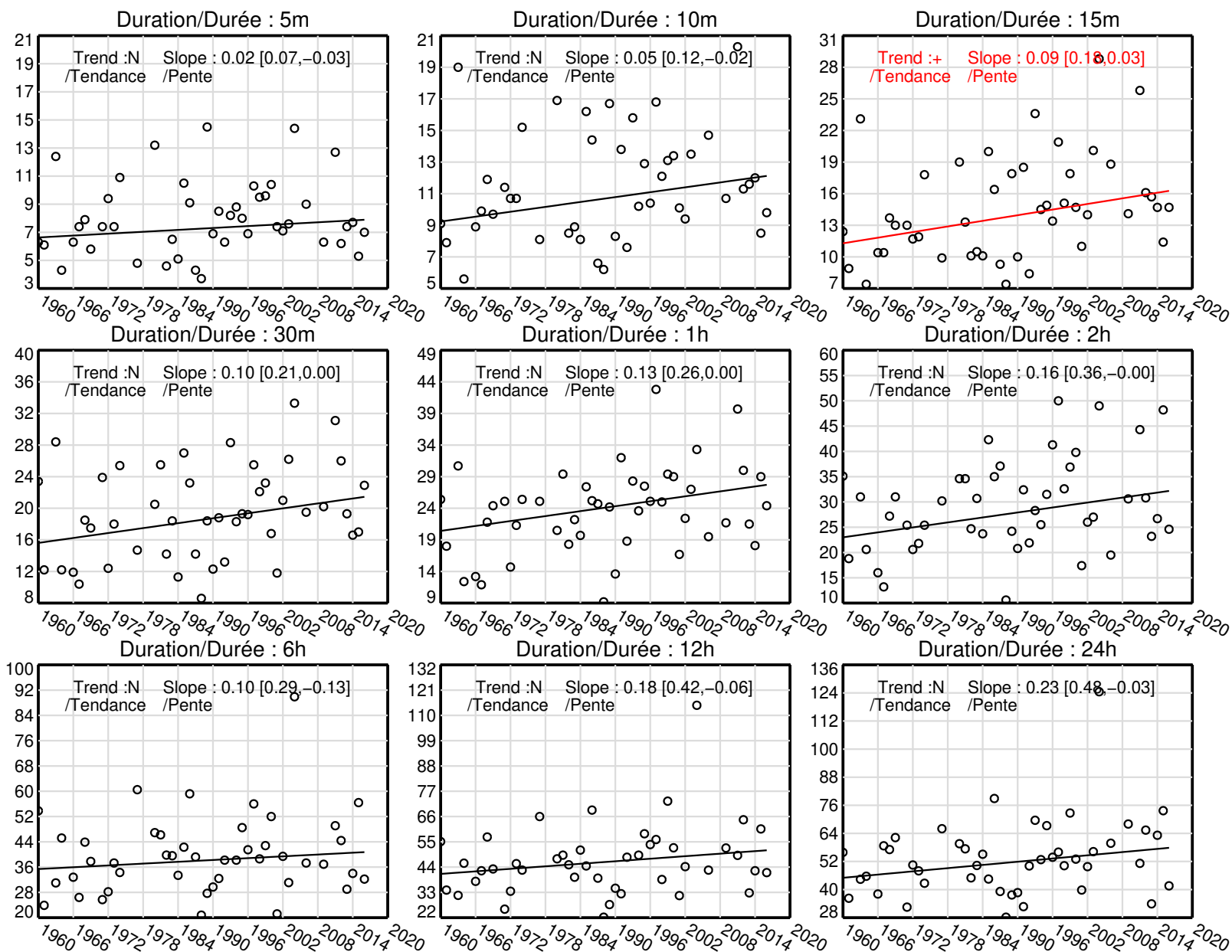
Return Level/Niveau de retour : BELLEVILLE, ON 6150689



Return Period/Période de retour (years/années)

Trend/Tendance : BELLEVILLE, ON 6150689

Annual Maximum/Maximum annuel (mm)



70	2011	12.7	20.3	25.8	31.1	39.7	44.3	49.1	49.1	51.2
71	2012	6.2	11.3	16.1	26.0	30.0	30.8	44.4	64.6	65.4
72	2013	7.4	11.6	15.7	19.3	21.5	23.2	29.0	32.8	33.9
73	2014	7.7	12.0	14.7	16.6	18.1	26.7	34.0	42.4	63.2
74	2015	5.3	8.5	11.4	17.0	29.0	48.2	56.4	60.6	73.7
75	2016	7.0	9.8	14.7	22.9	24.4	24.6	32.2	41.6	41.6
76										
77	# Yrs.	45	45	46	46	46	46	45	44	46
78	Années									
79	Mean	8.0	11.8	14.7	19.4	23.7	29.2	39.9	47.0	53.4
80	Moyenne									
81	Std. Dev.	2.6	3.8	4.9	5.9	6.8	9.2	12.5	15.5	16.1
82	Écart-type									
83	Skew.	0.80	0.78	0.86	0.26	0.30	0.43	1.54	1.96	1.88
84	Dissymétrie									
85	Kurtosis	3.48	3.43	3.72	2.61	3.95	3.11	7.71	10.31	10.23

*-99.9 Indicates Missing Data/Données manquantes

Warning: annual maximum amount greater than 100-yr return period amount
Avertissement : la quantité maximale annuelle excède la quantité
pour une période de retour de 100 ans

Year/Année	Duration/Durée	Data/Données	100-yr/ans
2004	6 h	89.9	78.9
2004	12 h	114.4	95.6
2004	24 h	124.5	104.0

Table 2a : Return Period Rainfall Amounts (mm)

Quantité de pluie (mm) par période de retour

Duration/Durée	2	5	10	25	50	100	#Years
	yr/ans	yr/ans	yr/ans	yr/ans	yr/ans	yr/ans	Années
5 min	7.6	9.9	11.4	13.3	14.8	16.2	45
10 min	11.1	14.5	16.7	19.5	21.5	23.6	45
15 min	13.9	18.2	21.0	24.6	27.3	29.9	46
30 min	18.4	23.6	27.1	31.4	34.7	37.9	46
1 h	22.6	28.5	32.5	37.5	41.3	45.0	46
2 h	27.7	35.8	41.1	47.9	52.9	57.9	46
6 h	37.8	48.8	56.1	65.3	72.2	78.9	45
12 h	44.5	58.1	67.2	78.6	87.1	95.6	44
24 h	50.8	65.0	74.5	86.4	95.2	104.0	46

Table 2b :

Return Period Rainfall Rates (mm/h) - 95% Confidence limits

Intensité de la pluie (mm/h) par période de retour - Limites de confiance de 95%

Duration/Durée	2	5	10	25	50	100	#Years
	yr/ans	yr/ans	yr/ans	yr/ans	yr/ans	yr/ans	Années
5 min	90.7	118.5	136.9	160.1	177.4	194.5	45
	+/- 8.4	+/- 14.2	+/- 19.2	+/- 25.9	+/- 31.0	+/- 36.1	45
10 min	66.8	86.8	100.0	116.7	129.1	141.4	45
	+/- 6.1	+/- 10.2	+/- 13.8	+/- 18.6	+/- 22.2	+/- 25.9	45
15 min	55.5	72.7	84.0	98.4	109.1	119.6	46
	+/- 5.2	+/- 8.7	+/- 11.7	+/- 15.8	+/- 18.9	+/- 22.0	46
30 min	36.9	47.3	54.2	62.9	69.3	75.8	46
	+/- 3.1	+/- 5.3	+/- 7.1	+/- 9.6	+/- 11.5	+/- 13.4	46
1 h	22.6	28.5	32.5	37.5	41.3	45.0	46
	+/- 1.8	+/- 3.0	+/- 4.1	+/- 5.5	+/- 6.6	+/- 7.7	46
2 h	13.8	17.9	20.6	24.0	26.5	29.0	46
	+/- 1.2	+/- 2.0	+/- 2.8	+/- 3.7	+/- 4.5	+/- 5.2	46

139	6 h	6.3	8.1	9.4	10.9	12.0	13.2	45
140		+/- 0.6	+/- 0.9	+/- 1.3	+/- 1.7	+/- 2.0	+/- 2.4	45
141	12 h	3.7	4.8	5.6	6.6	7.3	8.0	44
142		+/- 0.3	+/- 0.6	+/- 0.8	+/- 1.1	+/- 1.3	+/- 1.5	44
143	24 h	2.1	2.7	3.1	3.6	4.0	4.3	46
144		+/- 0.2	+/- 0.3	+/- 0.4	+/- 0.5	+/- 0.7	+/- 0.8	46

Table 3 : Interpolation Equation / Équation d'interpolation: $R = A \cdot T^B$

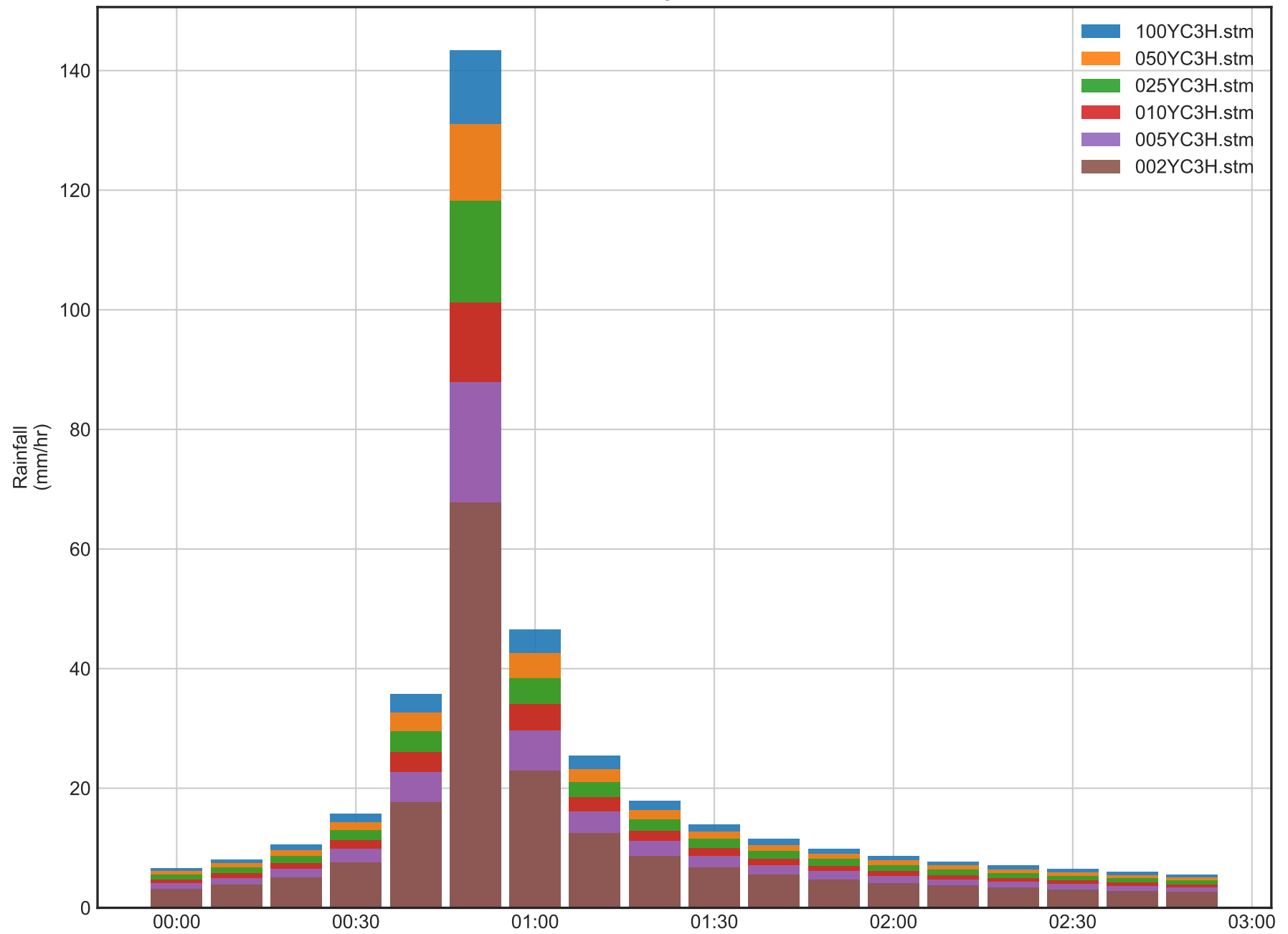
R = Interpolated Rainfall rate (mm/h)/Intensité interpolée de la pluie (mm/h)

RR = Rainfall rate (mm/h) / Intensité de la pluie (mm/h)

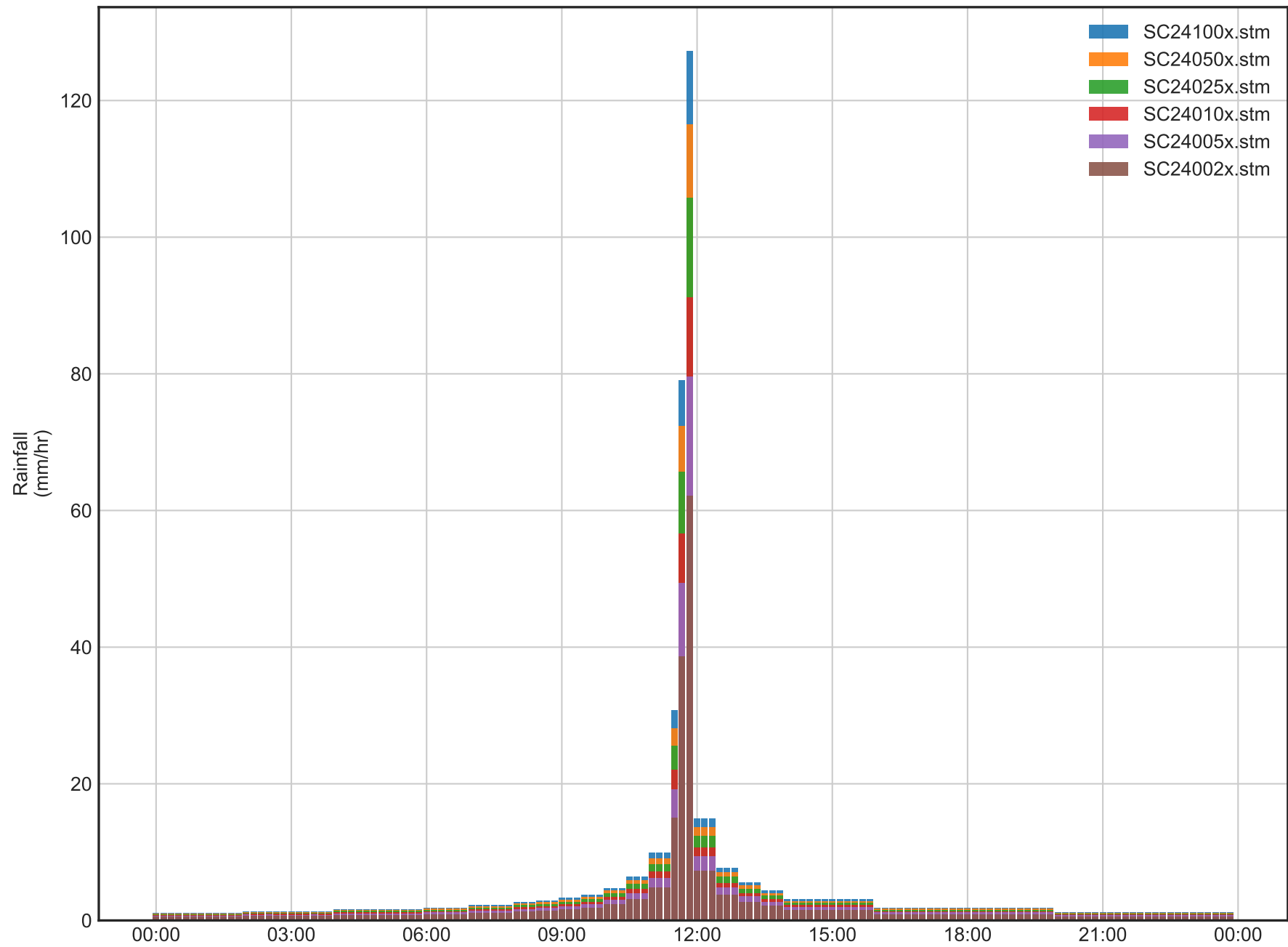
T = Rainfall duration (h) / Durée de la pluie (h)

156	Statistics/Statistiques	2	5	10	25	50	100
157		yr/ans	yr/ans	yr/ans	yr/ans	yr/ans	yr/ans
158	Mean of RR/Moyenne de RR	33.1	43.0	49.6	57.9	64.0	70.1
159	Std. Dev. /Écart-type (RR)	31.6	41.3	47.7	55.8	61.9	67.8
160	Std. Error/Erreur-type	7.6	9.6	10.9	12.6	13.9	15.1
161	Coefficient (A)	20.5	26.5	30.5	35.5	39.3	43.0
162	Exponent/Exposant (B)	-0.676	-0.677	-0.678	-0.679	-0.679	-0.679
163	Mean % Error/% erreur moyenne	8.5	8.1	8.0	7.8	7.7	7.7

Chicago Storms



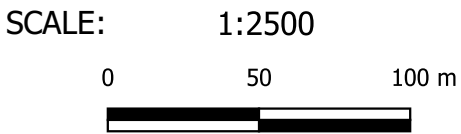
SCS Storms





Legend

-  Drainage Area
[Name]
[Area]





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Hogan Properties

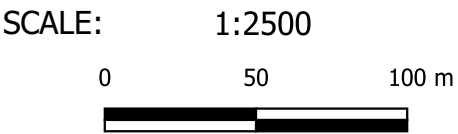
Figure A1: Pre Dev Areas

PROJECT	2468-23
DRAWN	BT
DATE	June 2023



Legend

- Drainage Area
- Land Use
 - Built Up Area - Pervious
 - Hedge Rows
 - Tilled
 - Transportation





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Hogan Properties

Figure A2: Land Use

PROJECT	2468-23
DRAWN	BT
DATE	June 2023



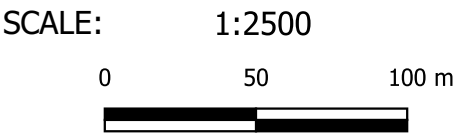
Legend

 Drainage Area

Soils

 OTONABEE LOAM

 SOLMESVILLE CLAY LOAM





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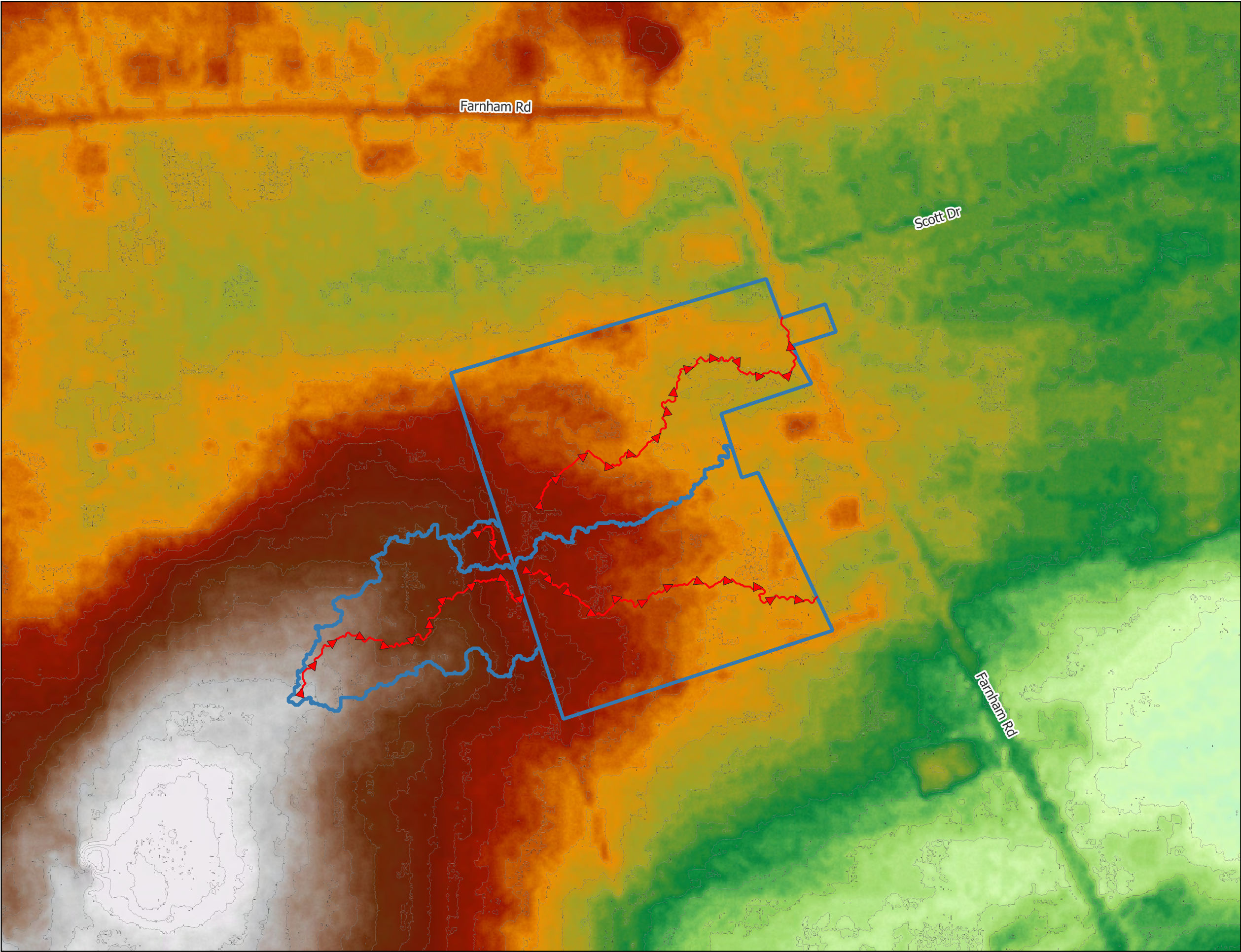
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Hogan Properties

Figure A3: Soils Map

PROJECT	2468-23
DRAWN	BT
DATE	June 2023



Legend

-  Drainage Area
-  Flow Lengths

Terrain (m)

-  108
-  109
-  110
-  111
-  112
-  113
-  114
-  115
-  116
-  117
-  118
-  119

SCALE: 1:2500

0 50 100 m



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ACADIA
ENGINEERING

Hogan Properties

Figure A4: Flow Lengths

PROJECT	2468-23
DRAWN	BT
DATE	June 2023

Table A1: Calculation of SCS Curve Number (CN)

Dev-FarnN (2.562 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.066	Transportation	SOLMESVILLE CLAY LOAM	C	Fair	98	2.6%	2.5
0.216	Hedge Rows	SOLMESVILLE CLAY LOAM	C	Fair	70	8.4%	5.9
0.029	Built Up Area - Pervious	SOLMESVILLE CLAY LOAM	C	Fair	79	1.1%	0.9
2.252	Tilled	SOLMESVILLE CLAY LOAM	C	Fair	79	87.9%	69.4
						CN	79

Dev-FarnS (2.142 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.296	Hedge Rows	SOLMESVILLE CLAY LOAM	C	Fair	70	13.8%	9.7
1.831	Tilled	SOLMESVILLE CLAY LOAM	C	Fair	79	85.5%	67.5
0.015	Built Up Area - Pervious	SOLMESVILLE CLAY LOAM	C	Fair	79	0.7%	0.6
						CN	78

Ext-FarnN (0.096 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.047	Hedge Rows	SOLMESVILLE CLAY LOAM	C	Fair	70	49.0%	34.3
0.049	Tilled	SOLMESVILLE CLAY LOAM	C	Fair	79	51.0%	40.3
						CN	75

Ext-FarnS (1.094 ha)							
Area (ha)	Land Type	Soil Name	Soil Condition	Soil Group	CN	% of Catchment	Weighted CN
0.861	Tilled	SOLMESVILLE CLAY LOAM	C	Fair	79	78.7%	62.2
0.029	Hedge Rows	SOLMESVILLE CLAY LOAM	C	Fair	70	2.7%	1.9
0.204	Tilled	OTONABEE LOAM	B	Fair	69	18.6%	12.9
						CN	77

Table A2: Time to Peak Calculations

Parameter	Units	Ext-FarnS	Ext-FarnN	Dev-FarnS	Dev-FarnN
Area	ha	1.09	0.10	2.14	2.56
CN	-	79	78	75	77
Ptotal to calc C from CN, use 2 yr 3 hr Chicago stom	P(mm)	31.05	31.05	31.05	31.05
	Ia(mm)	4.67	4.67	4.67	4.67
	RV(mm)	7.3	7.0	6.2	6.8
Ptotal to calc C from CN, use 2 yr 24 hr SCS stom	P(mm)	50.77	50.77	50.77	50.77
	RV(mm)	18.5	17.9	16.0	17.4
C (From Chicago storm)	-	0.24	0.23	0.20	0.22
C (From SCS storm)	-	0.37	0.35	0.32	0.34
Length of Channel	m	253	46	290	348
	ft	829	150	953	1141
Elevation of Head Water	m	118.12	115.05	114.56	114.24
	ft	388	377	376	375
Elevation of Outlet	m	114.52	114.64	112.33	112.36
	ft	376	376	369	369
Average Slope	m/m	1.42%	0.89%	0.77%	0.54%
	ft/ft	1.42%	0.89%	0.77%	0.54%
Kirpich					
Time of Concentration	mins	7	2	10	13
Time to Peak	min	5	2	7	9
Time to Peak	Hours	0.08	0.03	0.11	0.15
FAA (From Chicago storm)					
Time of Concentration	mins	40	20	55	66
Time to Peak	mins	27	13	36	44
Time to Peak	Hours	0.44	0.22	0.61	0.73
FAA (From SCS storm)					
Time of Concentration	mins	34	17	48	57
Time to Peak	mins	23	11	32	38
Time to Peak	Hours	0.38	0.19	0.53	0.63
Barnsby Williams					
Time of Concentration	mins	13	3	16	21
Time to Peak	mins	9	2	11	14
Time to Peak	Hours	0.15	0.04	0.18	0.23
SCS					
Time of Concentration	mins	24	8	41	53
Time to Peak	mins	16	5	27	35
Time to Peak	Hours	0.26	0.09	0.46	0.59
Selected Method					
FAA (From SCS storm)					
Time to Peak	min	23	11	32	38
Time to Peak	Hours	0.38	0.19	0.53	0.63

Note:

All methods calculated as per Appendix A of the SWMHYMO manual

Time to Peak calculated as 2/3 Time of concentration

```

1  20      Metric units
2  *#*****
3  *# Project Name: [P2468-JB Hogan Property - Bellville]    Project Number: [2468]
4  *# Date       : 2023-05
5  *# Modeller   : JB
6  *# Company    : JFSA
7  *# License #  : 2582634
8  *#*****
9  *#*****
10 *% 25mm, 3-Hour Chicago Storm
11 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[001]
12             ["25mmC3H.stm"] <--storm filename, one per line for NSTORM time
13 *%-----|-----
14 READ STORM  STORM_FILENAME=["storm.001"]
15 *%-----|-----
16 *=====|=====
17 CALIB NASHYD      NHYD=["Ext-FarnS"], DT=[1]min, AREA=[1.09](ha)
18                   DWF=[0.0](cms), CN=[79], IA=[4.67](mm), N=[3.0]
19                   Tp=[0.38]hrs, END=-1
20 *%-----|-----
21 CALIB NASHYD      NHYD=["Ext-FarnN"], DT=[1]min, AREA=[0.10](ha)
22                   DWF=[0.0](cms), CN=[78], IA=[4.67](mm), N=[3.0]
23                   Tp=[0.19]hrs, END=-1
24 *%-----|-----
25 CALIB NASHYD      NHYD=["Dev-FarnS"], DT=[1]min, AREA=[2.14](ha)
26                   DWF=[0.0](cms), CN=[75], IA=[4.67](mm), N=[3.0]
27                   Tp=[0.53]hrs, END=-1
28 *%-----|-----
29 CALIB NASHYD      NHYD=["Dev-FarnN"], DT=[1]min, AREA=[2.56](ha)
30                   DWF=[0.0](cms), CN=[77], IA=[4.67](mm), N=[3.0]
31                   Tp=[0.63]hrs, END=-1
32 *%-----|-----
33 *% STORMS
34 *%-----|-----
35 *% 2-Year, 3-Hour Chicago Storm
36 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
37             ["002YC3H.stm"] <--storm filename, one per line for NSTORM time
38 *%-----|-----
39 *% 5-Year, 3-Hour Chicago Storm
40 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
41             ["005YC3H.stm"] <--storm filename, one per line for NSTORM time
42 *%-----|-----
43 *% 10-Year, 3-Hour Chicago Storm
44 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
45             ["010YC3H.stm"] <--storm filename, one per line for NSTORM time
46 *%-----|-----
47 *% 25-Year, 3-Hour Chicago Storm
48 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
49             ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
50 *%-----|-----
51 *% 50-Year, 3-Hour Chicago Storm
52 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
53             ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
54 *%-----|-----
55 *% 100-Year, 3-Hour Chicago Storm
56 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
57             ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
58 *%-----|-----
59 *% 2-Year, 24-Hour SCS Storm
60 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
61             ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
62 *%-----|-----
63 *% 5-Year, 24-Hour SCS Storm
64 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
65             ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
66 *%-----|-----
67 *% 10-Year, 24-Hour SCS Storm

```



```
68 START                TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[110]
69                ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
70 %-----|-----|
71 % 25-Year, 24-Hour SCS Storm
72 START                TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[125]
73                ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
74 %-----|-----|
75 % 50-Year, 24-Hour SCS Storm
76 START                TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[150]
77                ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
78 %-----|-----|
79 % 100-Year, 24-Hour SCS Storm
80 START                TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[199]
81                ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
82 %-----|-----|
83 FINISH
```

```
00001 *****
00002 SSSSS W W M M H H Y Y M M M 000 222 000 11 5555 *****
00003 S W W M M H H Y Y M M M 0 0 2 0 0 11 5
00004 SSSSS W W M M H H Y Y M M M 0 0 2 0 0 11 5 Ver 5.500
00005 SSSSS W W M M H H Y Y M M M 0 0 222 0 0 11 555 FEB 2015
00006 SSSSS W W M M H H Y Y M M M 0 0 2 0 0 11 5
00007 *****
00008 *****
00009 *****
00010 StormWater Management Hydrologic Model 222 000 11 555 *****
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```

00361> [Cn= 77.0: N= 3.00: Tp= .63]
00362> ** END OF RUN : 104
00363>
00364>
00365>
00366>
00367>
00368>
00369>
00370> RUN:COMMAND#
00371> R0105:C00001
00372> START
00373> [TZERO = .00 hrs on 0]
00374> [METOUT= 2 (1=Imperial, 2=metric output)]
00375> [NFORM= 1]
00376> [NRUN = 0105]
00377> *****
00378> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00379> # Date : 2023-05
00380> # Modeler : JB
00381> # Company : JFSA
00382> # License # : 2582634
00383> *****
00384>
00385> R0105:C00002
00386> READ STORM
00387> Filename = storm.001
00388> Comment = 5 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00389> [SDT=10.00:SDUR= 24.00:PTOT= 65.00]
00390> R0105:C00003-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00391> CALIB NASHVD 1.0 01:Ext-FarnS 1.09 .050 No_date 12:17 28.47 .438 .000
00392> [Cn= 79.0: N= 3.00: Tp= .30]
00393> R0105:C00004-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00394> CALIB NASHVD 1.0 01:Ext-FarnN .10 .007 No_date 12:06 27.57 .424 .000
00395> [Cn= 78.0: N= 3.00: Tp= .10]
00396> R0105:C00005-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00397> CALIB NASHVD 1.0 01:Dev-FarnS 2.14 .068 No_date 12:28 25.10 .386 .000
00398> [Cn= 75.0: N= 3.00: Tp= .53]
00399> R0105:C00006-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00400> CALIB NASHVD 1.0 01:Dev-FarnN 2.58 .077 No_date 12:35 26.72 .411 .000
00401> [Cn= 77.0: N= 3.00: Tp= .63]
00402> ** END OF RUN : 109
00403>
00404>
00405>
00406>
00407>
00408>
00409>
00410> RUN:COMMAND#
00411> R0110:C00001
00412> START
00413> [TZERO = .00 hrs on 0]
00414> [METOUT= 2 (1=Imperial, 2=metric output)]
00415> [NFORM= 1]
00416> [NRUN = 0110]
00417> *****
00418> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00419> # Date : 2023-05
00420> # Modeler : JB
00421> # Company : JFSA
00422> # License # : 2582634
00423> *****
00424>
00425> R0110:C00002
00426> READ STORM
00427> Filename = storm.001
00428> Comment = 10 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00429> [SDT=10.00:SDUR= 24.00:PTOT= 74.47]
00430> R0110:C00003-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00431> CALIB NASHVD 1.0 01:Ext-FarnS 1.09 .063 No_date 12:17 35.48 .476 .000
00432> [Cn= 79.0: N= 3.00: Tp= .30]
00433> R0110:C00004-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00434> CALIB NASHVD 1.0 01:Ext-FarnN .10 .009 No_date 12:06 34.44 .462 .000
00435> [Cn= 78.0: N= 3.00: Tp= .10]
00436> R0110:C00005-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00437> CALIB NASHVD 1.0 01:Dev-FarnS 2.14 .066 No_date 12:27 31.54 .424 .000
00438> [Cn= 75.0: N= 3.00: Tp= .53]
00439> R0110:C00006-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00440> CALIB NASHVD 1.0 01:Dev-FarnN 2.58 .097 No_date 12:35 33.45 .448 .000
00441> [Cn= 77.0: N= 3.00: Tp= .63]
00442> ** END OF RUN : 124
00443>
00444>
00445>
00446>
00447>
00448>
00449>
00450> RUN:COMMAND#
00451> R0125:C00001
00452> START
00453> [TZERO = .00 hrs on 0]
00454> [METOUT= 2 (1=Imperial, 2=metric output)]
00455> [NFORM= 1]
00456> [NRUN = 0125]
00457> *****
00458> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00459> # Date : 2023-05
00460> # Modeler : JB
00461> # Company : JFSA
00462> # License # : 2582634
00463> *****
00464>
00465> R0125:C00002
00466> READ STORM
00467> Filename = storm.001
00468> Comment = 25 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00469> [SDT=10.00:SDUR= 24.00:PTOT= 86.41]
00470> R0125:C00003-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00471> CALIB NASHVD 1.0 01:Ext-FarnS 1.09 .080 No_date 12:17 44.77 .518 .000
00472> [Cn= 79.0: N= 3.00: Tp= .30]
00473> R0125:C00004-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00474> CALIB NASHVD 1.0 01:Ext-FarnN .10 .011 No_date 12:05 43.56 .504 .000
00475> [Cn= 78.0: N= 3.00: Tp= .10]
00476> R0125:C00005-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00477> CALIB NASHVD 1.0 01:Dev-FarnS 2.14 .118 No_date 12:27 40.15 .465 .000
00478> [Cn= 75.0: N= 3.00: Tp= .53]
00479> R0125:C00006-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00480> CALIB NASHVD 1.0 01:Dev-FarnN 2.58 .123 No_date 12:34 42.40 .491 .000
00481> [Cn= 77.0: N= 3.00: Tp= .63]
00482> ** END OF RUN : 149
00483>
00484>
00485>
00486>
00487>
00488>
00489>
00490> RUN:COMMAND#
00491> R0150:C00001
00492> START
00493> [TZERO = .00 hrs on 0]
00494> [METOUT= 2 (1=Imperial, 2=metric output)]
00495> [NFORM= 1]
00496> [NRUN = 0150]
00497> *****
00498> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00499> # Date : 2023-05
00500> # Modeler : JB
00501> # Company : JFSA
00502> # License # : 2582634
00503> *****
00504>
00505> R0150:C00002
00506> READ STORM
00507> Filename = storm.001
00508> Comment = 50 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00509> [SDT=10.00:SDUR= 24.00:PTOT= 95.19]
00510> R0150:C00003-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00511> CALIB NASHVD 1.0 01:Ext-FarnS 1.09 .093 No_date 12:16 51.84 .545 .000
00512> [Cn= 79.0: N= 3.00: Tp= .30]
00513> R0150:C00004-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00514> CALIB NASHVD 1.0 01:Ext-FarnN .10 .013 No_date 12:05 50.52 .531 .000
00515> [Cn= 78.0: N= 3.00: Tp= .10]
00516> R0150:C00005-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00517> CALIB NASHVD 1.0 01:Dev-FarnS 2.14 .129 No_date 12:27 46.77 .491 .000
00518> [Cn= 75.0: N= 3.00: Tp= .53]
00519> R0150:C00006-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00520> CALIB NASHVD 1.0 01:Dev-FarnN 2.58 .144 No_date 12:34 49.24 .517 .000
00521> [Cn= 77.0: N= 3.00: Tp= .63]
00522> ** END OF RUN : 198
00523>
00524>
00525>
00526>
00527>
00528>
00529>
00530> RUN:COMMAND#
00531> R0199:C00001
00532> START
00533> [TZERO = .00 hrs on 0]
00534> [METOUT= 2 (1=Imperial, 2=metric output)]
00535> [NFORM= 1]
00536> [NRUN = 0199]
00537> *****
00538> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00539> # Date : 2023-05
00540> # Modeler : JB

```

```

00541> # Company : JFSA
00542> # License # : 2582634
00543> *****
00544>
00545> R0199:C00002
00546> READ STORM
00547> Filename = storm.001
00548> Comment = 100 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00549> [SDT=10.00:SDUR= 24.00:PTOT= 103.90]
00550> R0199:C00003-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00551> CALIB NASHVD 1.0 01:Ext-FarnS 1.09 .107 No_date 12:16 59.12 .569 .000
00552> [Cn= 79.0: N= 3.00: Tp= .30]
00553> R0199:C00004-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00554> CALIB NASHVD 1.0 01:Ext-FarnN .10 .015 No_date 12:05 57.69 .555 .000
00555> [Cn= 78.0: N= 3.00: Tp= .10]
00556> R0199:C00005-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00557> CALIB NASHVD 1.0 01:Dev-FarnS 2.56 .165 No_date 12:34 56.30 .541 .000
00558> [Cn= 75.0: N= 3.00: Tp= .53]
00559> R0199:C00006-----DTmin-ID:NYVD-----AREAh-QPEAKCns-TpeakDate_hh:mm-----Rvmm-R.C-----DwFcns
00560> CALIB NASHVD 1.0 01:Dev-FarnN 2.56 .165 No_date 12:34 56.30 .541 .000
00561> [Cn= 77.0: N= 3.00: Tp= .63]
00562> R0199:C00002
00563> FINISH
00564>
00565> *****
00566> WARNINGS / ERRORS / NOTES
00567>
00568> Simulation ended on 2023-06-20 at 12:05:44
00569> *****
00570>

```

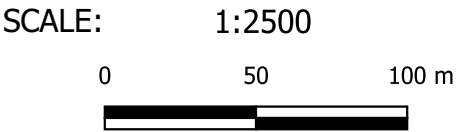
Attachment B

Post Development



Legend

- Development Area
- Parcel Lines





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www.jfsa.com



**ACADIA
ENGINEERING**

Hogan Properties

Figure B1: Post Development

PROJECT	2468-23
DRAWN	BT
DATE	June 2023

Table B1 - Hogan Property - SWM Pond Stage/Storage Curve

Elevation	Note	Incremental Area (m ²)	Cumulative Area (m ²)	Incremental Volume (m ³)	Cumulative Volume (m ³)	Active Storage (m ³)
109.25	Pond Bottom	43.72	43.7	0	0	-
109.3		7.83	51.5	2	2	-
109.4		8.34	59.9	6	8	-
109.5		380.51	440.4	22	30	-
109.6		45.98	486.4	46	76	-
109.7		46.96	533.3	51	127	-
109.8		47.92	581.3	56	183	-
109.9		48.89	630.1	61	244	-
110		49.86	680.0	65	309	-
110.1		50.82	730.8	71	380	-
110.2		51.79	782.6	76	455	-
110.3		52.75	835.3	81	536	-
110.4		53.73	889.1	86	622	-
110.5		54.69	943.8	92	714	-
110.6		62.21	1,006.0	97	811	-
110.7		54.07	1,060.0	103	915	0
110.8	Perm Pool Extened Detention	54.73	1,114.8	109	1,023	109
110.9		55.45	1,170.2	114	1,138	223
111		56.18	1,226.4	120	1,258	343
111.1		56.89	1,283.3	125	1,383	468
111.2		57.62	1,340.9	131	1,514	599
111.3		58.33	1,399.3	137	1,651	736
111.4		59.06	1,458.3	143	1,794	879
111.5		59.77	1,518.1	149	1,943	1,028
111.6		60.49	1,578.6	155	2,098	1,183
111.7		61.21	1,639.8	161	2,259	1,344
111.8		61.93	1,701.7	167	2,426	1,511
111.9		62.65	1,764.4	173	2,599	1,684
112		63.37	1,827.7	180	2,779	1,864
112.1		64.09	1,891.8	186	2,965	2,050
112.2		64.80	1,956.6	192	3,157	2,242
112.3		65.52	2,022.1	199	3,356	2,441
112.4		66.09	2,088.2	206	3,561	2,647
112.5	Top of Pond	1.30	2,089.5	209	3,770	2,856

Table B-2: Criteria for Required Storage Volumes

Pond	Area ⁽¹⁾ (ha)	Imperviousness (%)	Storage Volume for Impervious Level ⁽¹⁾ (m ³ /ha)
SWM Pond	4.71	55	190
		67.0	218
		70	225

⁽¹⁾ Protection Level for Wet Pond: Enhanced 80% long-term S.S. removal.

SWM Planning & Design Manual, Table 3.2, p.3-10 (March 2003).

Table B-3: Required Storage Volumes for SWM Facility

Pond Component	Required Volume (m ³)	Provided Volume ⁽⁴⁾ (m ³)	Volume Ratio	Elevation (m)
Permanent Pool (PP) ⁽¹⁾	838	915	1.09	110.70
Extended Detention ⁽²⁾	188	599	3.18	111.25
Forebay (20% PP)	168	N/A	N/A	-
PP - Forebay	671	N/A	N/A	-

⁽¹⁾ Required PP volume based on Table B-1.

⁽²⁾ Required quality control volume based on 40 m³/ha.

⁽⁴⁾ Provided volume based on stage-storage curve and extended detention (refer to Tables B-3 and B-4).

⁽⁶⁾ As per MOE, Maximum Forebay Area: 33% of Total Permanent Pool.

Table B-4: Extended Detention Drawdown Time for SWM Facility

Elev. (m)	Active Storage		C2 (m ² /m)	Drawdown Time (h)	Drawdown Time (days)	Flow (m ³ /s)	Demarkation Point
	V (m ³)	A (m ²)					
110.70	0	1,060	0.00	0.00		0.000	PP Elev
110.80	109	1,115	0.10	10.86	0.45	0.006	
110.90	223	1,170	0.20	14.95	0.62	0.010	QC Elev
111.00	343	1,226	0.30	17.86	0.74	0.013	
111.10	468	1,283	0.40	20.33	0.85	0.015	
111.20	599	1,341	0.50	22.56	0.94	0.017	Ext. Det.
111.30	736	1,399	0.60	24.39	1.02	0.024	
111.40	879	1,458	0.70	25.72	1.07	0.036	
111.50	1028	1,518	0.80	26.74	1.11	0.045	
111.60	1183	1,579	0.90	27.62	1.15	0.053	
111.70	1344	1,640	1.00	28.42	1.18	0.059	
111.80	1511	1,702	1.10	29.12	1.21	0.074	
111.90	1684	1,764	1.20	29.68	1.24	0.097	
112.00	1864	1,828	1.30	30.15	1.26	0.119	
112.10	2050	1,892	1.40	30.55	1.27	0.138	
112.20	2242	1,957	1.50	30.91	1.29	0.154	
112.30	2441	2,022	1.60	31.00	1.29	1.167	
112.40	2647	2,088	1.70	31.02	1.29	3.002	
112.50	2856	2,090	1.80	31.04	1.29	5.370	Top Of Pond

Notes:

- C2 is the slope coefficient from the area-depth linear regression.
- PP Elev indicates the elevation of the permanent pool.
- QC Elev indicates the elevation of the storage volume required by MOE for quality control.
- Ext Det indicates the elevation of extended detention.

Table B-5: Stage-Storage-Outflow Curve for SWM Facility (Free Outfall Conditions)

Elevation (m)	Active Sto. (m ³)	Demarkation Points	Quality Control Vertical Orifice Dia (m) 0.110		Quantity Control 1 Vertical Orifice Dia (m) 0.160		Quantity Control 2 Vertical Orifice Dia (m) 0.240		Emergency Overflow Broad Crested Weir L (m) 20.000		Outflow (m ³ /s)	Storage (ha-m)
			Area (m ²) Invert (m) C _o Q @ D Depth	Outflow (m ³ /s)	Area (m ²) Invert (m) C _o Q @ D Depth	Outflow (m ³ /s)	Area (m ²) Invert (m) C _o Q @ D Depth	Outflow (m ³ /s)	C _w Invert (m) n contr. Depth	Outflow (m ³ /s)		
110.70	0	PP Elev	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
110.80	109	QC Elev	0.100	0.006	0.000	0.000	0.000	0.000	0.000	0.000	0.006	0.011
110.90	223		0.200	0.010	0.000	0.000	0.000	0.000	0.000	0.000	0.010	0.022
111.00	343		0.300	0.013	0.000	0.000	0.000	0.000	0.000	0.000	0.013	0.034
111.10	468	Ext. Det.	0.400	0.015	0.000	0.000	0.000	0.000	0.000	0.000	0.015	0.047
111.20	599		0.500	0.017	0.000	0.000	0.000	0.000	0.000	0.000	0.017	0.060
111.30	736		0.600	0.019	0.050	0.005	0.000	0.000	0.000	0.000	0.024	0.074
111.40	879		0.700	0.021	0.150	0.015	0.000	0.000	0.000	0.000	0.036	0.088
111.50	1028		0.800	0.023	0.250	0.023	0.000	0.000	0.000	0.000	0.045	0.103
111.60	1183		0.900	0.024	0.350	0.029	0.000	0.000	0.000	0.000	0.053	0.118
111.70	1344		1.000	0.025	0.450	0.034	0.000	0.000	0.000	0.000	0.059	0.134
111.80	1511		1.100	0.027	0.550	0.038	0.050	0.009	0.000	0.000	0.074	0.151
111.90	1684		1.200	0.028	0.650	0.042	0.150	0.027	0.000	0.000	0.097	0.168
112.00	1864		1.300	0.029	0.750	0.045	0.250	0.045	0.000	0.000	0.119	0.186
112.10	2050		1.400	0.030	0.850	0.048	0.350	0.060	0.000	0.000	0.138	0.205
112.20	2242		1.500	0.031	0.950	0.052	0.450	0.071	0.000	0.000	0.154	0.224
112.30	2441	Ovf Elev Top of Pond	1.600	0.032	1.050	0.054	0.550	0.081	0.100	0.998	1.167	0.244
112.40	2647		1.700	0.033	1.150	0.057	0.650	0.090	0.200	2.821	3.002	0.265
112.50	2856		1.800	0.034	1.250	0.060	0.750	0.099	0.300	5.177	5.370	0.286

- Notes :
- PP Elev indicates the elevation of the permanent pool.
 - QC Elev indicates the elevation of the storage volume required by MOE for quality control.
 - Ext Det indicates the elevation of extended detention provided.
 - Ovf Elev indicates the elevation of the overflow provided above the 100-year water level.
 - Top of Berm indicates the elevation at the top of the berm.

CALCULATION SHEET B-1: FOREBAY SIZING FOR SWM FACILITY

Settling Criteria

From the SWMP Manual, the required length for settling is as follows:

$$L_{min} = \left(\frac{rQ_p}{V_s} \right)^{0.5}$$

where: r = length to width ratio, at the invert of the inlet pipe.
 Q_p = peak outflow during design quality storm
 V_s = settling velocity

Input: r = 1.67 (15 m / 9 m)
 Q_p = 0.010 m³/s (at elevation 65.0m)
 V_s = 0.0003 m/s

$$L_{min} = 7.43 \text{ m}$$

The peak flow rate from the pond during the quality storm is taken as the flow that would occur just below the quantity controls (Refer to Table B-5 of Appendix B)

Dispersion Criteria

From the SWMP Manual, the required length for dispersion is as follows:

$$L_{min} = \frac{8Q}{dV_f}$$

where: Q = Inlet flowrate (10-Year, 24-Hour SCS Storm)
 d = depth of permanent pool (forebay)
 V_f = desired final velocity

Input: Q = 0.867 m³/s
 d = 2.55 m
 V_f = 0.5 m/s

$$L_{min} = 5.44 \text{ m}$$

The minimum forebay length is determined by the larger of the settling or dispersion criteria.

Minimum Length of Forebay Required 7.43 m
Length of Forebay Provided 15.00 m (at elevation 109.85m)

Average Forebay Velocity - 25mm Event

From the SWMP Manual, the maximum allowable average velocity is 0.15 m/s:

$$V_{avg} = \frac{Q}{d W_{avg}}$$

where: Q = Inlet flowrate (25mm, 4-Hour CHI Storm)
 d = depth of forebay during peak
 W_{avg} = average width of forebay

Input: Q = 0.338 m³/s
 d = 1.92 m
 W_{avg} = 9 m (8 m bottom, 17 m permanent pool)

$$V = 0.02 \text{ m/s} < 0.15 \text{ m/s}$$

Average Forebay Velocity - 10 Year Event

From the SWMP Manual, the maximum allowable average velocity is 0.15 m/s:

$$V_{avg} = \frac{Q}{d W_{avg}}$$

where: Q = Inlet flowrate (10-Year, 24-Hour SCS Storm)
 d = depth of forebay during peak
 W_{avg} = average width of forebay

Input: Q = 0.867 m³/s
 d = 2.55 m
 W_{avg} = 9 m (8 m bottom, 17 m permanent pool)

$$V = 0.04 \text{ m/s} \leq 0.15 \text{ m/s}$$


```

1  20      Metric units
2  *#*****
3  *# Project Name: [P2468-JB Hogan Property - Bellville]    Project Number: [2468]
4  *# Date       : 2023-05
5  *# Modeller   : JB
6  *# Company    : JFSA
7  *# License #   : 2582634
8  *#*****
9  *#*****
10 *% 25mm, 3-Hour Chicago Storm
11 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[001]
12 *          ["25mmC3H.stm"] <--storm filename, one per line for NSTORM time
13 *%-----|-----
14 READ STORM  STORM_FILENAME=["storm.001"]
15 *%-----|-----
16 *=====|=====
17 *Development Lands
18 CALIB STANDHYD NHYD=["Post"], DT=[1](min), AREA=[4.710](ha), XIMP=[0.57],
19 TIMP=[0.67], DWF=[0.](cms),
20 LOSS=[1] Horton Equ: Fo=[76.2](mm/hr), Fc=[13.2](mm/hr),
21 DCAY=[4.14](/hr), F=[0.00](mm),
22 Pervious areas: IAPER=[4.67](mm), SLPP=[2.0](%), LGP=[40](m),
23 MNP=[0.25], SCP=[0](min),
24 Impervious areas: IAimp=[1.57](mm), SLPI=[0.5](%), LGI=[177](m),
25 MNI=[0.013], SCI=[0](min),
26 RAINFALL=[ , , -1](mm/hr)
27 *%-----|-----
28 ROUTE RESERVOIR NHYDout=["SWM-Out"], NHYDin=["POST"], RDT=[1](min),
29 TABLE of ( OUTFLOW-STORAGE ) values
30 (cms) - (ha-m)
31 [ 0 , 0 ]
32 [ 0.006 , 0.011 ]
33 [ 0.01 , 0.022 ]
34 [ 0.013 , 0.034 ]
35 [ 0.015 , 0.047 ]
36 [ 0.017 , 0.06 ]
37 [ 0.024 , 0.074 ]
38 [ 0.036 , 0.088 ]
39 [ 0.045 , 0.103 ]
40 [ 0.053 , 0.118 ]
41 [ 0.059 , 0.134 ]
42 [ 0.074 , 0.151 ]
43 [ 0.097 , 0.168 ]
44 [ 0.119 , 0.186 ]
45 [ 0.138 , 0.205 ]
46 [ 0.154 , 0.224 ]
47 [ 1.167 , 0.244 ]
48 [ 3.002 , 0.265 ]
49 [ 5.37 , 0.286 ]
50 [ -1 , -1 ] (maximum one hundred pairs of points)
51 NHYDovf=["SWM-Over"],
52 *%-----|-----
53 ADD HYD      NHYDsum=["Total"], NHYDs to add=["SWM-Out"+"SWM-Over"]
54 *%-----|-----
55 **% STORMS
56 *%-----|-----
57 *% 2-Year, 3-Hour Chicago Storm
58 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[002]
59 [ "002YC3H.stm" ] <--storm filename, one per line for NSTORM time
60 *%-----|-----
61 *% 5-Year, 3-Hour Chicago Storm
62 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[005]
63 [ "005YC3H.stm" ] <--storm filename, one per line for NSTORM time
64 *%-----|-----
65 *% 10-Year, 3-Hour Chicago Storm
66 START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[010]
67 [ "010YC3H.stm" ] <--storm filename, one per line for NSTORM time

```

```

64  *%-----|-----|
65  *% 25-Year, 3-Hour Chicago Storm
66  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[025]
67             ["025YC3H.stm"] <--storm filename, one per line for NSTORM time
68  *%-----|-----|
69  *% 50-Year, 3-Hour Chicago Storm
70  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[050]
71             ["050YC3H.stm"] <--storm filename, one per line for NSTORM time
72  *%-----|-----|
73  *% 100-Year, 3-Hour Chicago Storm
74  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[099]
75             ["100YC3H.stm"] <--storm filename, one per line for NSTORM time
76  *%-----|-----|
77  *% 2-Year, 24-Hour SCS Storm
78  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[102]
79             ["SC24002x.stm"] <--storm filename, one per line for NSTORM time
80  *%-----|-----|
81  *% 5-Year, 24-Hour SCS Storm
82  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[105]
83             ["SC24005x.stm"] <--storm filename, one per line for NSTORM time
84  *%-----|-----|
85  *% 10-Year, 24-Hour SCS Storm
86  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[110]
87             ["SC24010x.stm"] <--storm filename, one per line for NSTORM time
88  *%-----|-----|
89  *% 25-Year, 24-Hour SCS Storm
90  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[125]
91             ["SC24025x.stm"] <--storm filename, one per line for NSTORM time
92  *%-----|-----|
93  *% 50-Year, 24-Hour SCS Storm
94  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[150]
95             ["SC24050x.stm"] <--storm filename, one per line for NSTORM time
96  *%-----|-----|
97  *% 100-Year, 24-Hour SCS Storm
98  START      TZERO=[0.0], METOUT=[2], NSTORM=[1], NRUN=[199]
99             ["SC24100x.stm"] <--storm filename, one per line for NSTORM time
100  *%-----|-----|
101  FINISH

```

```
00001 *****
00002 SSSSS W W M M H H H Y M M 000 222 000 11 5555 *****
00003 S W W M M H H H Y Y M M 0 0 2 0 0 11 5
00004 SSSSS W W M M H H H Y Y M M 0 0 2 0 0 11 5 Ver 5.900
00005 S W W M M H H H Y Y M M 0 0 222 0 0 11 555 FEB 2015
00006 SSSSS W W M M H H H Y Y M M 0 0 2 0 0 11 5
00007 *****
00008 StormWater Management Hydrologic Model 222 000 11 555 *****
00009 *****
00010 *****
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00361> # Modeller : JB
00362> # Company : JFSA
00363> # License # : 2582634
00364> *****
00365> #*****
00366> R0102:C00002-----
00367> READ STORM
00368> Filename = storm.001
00369> Comment = 2 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00370> [SDT=10.00:SDUR= 24.00:PTOT= 50.77]
00371> R0102:C00003-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00372> CALIB STANDHYD 1.0 01:Post 4.71 .523 No.date 12:01 33.26 .655 .000
00373> [XfPM:57:TIMP:.67]
00374> [Horton parameters: Fm= 76.20:Fc= 13.20:DCAY=4.14: F= .00]
00375> [Previous area: IAPer= 4.67:SLPP=2.00:LGPs= 40.:MNP=.250:SCPs= .0]
00376> [Impervious area: IALmp= 1.57:SLPI=.50:LGIs= 177.:MNI=.013:SCIs= .0]
00377> R0102:C00004-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00378> ROUTE RESERVOIR -> 1.0 02:POST 4.71 .523 No.date 12:01 33.26 n/a .000
00379> out <= 1.0 01:SMW-Out 4.71 .641 No.date 12:47 33.26 n/a .000
00380> overflow <= 1.0 03:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00381> (MxStoUsed=.9714E-01 n3, TotDvVol=.0000E+00 n3, N-Ovf= 0, TotDurOvf= 0.hrs)
00382> R0102:C00005-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00383> ADD HYD + 1.0 02:SMW-Over 4.71 .641 No.date 12:47 33.26 n/a .000
00384> SUM= 1.0 02:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00385> 1.0 01:Total 4.71 .641 No.date 12:47 33.26 n/a .000
00386> ** END OF RUN : 104
00387>
00388>
00389>
00390>
00391>
00392>
00393>
00394> RUN:COMMAND#
00395> R0105:C00001-----
00396> START
00397> [TZERO = .00 hrs on 0]
00398> [METOUT= 2 (1=imperial, 2=metric output)]
00399> [NSTORM= 1]
00400> [NRUN = 0105]
00401> *****
00402> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00403> # Date : 2023-05
00404> # Modeller : JB
00405> # Company : JFSA
00406> # License # : 2582634
00407> *****
00408> #*****
00409> R0105:C00002-----
00410> READ STORM
00411> Filename = storm.001
00412> Comment = 5 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00413> [SDT=10.00:SDUR= 24.00:PTOT= 65.00]
00414> R0105:C00003-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00415> CALIB STANDHYD 1.0 01:Post 4.71 .724 No.date 12:01 44.02 .677 .000
00416> [XfPM:57:TIMP:.67]
00417> [Horton parameters: Fm= 76.20:Fc= 13.20:DCAY=4.14: F= .00]
00418> [Previous area: IAPer= 4.67:SLPP=2.00:LGPs= 40.:MNP=.250:SCPs= .0]
00419> [Impervious area: IALmp= 1.57:SLPI=.50:LGIs= 177.:MNI=.013:SCIs= .0]
00420> R0105:C00004-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00421> ROUTE RESERVOIR -> 1.0 02:POST 4.71 .724 No.date 12:01 44.02 n/a .000
00422> out <= 1.0 01:SMW-Out 4.71 .657 No.date 12:42 44.02 n/a .000
00423> overflow <= 1.0 03:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00424> (MxStoUsed=.1293E+00 n3, TotDvVol=.0000E+00 n3, N-Ovf= 0, TotDurOvf= 0.hrs)
00425> R0105:C00005-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00426> ADD HYD + 1.0 02:SMW-Over 4.71 .657 No.date 12:42 44.02 n/a .000
00427> 1.0 02:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00428> SUM= 1.0 01:Total 4.71 .657 No.date 12:42 44.02 n/a .000
00429> ** END OF RUN : 109
00430>
00431>
00432>
00433>
00434>
00435>
00436>
00437> RUN:COMMAND#
00438> R0110:C00001-----
00439> START
00440> [TZERO = .00 hrs on 0]
00441> [METOUT= 2 (1=imperial, 2=metric output)]
00442> [NSTORM= 1]
00443> [NRUN = 0110]
00444> *****
00445> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00446> # Date : 2023-05
00447> # Modeller : JB
00448> # Company : JFSA
00449> # License # : 2582634
00450> *****
00451> #*****
00452> R0110:C00002-----
00453> READ STORM
00454> Filename = storm.001
00455> Comment = 10 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00456> [SDT=10.00:SDUR= 24.00:PTOT= 74.47]
00457> R0110:C00003-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00458> CALIB STANDHYD 1.0 01:Post 4.71 .867 No.date 12:01 51.38 .699 .000
00459> [XfPM:57:TIMP:.67]
00460> [Horton parameters: Fm= 76.20:Fc= 13.20:DCAY=4.14: F= .00]
00461> [Previous area: IAPer= 4.67:SLPP=2.00:LGPs= 40.:MNP=.250:SCPs= .0]
00462> [Impervious area: IALmp= 1.57:SLPI=.50:LGIs= 177.:MNI=.013:SCIs= .0]
00463> R0110:C00004-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00464> ROUTE RESERVOIR -> 1.0 02:POST 4.71 .867 No.date 12:01 51.38 n/a .000
00465> out <= 1.0 01:SMW-Out 4.71 .074 No.date 12:39 51.38 n/a .000
00466> overflow <= 1.0 03:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00467> (MxStoUsed=.1533E+00 n3, TotDvVol=.0000E+00 n3, N-Ovf= 0, TotDurOvf= 0.hrs)
00468> R0110:C00005-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00469> ADD HYD + 1.0 02:SMW-Over 4.71 .074 No.date 12:39 51.38 n/a .000
00470> 1.0 02:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00471> SUM= 1.0 01:Total 4.71 .074 No.date 12:39 51.38 n/a .000
00472> ** END OF RUN : 124
00473>
00474>
00475>
00476>
00477>
00478>
00479>
00480> RUN:COMMAND#
00481> R0125:C00001-----
00482> START
00483> [TZERO = .00 hrs on 0]
00484> [METOUT= 2 (1=imperial, 2=metric output)]
00485> [NSTORM= 1]
00486> [NRUN = 0125]
00487> *****
00488> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00489> # Date : 2023-05
00490> # Modeller : JB
00491> # Company : JFSA
00492> # License # : 2582634
00493> *****
00494> #*****
00495> R0125:C00002-----
00496> READ STORM
00497> Filename = storm.001
00498> Comment = 25 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00499> [SDT=10.00:SDUR= 24.00:PTOT= 86.41]
00500> R0125:C00003-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00501> CALIB STANDHYD 1.0 01:Post 4.71 1.046 No.date 12:01 60.68 .702 .000
00502> [XfPM:57:TIMP:.67]
00503> [Horton parameters: Fm= 76.20:Fc= 13.20:DCAY=4.14: F= .00]
00504> [Previous area: IAPer= 4.67:SLPP=2.00:LGPs= 40.:MNP=.250:SCPs= .0]
00505> [Impervious area: IALmp= 1.57:SLPI=.50:LGIs= 177.:MNI=.013:SCIs= .0]
00506> R0125:C00004-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00507> ROUTE RESERVOIR -> 1.0 02:POST 4.71 1.046 No.date 12:01 60.68 n/a .000
00508> out <= 1.0 01:SMW-Out 4.71 .108 No.date 12:35 60.68 n/a .000
00509> overflow <= 1.0 03:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00510> (MxStoUsed=.1766E+00 n3, TotDvVol=.0000E+00 n3, N-Ovf= 0, TotDurOvf= 0.hrs)
00511> R0125:C00005-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00512> ADD HYD + 1.0 02:SMW-Over 4.71 .108 No.date 12:35 60.68 n/a .000
00513> 1.0 02:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00514> SUM= 1.0 01:Total 4.71 .108 No.date 12:35 60.68 n/a .000
00515> ** END OF RUN : 149
00516>
00517>
00518>
00519>
00520>
00521>
00522>
00523> RUN:COMMAND#
00524> R0150:C00001-----
00525> START
00526> [TZERO = .00 hrs on 0]
00527> [METOUT= 2 (1=imperial, 2=metric output)]
00528> [NSTORM= 1]
00529> [NRUN = 0150]
00530> *****
00531> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00532> # Date : 2023-05
00533> # Modeller : JB
00534> # Company : JFSA
00535> # License # : 2582634
00536> *****
00537> #*****
00538> R0150:C00002-----
00539> READ STORM
00540> Filename = storm.001
00541> Comment = 50 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00542> [SDT=10.00:SDUR= 24.00:PTOT= 95.10]
00543> R0150:C00003-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00544> CALIB STANDHYD 1.0 01:Post 4.71 1.186 No.date 12:00 67.45 .709 .000
00545> [XfPM:57:TIMP:.67]
00546> [Horton parameters: Fm= 76.20:Fc= 13.20:DCAY=4.14: F= .00]
00547> [Previous area: IAPer= 4.67:SLPP=2.00:LGPs= 40.:MNP=.250:SCPs= .0]
00548> [Impervious area: IALmp= 1.57:SLPI=.50:LGIs= 177.:MNI=.013:SCIs= .0]
00549> R0150:C00004-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00550> ROUTE RESERVOIR -> 1.0 02:POST 4.71 1.186 No.date 12:00 67.45 n/a .000
00551> out <= 1.0 01:SMW-Out 4.71 .128 No.date 12:34 67.45 n/a .000
00552> overflow <= 1.0 03:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00553> (MxStoUsed=.1951E+00 n3, TotDvVol=.0000E+00 n3, N-Ovf= 0, TotDurOvf= 0.hrs)
00554> R0150:C00005-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00555> ADD HYD + 1.0 02:SMW-Over 4.71 .128 No.date 12:34 67.45 n/a .000
00556> 1.0 02:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00557> SUM= 1.0 01:Total 4.71 .128 No.date 12:34 67.45 n/a .000
00558> ** END OF RUN : 198
00559>
00560>
00561>
00562>
00563>
00564>
00565>
00566> RUN:COMMAND#
00567> R0199:C00001-----
00568> START
00569> [TZERO = .00 hrs on 0]
00570> [METOUT= 2 (1=imperial, 2=metric output)]
00571> [NSTORM= 1]
00572> [NRUN = 0199]
00573> *****
00574> # Project Name: [P2468-JB Hogan Property - Belleville] Project Number: [2468]
00575> # Date : 2023-05
00576> # Modeller : JB
00577> # Company : JFSA
00578> # License # : 2582634
00579> *****
00580> #*****
00581> R0199:C00002-----
00582> READ STORM
00583> Filename = storm.001
00584> Comment = 100 years SCS Type 2 Storm 24 Hours step 10 min, Belleville
00585> [SDT=10.00:SDUR= 24.00:PTOT= 103.98]
00586> R0199:C00003-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00587> CALIB STANDHYD 1.0 01:Post 4.71 1.312 No.date 12:00 74.21 .714 .000
00588> [XfPM:57:TIMP:.67]
00589> [Horton parameters: Fm= 76.20:Fc= 13.20:DCAY=4.14: F= .00]
00590> [Previous area: IAPer= 4.67:SLPP=2.00:LGPs= 40.:MNP=.250:SCPs= .0]
00591> [Impervious area: IALmp= 1.57:SLPI=.50:LGIs= 177.:MNI=.013:SCIs= .0]
00592> R0199:C00004-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00593> ROUTE RESERVOIR -> 1.0 02:POST 4.71 1.312 No.date 12:00 74.21 n/a .000
00594> out <= 1.0 01:SMW-Out 4.71 .146 No.date 12:34 74.21 n/a .000
00595> overflow <= 1.0 03:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00596> (MxStoUsed=.2140E+00 n3, TotDvVol=.0000E+00 n3, N-Ovf= 0, TotDurOvf= 0.hrs)
00597> R0199:C00005-----DTIn-ID:NYHD-----AREAh-QPEAKCms-TpeakDate,h:mm-----Rvmm-R.C-----DfCms
00598> ADD HYD + 1.0 02:SMW-Over 4.71 .146 No.date 12:34 74.21 n/a .000
00599> 1.0 02:SMW-Over .00 .000 No.date 0:00 .00 n/a .000
00600> SUM= 1.0 01:Total 4.71 .146 No.date 12:34 74.21 n/a .000
00601> R0199:C00006-----
00602> FINISH
00603>
00604> *****
00605> WARNINGS / ERRORS / NOTES
00606>
00607> Simulation ended on 2023-06-28 at 15:10:26
00608> =====
00609>

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